Institute for Biomedical Engineering, Karlsruhe Institute of Technology

Electromagnetics and Numerical Calculation of Fields

Lecture: Prof. Dr. rer nat Olaf Dössel

Examination 2011

Question 1

Write down the Maxwell's equations in differential and integral form (arbitrary materials). [8 pt]

Question 2

 \mathbf{E}_1 and \mathbf{E}_2 are given by

a)
$$\mathbf{E}_{1} = k \cdot \begin{pmatrix} yz \\ xy \\ 2xz \end{pmatrix}$$

b)
$$\mathbf{E}_{2} = k \cdot \begin{pmatrix} y^{2} \\ 2xy + z \\ y \end{pmatrix}$$

where k is a constant with appropriate units.

- (a) Which of these is an electrostatic field. (What was that again about the curl...) [4 pt]
- (b) For the electrostatic field, find the potential $\phi(x_0, y_0, z_0)$. Use the origin as your reference point. Hint: You must integrate along an arbitrary path from (0, 0, 0) to (x_0, y_0, z_0) . [8 pt]
- (c) Check the results by calculating $\mathbf{E} = -\nabla \phi$. [2 pt]

Find the capacitance of a cylindrical capacitor with inner radius R_i , outer radius R_a , Length L where $L >> R_a$ and the dielectric constant $\epsilon_r = 1$ (Vacuum) [6 pt]



Question 4

Find the electrostatic force between the plates of a parallel plate capacitor (area A, distance s and dielectric constant $\epsilon_r = 1$) via the electric field energy. [4 pt]

Question 5

- (a) Give the "lumped element" circuit of one piece of transmission line (Transmission line model).
 [4 pt]
- (b) Give the formula for the characteristic impedance of a lossless transmission line? [2 pt]
- (c) Give the formula for the phase velocity of a wave propagating in a lossless transmission line ? [2 pt]
- (d) What do you have to do to avoid reflection at the end of a terminated transmission line. [2 pt]

- (a) What is characteristic for TM waves in a waveguide and what is characteristic for TE waves in a waveguide ? [4 pt]
- (b) What is the meaning of "cut-off frequency" for a specific mode ? [2 pt]

- (a) What is the meaning of the Poynting vector \mathbf{S} ? [2 pt]
- (b) Give the formular to determine \mathbf{S} from a given electromagnetic field. [2 pt]
- (c) Give a sketch of the electric and magnetic field lines of a wave propagating in a coaxial cable (Sketch of the cross section of the coaxial cable is sufficient !). [4 pt]
- (d) Give a sketch of the Poynting vector along a piece of one wavelength of a coaxial line (Sketch of the side view of the coaxial cable) [2 pt]



Question 8

Derive the general wave equation for conducting, dielectric, paramagnetic, isotropic and linear materials with charge density $\rho = 0$ from the Maxwell equations. [10 pt] Hint: rot rot $\mathbf{F} = \operatorname{grad} \operatorname{div} \mathbf{F} - \Delta \mathbf{F}$

Question 9

Give a sketch of Yee's lattice (FDTD). [6 pt]

- (a) Describe the basic idea and equations of the Finite Element Method using Weighted Residuals with Poisson's Equation as an example. [8 pt]
 - What is the Residuum?
 - Show how to find the best approximation.
 - Show how to apply the Green's 2nd identity to obtain the weak form without second derivatives.
 - What was Galerkin's idea?
 - Give a formula, how to approximate a scalar function ϕ using linear node shape functions. Hint: $\int (\psi \Delta \phi + (\nabla \psi)(\nabla \phi)) dv = \int \psi(\nabla \phi) d\mathbf{a}$
- (b) Give a sketch of the linear shape functions in 1D case. [4 pt]

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Examination 2011: Solutions

Question 1

$$\nabla \cdot \mathbf{D} = \rho \leftrightarrow \int_{S} \mathbf{D} d\mathbf{a} = \int \rho dV \tag{1}$$

$$\nabla \times \mathbf{E} = -\frac{\partial}{\partial t} \mathbf{B} \leftrightarrow \int_C \mathbf{E} d\mathbf{l} = -\frac{\partial}{\partial t} \int_S \mathbf{B} d\mathbf{a}$$
(2)

$$\nabla \cdot \mathbf{B} = 0 \leftrightarrow \int_{S} \mathbf{B} d\mathbf{a} = 0 \tag{3}$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial}{\partial t} \mathbf{D} \leftrightarrow \int_{C} \mathbf{H} d\mathbf{l} = \int_{S} (\mathbf{J} + \frac{\partial}{\partial t} \mathbf{D}) d\mathbf{a}$$
(4)

Question 2

(a)

$$\nabla \times \mathbf{E}_1 = k \begin{pmatrix} 0 - 0 \\ y - 2z \\ y - z \end{pmatrix} \neq 0 \rightarrow \text{Impossible electrostatic field !}$$
$$\nabla \times \mathbf{E}_2 = k \begin{pmatrix} 1 - 1 \\ 0 - 0 \\ 2y - 2y \end{pmatrix} = 0 \rightarrow \text{Possible electrostatic field !}$$

(b) Proposed Path:

Step I:
$$y = z = 0 \rightarrow \int \mathbf{E}_2 \, d\mathbf{l} = \int ky^2 dx = 0$$
(since y=0)
Step II: $x = x_0, y : 0 \rightarrow y_0, z = 0 \rightarrow \int \mathbf{E}_2 \, d\mathbf{l} = 2kx_0 \int_0^{y_0} y dy = kx_0 y_0^2$
Step III: $x = x_0, y = y_0, z : 0 \rightarrow z_0 \rightarrow \int \mathbf{E}_2 \, d\mathbf{l} = ky_0 \int_0^{z_0} 1 dz = ky_0 z_0$
 $\rightarrow V(x_0, y_0, z_0) = -\int \mathbf{E}_2 d\mathbf{l} = -\sum_{\text{Step I - III}} = -k(x_0 y_0^2 + y_0 z_0)$
or $V(x, y, z) = -k(xy^2 + yz)$



Figure 1: Proposed Path

$$\int \mathbf{E}d\mathbf{a} = \frac{Q}{\epsilon_0} \tag{5}$$

$$\rightarrow E_r = \frac{Q}{2\pi\epsilon_0 L} \frac{1}{r} \tag{6}$$

$$U = \int_{R_i}^{R_a} E_r dr = \frac{Q}{2\pi\epsilon_0 L} ln\left(\frac{R_a}{R_i}\right) \tag{7}$$

$$C = \frac{Q}{U} \tag{8}$$

$$\rightarrow C = \frac{2\pi\epsilon_0 L}{\ln\left(\frac{R_a}{R_i}\right)} \tag{9}$$

(10)

$$W_e = \frac{1}{2}CU^2 = \frac{1}{2}\frac{Q^2}{C}$$
(11)

$$C = \frac{\epsilon_0 A}{s} \tag{12}$$

$$F_Q = \left| -\frac{\partial}{\partial s} \left(\frac{1}{2} \frac{s}{\epsilon_0 A} Q^2 \right) \right| = \frac{1}{2} \frac{1}{\epsilon_0 A} Q^2 \tag{13}$$

(a) Transmission line:



(b)

$$Z_0 = \sqrt{\frac{L}{C}} \tag{14}$$

(c)

$$v = \frac{1}{\sqrt{LC}} \tag{15}$$

(d) The load impedance has to be equal to the characteristic impedance of the transmission line.

Question 6

- (a) For TE waves the electric field is completely transverse to the direction of propagation, $E_z = 0$. For TM waves the magnetic field is completely transverse to the direction of propagation, $H_z = 0$.
- (b) For every mode, the cut-off frequency is the lowest frequency that allows undamped propagation.

- (a) The Poynting vector is the power per area that is transmitted through a given area via electromagnetic fields.
- (b) Power flux density:

$$\mathbf{S} = \mathbf{E} \times \mathbf{H} \tag{16}$$

(c) and (d) (d)



Give a sketch of E and B

Question 8

$$\mathbf{D} = \epsilon_0 \epsilon \mathbf{E} = \epsilon \mathbf{E} \tag{17}$$

$$\nabla \times \mathbf{E} = -\mu \frac{\partial}{\partial t} \mathbf{H}$$
(18)

$$\nabla \times \nabla \times \mathbf{E} = -\mu \nabla \times \frac{\partial}{\partial t} \mathbf{H}$$
⁽¹⁹⁾

$$\nabla \nabla \mathbf{E} - \Delta \mathbf{E} = -\mu \frac{\partial}{\partial t} \nabla \times \mathbf{H}$$
(20)
$$\nabla \mathbf{E} = 0$$
(21)

$$\nabla \mathbf{E} = 0 \tag{21}$$

$$\rightarrow \Delta \mathbf{E} - \mu \frac{\partial}{\partial t} (\mathbf{J} + \epsilon \frac{\partial}{\partial t} \mathbf{E}) = 0$$
⁽²²⁾

$$\Delta \mathbf{E} - \mu \kappa \frac{\partial}{\partial t} \mathbf{E} - \mu \epsilon \frac{\partial^2}{\partial t^2} \mathbf{E} = 0$$
⁽²³⁾

$$\mathbf{H} = \frac{1}{\mu_0 \mu_r} \mathbf{B} = \frac{1}{\mu} \mathbf{B}$$
(24)

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial}{\partial t} \mathbf{D}$$
(25)

$$\nabla \times \nabla \times \mathbf{H} = \kappa \nabla \times \mathbf{E} + \epsilon \nabla \times \frac{\partial}{\partial t} \mathbf{E}$$
(26)

$$\nabla \nabla \mathbf{H} - \Delta \mathbf{H} = -\mu \kappa \frac{\partial}{\partial t} \mathbf{H} + \epsilon \frac{\partial}{\partial t} \nabla \times \mathbf{E}$$
(27)

$$\nabla \nabla \mathbf{H} - \Delta \mathbf{H} = -\mu \kappa \frac{\partial}{\partial t} \mathbf{H} - \mu \epsilon \frac{\partial^2}{\partial t^2} \mathbf{H}$$
(28)
$$\nabla \mathbf{H} = 0$$
(29)

$$\mathbf{H} = 0 \tag{29}$$

$$\rightarrow \Delta \mathbf{H} - \mu \kappa \frac{\partial}{\partial t} \mathbf{H} - \mu \epsilon \frac{\partial^2}{\partial t^2} \mathbf{H} = 0$$
(30)

(31)





(a) Poisson's equation:

$$\Delta \phi = -\frac{\rho}{\epsilon} \tag{32}$$

Ideal solution:

$$\Delta \phi + \frac{\rho}{\epsilon} = 0 \tag{33}$$

Approximated solution:

$$\Delta \tilde{\phi} + \frac{\rho}{\epsilon} = R \tag{34}$$

where R is the Residuum Best approximation:

$$\int \omega \cdot R dv = \int \left(\Delta \tilde{\phi} + \frac{\rho}{\epsilon}\right) \omega dv = 0 \tag{35}$$

where ω is the weighting function Using Green's 2nd law:

$$\int (\nabla \tilde{\phi}) (\nabla \omega) dv - \int \omega \frac{\partial \tilde{\phi}}{\partial n} da - \int \frac{\rho}{\epsilon} \omega dv = 0$$
(36)

In the Galerkin's method, the weighting functions are chosen to be the basis functions (node shape functions):

$$\tilde{\phi} = \sum_{l=1}^{nodes} \alpha_l(x, y, z) \phi_l \tag{37}$$

$$\omega_l(x, y, z) = \alpha_l(x, y, z) \tag{38}$$

(b) Linear 1D shape functions:

