#### **Computational Photonics**

# Basics of grating theories

# Grating theories

- rigorous solution of the diffraction of light at a periodic structure, e.g. dielectric gratings, finite photonic crystal slabs, arrays of metallic nano particles etc.
- methods
  - A) thin element approximation (scalar approximation)
  - B) rigorous solutions (Fourier modal method)
- strategy for rigorous solution
  - finding the eigenmodes sustained in the periodic region
  - finding modal amplitudes by matching boundary condition

# Final goal calculating diffraction at a grating

characterised by a periodic variation of the materials in x and y direction



1D grating

2D grating (*biperiodic*)

(Pictures from the IAP Uni Jena, E. B. Kley)

# Final goal calculating diffraction at a grating



#### Statement of the problem in 2D

field distribution around a binary grating (TE)



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Direction and amplitude of reflected and transmitted amplitudes? <sup>6</sup>

wave number of each wave is given by

$$k = \frac{2\pi}{\lambda_0}n = \sqrt{k_x^2 + k_z^2}$$

incident wave is characterised by

 $k_{xI} = \frac{2\pi}{\lambda_0} n_I \sin\theta$  $k_{zI} = \frac{2\pi}{\lambda_0} n_I \cos\theta$ 

grating provides a momentum for each diffraction order of

$$k_{xi}=irac{2\pi}{\Lambda}$$
  $i$  integer

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$$k_{zI} = \frac{2\pi}{\lambda_0} n_I \cos\theta$$

$$k_{xI} = \frac{2\pi}{\lambda_0} n_I \sin\theta$$

diffracted waves propagate along

$$k_{xi} = i\frac{2\pi}{\Lambda} + k_0 n_I \sin\theta$$

 $k_{I/II,zi} = \sqrt{k_0^2 n_{I/II}^2 - k_{xi}^2}$ 





propagation direction of each diffracted wave (applies to all kind of diffraction; X-Ray, grating)



$$\mathbf{k}_{xi} = i\frac{2\pi}{\Lambda} + k_0 n_I \sin \theta$$
$$\mathbf{k}_{I,zi} \quad \mathbf{k}_{II,zi}$$
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$$\mathbf{k}_{I/II,zi} = \sqrt{k_0^2 n_{I/II}^2 - k_{xi}^2}$$
$$\mathbf{k}_{xi}^2 \le k_0^2 n_{I/II}^2 \implies \text{Propagating}$$
$$\mathbf{k}_{xi}^2 > k_0^2 n_{I/II}^2 \implies \text{Evanescent}$$

# Scalar theory and thin element approach

field after the grating is given by the incident field multiplied by the transmission function

$$U_T(x,y) = T(x,y)U_0(x,y) \qquad U = \mathbf{E}_{\omega} \cdot \mathbf{y}$$

$$T(x,y) = |T(x,y)|e^{i\phi(x,y)}$$



# Scalar theory and thin element approach

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  $U = \mathbf{E}_{\omega} \cdot \mathbf{y}$   
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for a phase grating the amplitude transmission function equals unity and the phase is given by

$$\phi(x) = k_0(n_{II} - n_I)f(x)$$

# Scalar theory and thin element approach

for normal plane wave illumination the field after the structure is given by

 $e^{\imath\phi(x)}$ 

amplitudes of the diffracted waves are given by Fourier series

$$T_n = \int_0^{\Lambda} e^{ik_0(n_{II} - n_I)f(x)} e^{-ik_{xn}x} dx$$

$$T_n = \mathrm{FT}\left[e^{i\phi(x)}\right]$$

amplitudes are given by a Fourier-transformation of the transmission function

# Diffraction efficiencies

Diffraction efficiency corresponds to the energy transferred into a diffraction order normalised to the incident energy (given by the Poynting vector)

# $\mathbf{S} = \mathbf{E} \times \mathbf{H}$

Introducing the plane waves into the equation leads to

$$\eta_{T,n} = \frac{p_I}{p_{II}} Re \left\{ \frac{k_{II,zi}}{k_0} \right\} |T_n|^2 \quad \begin{array}{c} \text{TE:} \quad p_{I,II} = 1\\ \text{TM:} \quad p_{I,II} = \epsilon_{I,II} \end{array}$$

$$\eta_{R,n} = Re\left\{\frac{k_{I,zi}}{k_0}\right\}|R_n|^2$$

Energy conservation for loss-less materials!!

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#### Limitations of the scalar method



#### field after illuminating a sinusoidal grating with a plane wave

 $\Lambda$  is much larger than  $\lambda$ 

thin element approach justified

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#### field after illuminating a sinusoidal grating with a plane wave

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# Limitations of the scalar method



phase of the field directly after the grating  $(h=\lambda, n_I=1, n_{II}=2, TE, sinusoidal)$ 

scalar theory fails for periods comparable to wavelength and for significant grating thicknesses

 no proper description of the field inside the grating (0<z<d)</li>

> ⇒ have to solve Maxwell's equations properly also for the region inside the grating

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