Computational Photonics

Finite-Difference Time-Domain

Relation between frequency and time domain

• the frequency spectrum used for the illumination is given by the Fourier-transformation of the time dependent incident field



 with a single calculation we can calculate the entire frequency response, detecting the temporal evolution of the field behind a structure and FT (N_t = total number of time steps)

$$\triangle f = \frac{1}{T} = \frac{1}{N_t \cdot \triangle t}$$

(frequency resolution)

$$\triangle \lambda = \frac{\lambda^2}{c \cdot \triangle t \cdot N_t}$$

(wavelength resolution) 2

Relation between frequency and time domain

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- with a single calculation we can calculate the entire frequency response, detecting the temporal evolution of the field behind a structure and FT (N_t = total number of time steps)
 - ➡ for a high resolution in the wavelength domain, we have to record the temporal evolution of the field for an excess in time kind of disadvantage

Example of a grating wave guide coupler



(n1=1.58, n2=1.87,d1=d2=165nm, TE)

Example of a grating wave guide coupler



transmission function of a PC wave guide (n1=1.58, n2=1.87,d1=d2=165nm, TE)

Example of a grating wave guide coupler



z in μ**m**

0

Amplitude at λ =0.1768 μ m



dips are waveguide resonances excited if the momentum provided by the grating matches the propagation constant of a waveguide mode

Inclusion of other materials

- FDTD is not directly applicable for materials with $\epsilon < 1$ (e.g. metals)
- material properties depend strongly on the wavelength (dispersion)
- nonlinear properties of interest (instantaneous or non-instantaneous)
- great diversity of approaches, but they require usually all the simulation of an additional quantity

PPolarisation

 ${\rm \circ}~$ so far we have taken into account ${\rm E}$ and ${\rm H}$



Displacement

FDTD for metals



+ eqn. relating current and electric field (Drude model, mean drift velocity of electrons in a field)

$$\frac{\partial \mathbf{J}}{\partial t} + \gamma \mathbf{J} = \epsilon_0 \omega_{\mathrm{P}}^2 \mathbf{E}$$

 $\omega_{\rm P} \implies$ plasma frequency $1/\gamma \implies$ relaxation time τ



FDTD for metals

Maxwell: $\nabla \times \mathbf{E} = -\mu_0 \frac{\partial \mathbf{H}}{\partial t}$ $\nabla \times \mathbf{H} = \epsilon_{\mathrm{BG}} \epsilon_0 \frac{\partial \mathbf{E}}{\partial t} + \mathbf{J}$

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scattering cross section of a circular silver cylinder (r=25nm, TM)

FDTD for Lorentz-materials

• assuming a 2D geometry (y-z-plane) with TM polarisation

 $\mathbf{E} = E_x \hat{x} \qquad \qquad \mathbf{P} = P_x \hat{x}$

Lorentz dispersion (frequency domain) (the same as Drude-model but resonance frequency is not at 0)

$$P_{x,\omega} = \frac{\epsilon_0 \omega_p^2 \chi_L}{\omega_0^2 - \omega^2 + j \omega \Gamma} E_{x,\omega}$$

Fouriertransformation

Lorentz dispersion (time domain)

$$\frac{\partial^2 P_x}{\partial t^2} + \Gamma \frac{\partial P_x}{\partial t} + \omega_0^2 P_x = \epsilon_0 \omega_p^2 \chi_L E_x$$

(R.W. Ziolkowski et al., JOSA A, Vol. 16, No. 4, 980)

FDTD for nonlinear/nondispersive materials

• going back to Maxwell's equations

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \qquad \nabla \cdot \mathbf{D} = \rho$$
$$\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t} + \mathbf{j} \qquad \nabla \cdot \mathbf{B} = 0$$

$$\implies$$
 linear: $\mathbf{D} = \epsilon \epsilon_0 \mathbf{E}$

instantaneous!

$$\implies \text{non-Linear:} \quad \mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P}$$
$$\mathbf{P} = \epsilon_0 \left[\hat{\chi}^{(1)} \mathbf{E} + \hat{\chi}^{(2)} \mathbf{E}^2 + \hat{\chi}^{(3)} \mathbf{E}^3 + \cdots \right]$$

• EXAMPLE OF AN INSTANTANEOUS Kerr $\hat{\chi}^{(3)}$ nonlinearity

$$D = \epsilon_0 \epsilon E \quad \epsilon = n^2$$

= $(n_0 + n_2 |E|^2)^2$
 $\simeq n_0^2 + 2n_0 n_2 |E|^2$

nonlinear refractive index depends on the square of the E-Field $(n_2 \ll n_0)$

$$E = \frac{D}{n_0^2 + 2n_0 n_2 |E|^2}$$

solution by a Newton iterative procedure (or direct)

 \Rightarrow straight forward applicable to instantaneous $\hat{\chi}^{(2)}$ media

• problems appear if the fields at the boundary have to be evaluated



- for keeping the discretized mesh treatable on a computer, we have to limit its size
 but
- for a proper determination of the field components that are positioned directly at the boundary of the computational domain, we need actually information about field components outside



choosing proper boundary conditions

• easiest boundary conditions: perfectly conducting material (E or H)



(physical grid)

field cannot penetrate the structure setting the field values outside the structure equal to zero

$$\begin{split} H_x^{n+\frac{1}{2}}(j+\frac{1}{2},k+\frac{1}{2}) &= H_x^{n-\frac{1}{2}}(j+\frac{1}{2},k+\frac{1}{2}) + \\ \frac{\Delta t}{\mu(j+\frac{1}{2},k+\frac{1}{2})\Delta z} [E_y^n(j,k+\frac{1}{2}) - E_g^n(j,k-\frac{1}{2})] - \\ \frac{\Delta t}{\mu(j+\frac{1}{2},k+\frac{1}{2})\Delta y} [E_z^n(j+\frac{1}{2},k) - E_z^n(j-\frac{1}{2},k)] \end{split}$$

• Floquet-Bloch boundaries for periodic objects (gratings, photonic crystals)



Ev

(physical grid)

Ez

 H_{x}

• Incident plane wave (arbitrary propagation direction)

$$E^{\text{Inc}} \propto e^{ik_x x} e^{ik_y y} e^{ik_z z} e^{-i\omega t}$$

• Floquet-Bloch boundaries in the frequency domain (in x-direction)

$$E(x + \Lambda_x, y, z, t) = E(x, y, z, t) e^{ik_x\Lambda_x}$$

- amplitude of the field displaced by one unit cell is identical, necessary since individual unit cells of a periodic structure is indistinguishable
- only the phase changes by what is known as the Bloch phase

• Floquet-Bloch boundaries for calculating the band structure of a PC



• launching an arbitrary field distribution and recording the evolving pattern on some discrete points in the space



time evolution of the field

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$$(\epsilon = 13, R = 0.3a)$$

• launching an arbitrary field distribution and recording the evolving pattern on some discrete points in the space



 $(\epsilon = 13, R = 0.3a)$

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• all the frequencies which do not satisfy the periodic boundaries are annihilated and only the modes that are allowed to propagate persist



spectra obtained as a FFT

time evolution of the field

$$(\epsilon = 13, R = 0.3a)$$

• scanning the k-space and tracing the frequencies that persist as modes delivers the band structure via FDTD





band structure computation

$$(\epsilon = 13, R = 0.3a)$$

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 neglecting the vectorial aspect: each field component obeys a scalar wave equation

$$\frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} - \frac{1}{c^2} \frac{\partial^2 f}{\partial t^2} = 0 \quad Lf = 0$$

with $L = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} = \partial_x^2 + \partial_y^2 + \partial_z^2 - c^{-2} \partial_t^2$

$$LU = L^+ L^- U = 0$$

• for propagation in the +/- x-direction the operators are written as

$$L^{-} = \partial_{x} - c^{-1} \partial_{t} \sqrt{1 - S^{2}} \implies \text{wave propagating in the -x-direction}$$
$$L^{+} = \partial_{x} + c^{-1} \partial_{t} \sqrt{1 - S^{2}} \implies \text{wave propagating in the +x-direction}$$
$$S^{2} = \left(\frac{\partial_{y}}{c^{-1} \partial_{t}}\right)^{2} + \left(\frac{\partial_{z}}{c^{-1} \partial_{t}}\right)^{2} \qquad L^{-} f = 0$$

Engquist-Madja exact ABC (Mathematics of Computation, Vol. 31, 629, 1977)

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• direct implementation of operator not possible, but the square-root can be expanded as a Taylor-series

$$(1-S^2)^{1/2} = (1) - \frac{1}{2}S^2 + O(S^4)$$

first order approximation



nearly plane wave propagating in x-direction

$$L^{-}f = \partial_x f - c^{-1}\partial_t f = 0$$



Second order approximation

$(1-S^2)^{1/2} \approx 1 - \frac{1}{2}S^2$
$S^{2} = \left(\frac{\partial_{y}}{c^{-1}\partial_{t}}\right)^{2} + \left(\frac{\partial_{z}}{c^{-1}\partial_{t}}\right)^{2}$
$L^{-} = \partial_{x} - \frac{\partial_{t}}{c} + \frac{1}{2} \frac{c}{\partial_{t}} \left(\partial_{y}^{2} + \partial_{z}^{2} \right)$

 $L^{-}f = \partial_{xt}^{2}f - c^{-1}\partial_{tt}^{2}f + 0.5c(\partial_{yy}^{2}f + \partial_{zz}^{2}f) = 0$

- writing the differential operators as finite differences (G. Mur, IEEE Trans. Electromagnetic Compatibility, Vol. 32, 377, 1981)
- discretising the operator a half spatial step in front of the boundary (example of the boundary at x=0)

$$\partial_{xt}^2 f\Big|_{1/2,j,k}^n = \frac{1}{2\triangle t} \left(\frac{f_{1,j,k}^{n+1} - f_{0,j,k}^{n+1}}{\triangle x} - \frac{f_{1,j,k}^{n-1} - f_{0,j,k}^{n-1}}{\triangle x} \right)$$

• averaging the second time derivatives at x=0 and $x=\Delta x$

$$\partial_t^2 f = \frac{1}{2} \left[\frac{f_{0,j,k}^{n+1} - 2f_{0,j,k}^n + f_{0,j,k}^{n-1}}{{}_{\Delta}t^2} + \frac{f_{1,j,k}^{n+1} - 2f_{1,j,k}^n + f_{1,j,k}^{n-1}}{{}_{\Delta}t^2} \right]$$

• same holds for the second time derivatives in y and z direction 25

• inserting all those difference scheme leads to

$$\begin{split} f_{0,j,k}^{n+1} &= -f_{0,j,k}^{n-1} + k_1 (f_{1,j,k}^{n+1} + f_{0,j,k}^{n-1}) + k_2 (f_{1,j,k}^n + f_{0,j,k}^n) + \\ &\quad k_{3y} (f_{0,j-1,k}^n - 2f_{0,j,k}^n + f_{0,j+1,k}^n + f_{1,j-1,k}^n - 2f_{1,j,k}^n + f_{1,j+1,k}^n) + \\ &\quad k_{3z} (f_{0,j,k-1}^n - 2f_{0,j,k}^n + f_{0,j,k+1}^n + f_{1,j,k-1}^n - 2f_{1,j,k}^n + f_{1,j,k+1}^n) \end{split}$$

$$k_1 = \frac{c\Delta t - \Delta x}{c\Delta t + \Delta x} \qquad k_2 = \frac{2\Delta x}{c\Delta t + \Delta x} \qquad k_{3y} = \frac{(c\Delta t)^2 \Delta x}{2\Delta y^2 (x\Delta t + \Delta x)}$$

 \circ example for boundary x=0, similar equations for other boundaries

• fields have to be stored for 2 different time steps

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• simplification by using only the first order Taylor approximation (skipping the derivatives along the y and z directions)

$$f_{0,j,k}^{n+1} = -f_{0,j,k}^{n-1} + k_1(f_{1,j,k}^{n+1} + f_{0,j,k}^{n-1}) + k_2(f_{1,j,k}^n + f_{0,j,k}^n)$$

• only the fields components that are evaluated at this (most outer) boundary have to be updated with this equation (the tangential components of the E-field e.g. at the boundary x=0)

 \circ reflection coefficients are in the order of 10⁻²

• easy to implement

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