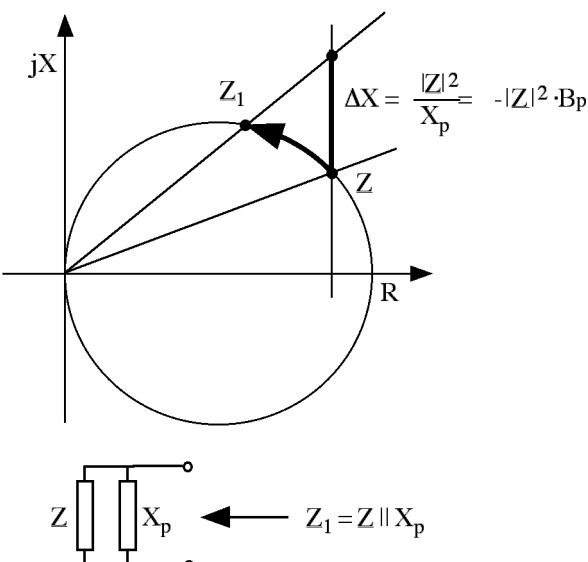
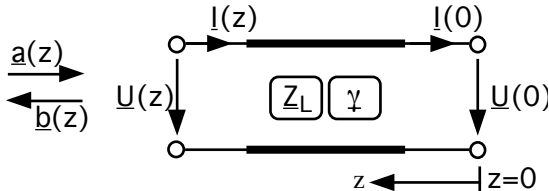
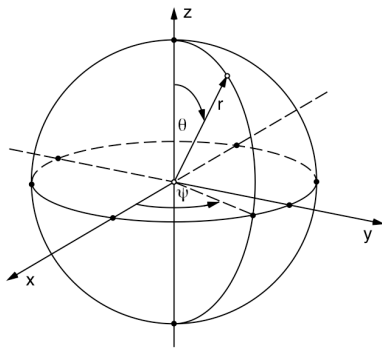


Formelblatt zur Vorlesung 'Grundlagen der Hochfrequenztechnik'

Impedanz $\longleftrightarrow \frac{Z=1/Y}{\text{Admittanz}}$ $\underline{Z} = R + jX \quad \underline{Y} = G + jB$ $\underline{Z} = \frac{G}{G^2 + B^2} - j \frac{B}{G^2 + B^2} \quad \underline{Y} = \frac{R}{R^2 + X^2} - j \frac{X}{R^2 + X^2}$	Hilfskonstruktion zur Transformation 
Kompensation mit dualen Elementen  Bedingungen für Kompensation: $X_s = R^2 \cdot B_p$ Frequenzfaktor: $F(f) = \sqrt{X_s \cdot B_p}$ krit. Frequenz, Grenzfrequenz: $F(f_k) = 1$	Leitungen  $\underline{U}(z) = \underline{U}_H(0)e^{\gamma z} + \underline{U}_R(0)e^{-\gamma z} = \sqrt{\underline{Z}_L} (\underline{a}(z) + \underline{b}(z))$ $\underline{I}(z) = \frac{\underline{U}_H(0)}{\underline{Z}_L} e^{\gamma z} - \frac{\underline{U}_R(0)}{\underline{Z}_L} e^{-\gamma z} = \frac{1}{\sqrt{\underline{Z}_L}} (\underline{a}(z) - \underline{b}(z))$ $\underline{\gamma} = \alpha + j\beta = \sqrt{(R' + j\omega L')(G' + j\omega C')}; \quad \underline{Z}_L = \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}}$
Koaxialleitung $\underline{Z}_L = \frac{1}{2\pi} \cdot \sqrt{\frac{\mu}{\epsilon}} \cdot \ln\left(\frac{\rho_2}{\rho_1}\right)$	ungedämpfte Leitung (homogenes Dielektrikum und konst. Querschnitt) $\beta = \omega \cdot \sqrt{L'C'} = \omega \cdot \sqrt{\mu\epsilon}; \quad \lambda = \frac{2\pi}{\beta}; \quad C' = \frac{\sqrt{\mu\epsilon}}{\underline{Z}_L}; \quad L' = \underline{Z}_L \cdot \sqrt{\mu\epsilon}; \quad v_\varphi = \frac{\omega}{\beta}$
schwach gedämpfte Leitungen ($R' \ll \omega L'; G' \ll \omega C'$) $\alpha \approx \frac{1}{2} \left(\frac{R'}{\underline{Z}_L} + G' \cdot \underline{Z}_L \right); \quad G' = \omega C' \cdot \tan(\delta_c); \quad R' \sim \frac{1}{\kappa \cdot s}$	Dämpfung einer Leitung der Länge l (für hinlaufende Welle a) $D/dB = 10 \cdot \log\left(\frac{P_a(l)}{P_a(0)}\right) = 10 \cdot \log(e^{2\alpha l})$
Eindringtiefe s $s = \sqrt{\frac{2}{\omega \kappa \mu}}$	Reflexionsfaktor r $\underline{r}(z) = \frac{\underline{U}_R(z)}{\underline{U}_H(z)} = \frac{\underline{b}(z)}{\underline{a}(z)} = \frac{\underline{b}(0)}{\underline{a}(0)} \cdot e^{-2\gamma z}$ Reflexionsfaktor → Impedanz $\underline{r}(l) = \frac{\underline{Z}(l) - \underline{Z}_L}{\underline{Z}(l) + \underline{Z}_L}; \quad \underline{Z}(l) = \frac{\underline{U}(l)}{\underline{I}(l)} = \frac{1 + \underline{r}(l)}{1 - \underline{r}(l)} \cdot \underline{Z}_L$
Anpassungsfaktor, Stehwellenverhältnis $m = \frac{1}{VSWR} = \frac{1 - \underline{r} }{1 + \underline{r} } = \frac{U_{\min}}{U_{\max}}$	Dem Verbraucher zugeführte Wirkleistung P_w mit: $\underline{a}(z) = \frac{\underline{U}_H(z)}{\sqrt{\underline{Z}_L}} = \sqrt{\underline{Z}_L} \cdot \underline{I}_H(z)$ $P_w = P_a(0) - P_b(0) = \frac{1}{2} \left(\underline{a}(0) ^2 - \underline{b}(0) ^2 \right) = \frac{1}{2} \underline{a}(0) ^2 \cdot (1 - \underline{r}(0) ^2)$
Transformation durch Kettenschaltung einer Leitung $\underline{Z}(l) = \underline{Z}_L \cdot \frac{\underline{Z}(0) + \underline{Z}_L \tanh(\underline{\gamma} l)}{\underline{Z}_L + \underline{Z}(0) \tanh(\underline{\gamma} l)} = \underline{Z}(0) \cdot \frac{1 + j \frac{\underline{Z}_L}{\underline{Z}(0)} \tan(\beta l)}{1 + j \frac{\underline{Z}(0)}{\underline{Z}_L} \tan(\beta l)} \Bigg _{\alpha=0}$ Konstanten $\underline{Z}_{F0} = \sqrt{\frac{\mu_o}{\epsilon_o}} = 120\pi \Omega$ $c_o = 2,997925 \cdot 10^8 \frac{m}{s}$ $k = 1,38065 \cdot 10^{-23} \frac{Ws}{K}$ $\mu_o = 4\pi \cdot 10^{-7} \frac{Vs}{Am}$ $\epsilon_o = 8,854 \cdot 10^{-12} \frac{As}{Vm}$	Kugelkoordinaten  Azimuth: ψ Elevation: θ Volumen: $V = \frac{4}{3} \pi r^3$ Oberfläche: $F = 4\pi r^2$
Anmerkung: Dieses Doppelblatt wird Ihnen zur Prüfung als einziges Hilfsmittel ausgeteilt. Versuchen Sie deshalb zumindest in der Endphase der Prüfungsvorbereitung, alle Aufgaben ohne weitere Hilfen zu lösen!	

Umrechnung verschiedener Zweitorparameter

	[S]	[Z]	[Y]	[A](ABCD)	[T]
S ₁₁	S ₁₁	$\frac{(Z_{11} - Z_0)(Z_{22} + Z_0) - Z_{12}Z_{21}}{(Z_{11} + Z_0)(Z_{22} + Z_0) - Z_{12}Z_{21}}$	$\frac{(Y_0 - Y_{11})(Y_0 + Y_{22}) + Y_{12}Y_{21}}{(Y_{11} + Y_0)(Y_{22} + Y_0) - Y_{12}Y_{21}}$	$\frac{A + B/Z_0 - CZ_0 - D}{A + B/Z_0 + CZ_0 + D}$	$\frac{T_{12}}{T_{22}}$
S ₁₂	S ₁₂	$\frac{2Z_{12}Z_0}{(Z_{11} + Z_0)(Z_{22} + Z_0) - Z_{12}Z_{21}}$	$\frac{-2Y_{12}Y_0}{(Y_{11} + Y_0)(Y_{22} + Y_0) - Y_{12}Y_{21}}$	$\frac{2(AD - BC)}{A + B/Z_0 + CZ_0 + D}$	$\frac{T_{11}T_{22} - T_{12}T_{21}}{T_{22}}$
S ₂₁	S ₂₁	$\frac{2Z_{21}Z_0}{(Z_{11} + Z_0)(Z_{22} + Z_0) - Z_{12}Z_{21}}$	$\frac{-2Y_{21}Y_0}{(Y_{11} + Y_0)(Y_{22} + Y_0) - Y_{12}Y_{21}}$	$\frac{A + B/Z_0 + CZ_0 + D}{-A + B/Z_0 - CZ_0 + D}$	$\frac{1}{T_{22}}$
S ₂₂	S ₂₂	$\frac{2Z_{12}Z_{21}}{(Z_{11} + Z_0)(Z_{22} + Z_0) - Z_{12}Z_{21}}$	$\frac{2Y_{12}Y_{21}}{(Y_{11} + Y_0)(Y_{22} + Y_0) - Y_{12}Y_{21}}$	$\frac{A + B/Z_0 + CZ_0 + D}{A + B/Z_0 + CZ_0 + D}$	$\frac{T_{22}}{-T_{21}}$
Z ₁₁	$Z_0 \frac{(1 + S_{11})(1 - S_{22}) + S_{12}S_{21}}{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}$	Z ₁₁	$\frac{Y_{22}}{Y_{11}Y_{22} - Y_{12}Y_{21}}$	$\frac{A}{C}$	
Z ₁₂	$Z_0 \frac{2S_{12}}{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}$	Z ₁₂	$\frac{-Y_{12}}{Y_{11}Y_{22} - Y_{12}Y_{21}}$	$\frac{AD - BC}{C}$	
Z ₂₁	$Z_0 \frac{2S_{21}}{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}$	Z ₂₁	$\frac{-Y_{21}}{Y_{11}Y_{22} - Y_{12}Y_{21}}$	$\frac{1}{C}$	
Z ₂₂	$Z_0 \frac{(1 - S_{11})(1 + S_{22}) + S_{12}S_{21}}{(1 - S_{11})(1 + S_{22}) - S_{12}S_{21}}$	Z ₂₂	$\frac{Y_{11}}{Y_{11}Y_{22} - Y_{12}Y_{21}}$	$\frac{D}{C}$	
Y ₁₁	$Y_0 \frac{(1 - S_{11})(1 + S_{22}) + S_{12}S_{21}}{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}$	$\frac{Z_{22}}{Z_{11}Z_{22} - Z_{12}Z_{21}}$	Y ₁₁	$\frac{D}{B}$	
Y ₁₂	$Y_0 \frac{-2S_{12}}{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}$	$\frac{-Z_{12}}{Z_{11}Z_{22} - Z_{12}Z_{21}}$	Y ₁₂	$\frac{BC - AD}{B}$	
Y ₂₁	$Y_0 \frac{-2S_{21}}{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}$	$\frac{-Z_{21}}{Z_{11}Z_{22} - Z_{12}Z_{21}}$	Y ₂₁	$\frac{-1}{B}$	
Y ₂₂	$Y_0 \frac{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}{(1 + S_{11})(1 - S_{22}) + S_{12}S_{21}}$	$\frac{Z_{11}}{Z_{11}Z_{22} - Z_{12}Z_{21}}$	Y ₂₂	$\frac{A}{B}$	
A	$\frac{(1 + S_{11})(1 - S_{22}) + S_{12}S_{21}}{2S_{21}}$	$\frac{Z_{11}}{Z_{21}}$	$\frac{-Y_{22}}{Y_{21}}$	A	
B	$Z_0 \frac{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}{2S_{21}}$	$\frac{Z_{11}Z_{22} - Z_{12}Z_{21}}{Z_{21}}$	$\frac{-1}{Y_{21}}$	B	
C	$\frac{1}{Z_0} \frac{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}{2S_{21}}$	$\frac{1}{Z_{21}}$	$\frac{Y_{12}Y_{21} - Y_{11}Y_{22}}{Y_{21}}$	C	
D	$\frac{(1 - S_{11})(1 + S_{22}) + S_{12}S_{21}}{2S_{21}}$	$\frac{Z_{22}}{Z_{21}}$	$\frac{Y_{22}}{Y_{21}}$	D	
T ₁₁	$\frac{S_{12}S_{21} - S_{11}S_{22}}{S_{21}}$				T ₁₁
T ₁₂	$\frac{S_{11}}{S_{21}}$				T ₁₂
T ₂₁	$\frac{S_{21}}{-S_{22}}$				T ₂₁
T ₂₂	$\frac{1}{S_{21}}$				T ₂₂