

Electronics for Physicists

Analog Electronics

Chapter 2; Lecture 05

Frank Simon

Institute for Data Processing and Electronics

14.11.2023

KIT, Winter 2023/24

Chapter 2

Circuits with R, C, L

- AC behavior of R, C, L
- Complex Voltages & Currents
- Filters
- Oscillators

Overview

1. Basics
2. Circuits with R, C, L with Alternating Current
3. Diodes
4. Operational Amplifiers
5. Transistors - Basics
6. 2-Transistor Circuits
7. Field Effect Transistors
8. Additional Topics
 - Filters
 - Voltage Regulators
 - Noise

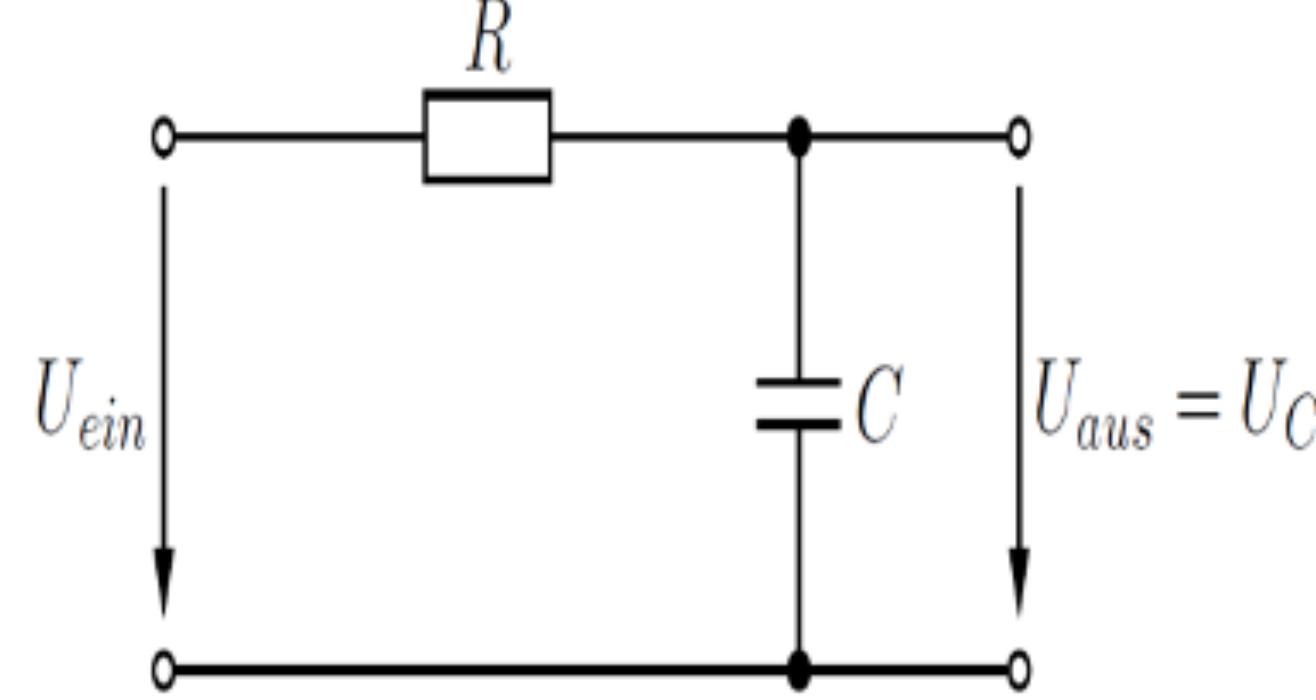
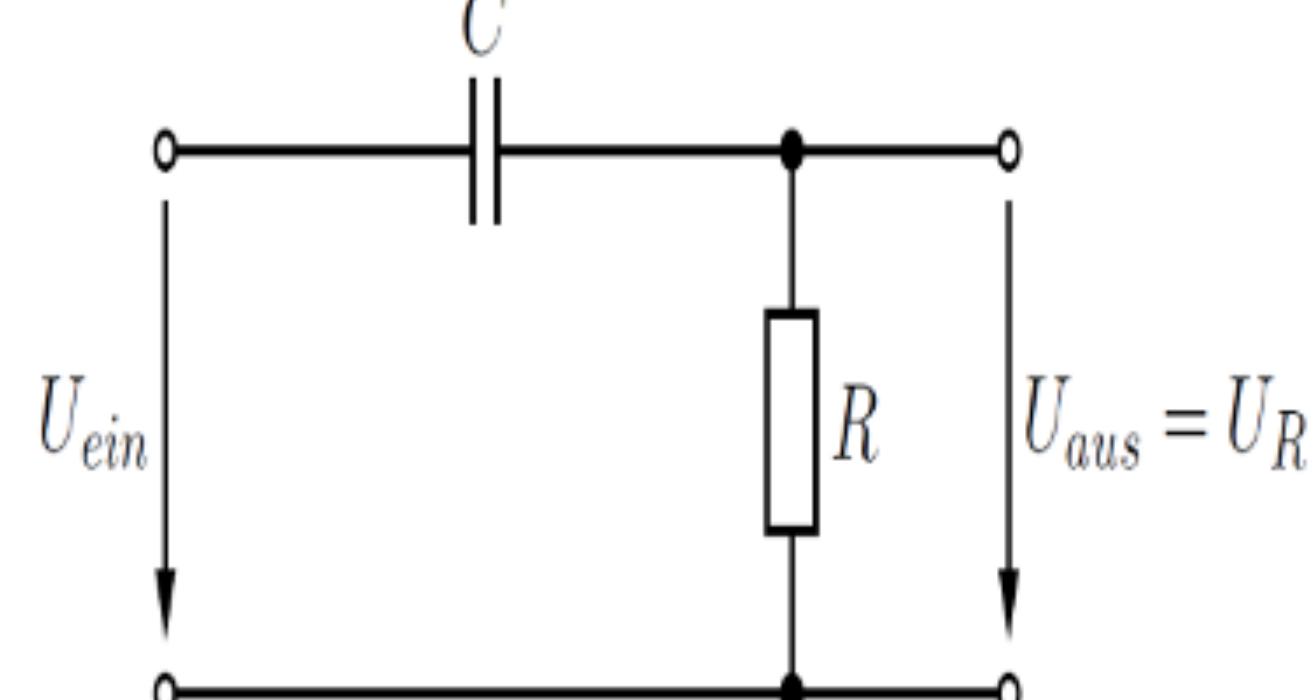
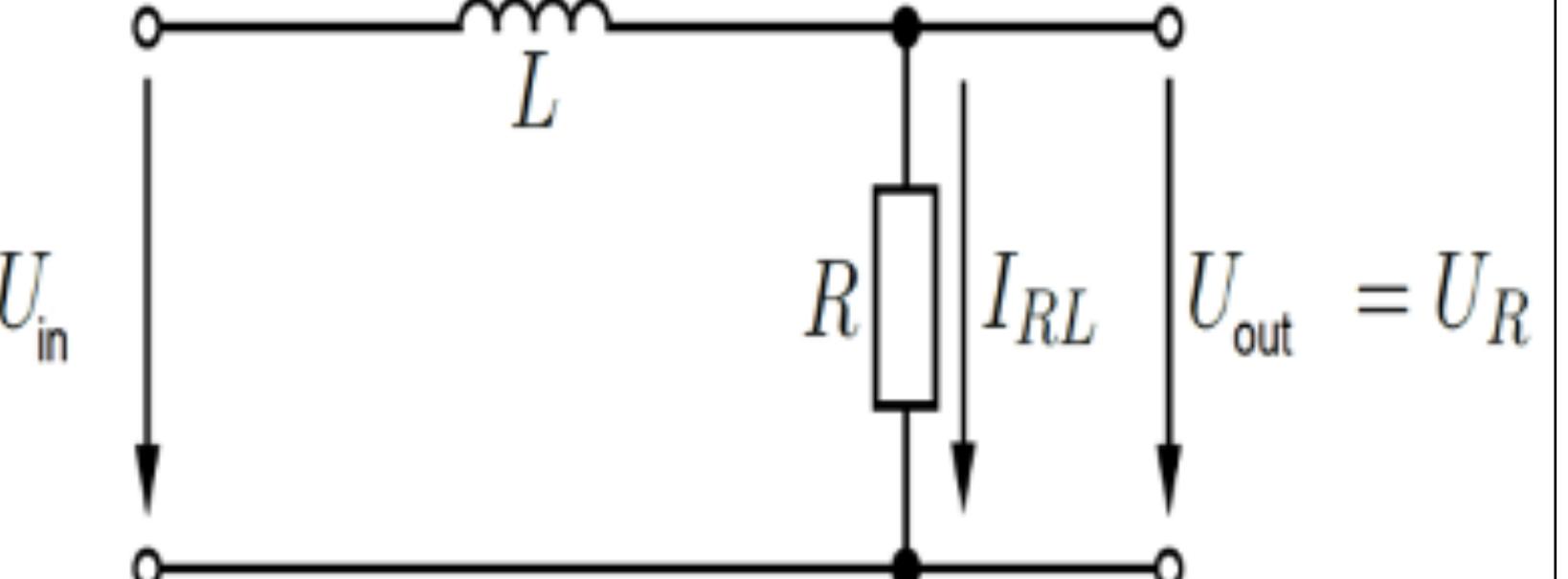
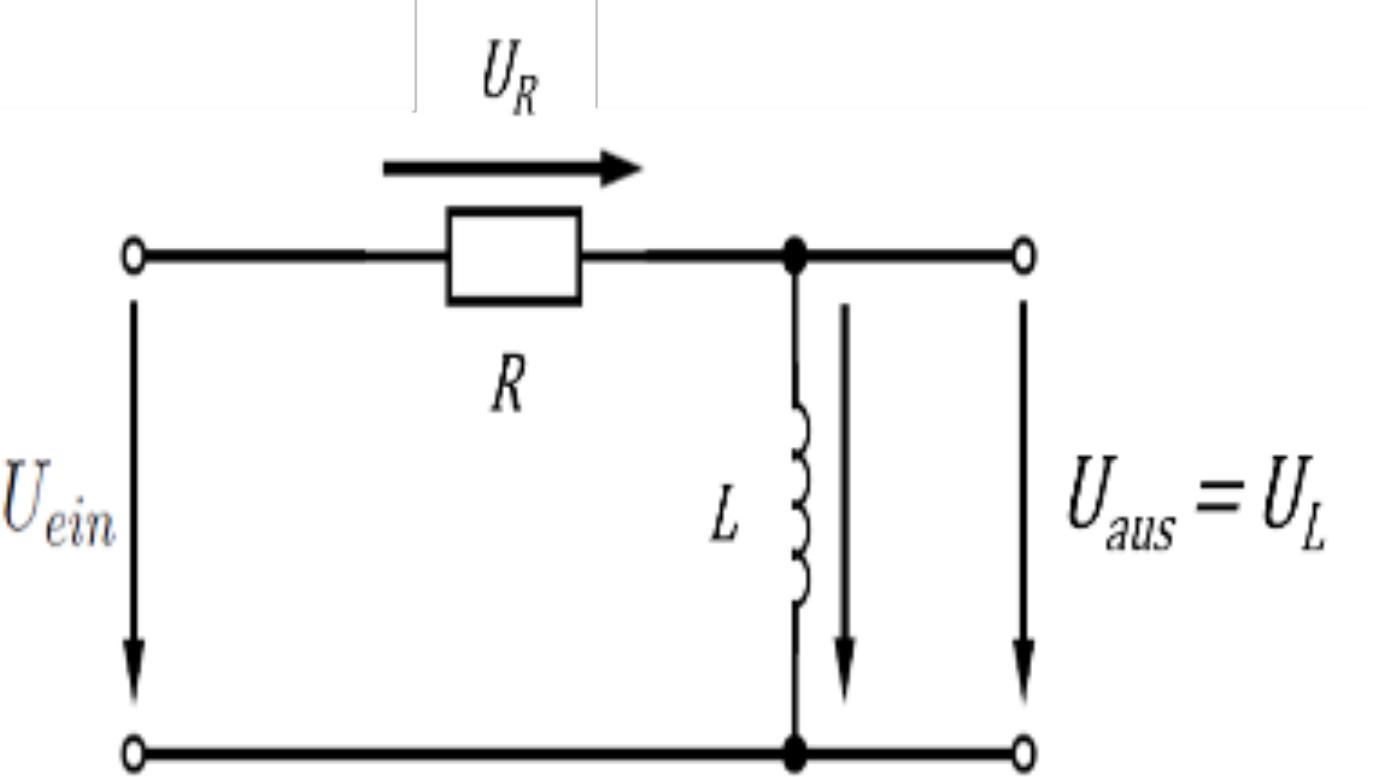
Chapter 2

Filters

In: Circuits with R, C, L

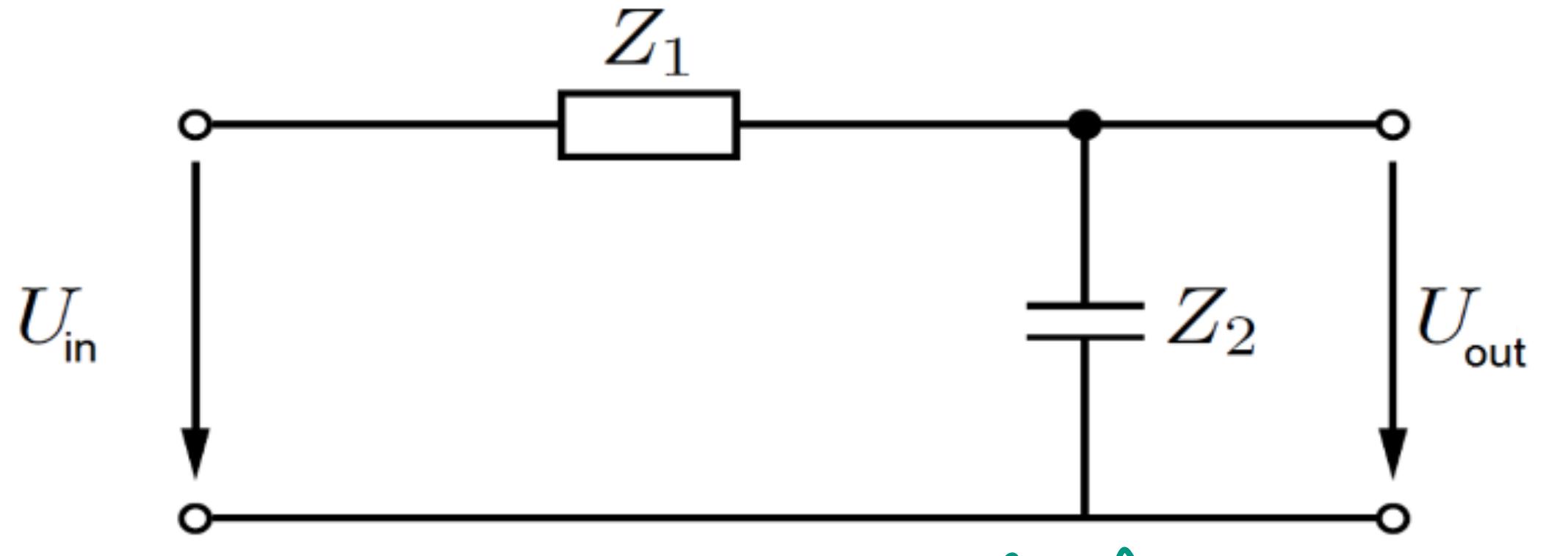
High- and Low Pass Filters

Reminder / Summary

Type	low pass	high pass
RC	 $U_{aus} = U_C$	 $U_{aus} = U_R$
RL	 $U_{out} = U_R$ (a)	 $U_{aus} = U_L$

Low Pass

Tiefpass



complex transfer function

$$\frac{\underline{U}_{\text{out}}}{\underline{U}_{\text{in}}} = \underline{Z} = \frac{\underline{Z}_2}{\underline{Z}_1 + \underline{Z}_2} = \frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + R} = \frac{1}{1 + j\omega RC} = \frac{1 - j\omega RC}{1 + (\omega RC)^2}$$

with $\underline{Z} = Z e^{j\varphi}$:

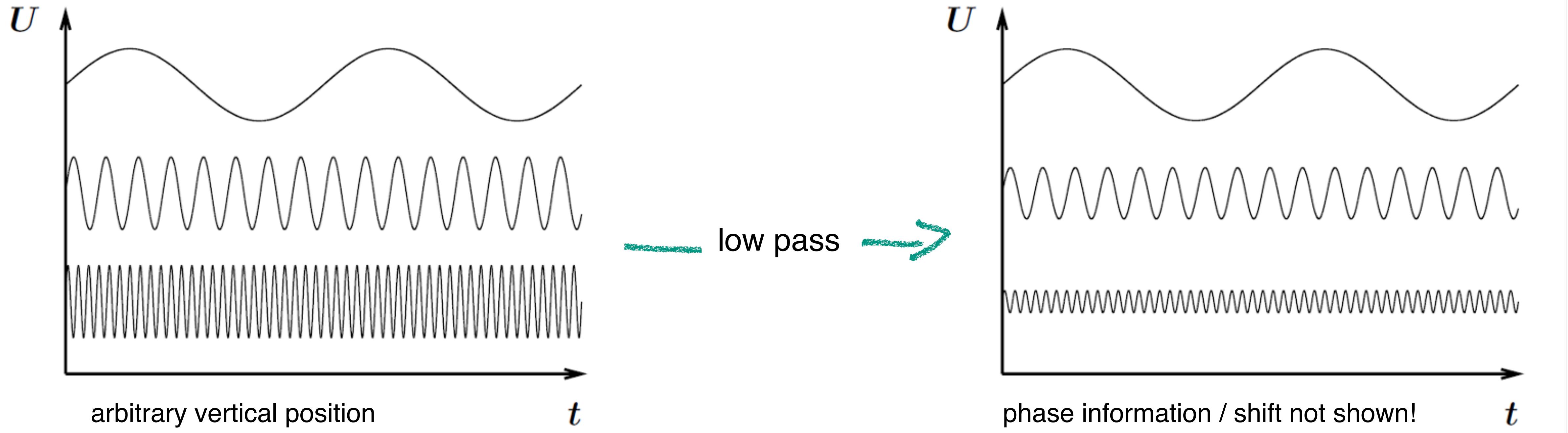
$$Z = \frac{1}{\sqrt{1 + (\omega RC)^2}} \quad \text{and} \quad \tan \varphi = \frac{\text{Im}(\underline{Z})}{\text{Re}(\underline{Z})} = -\omega RC$$

$Z \approx 1$ for $\omega \approx 0$

and $Z \approx 0$ for $\omega \gg 1/(RC)$

Low Pass

Impact on Signals

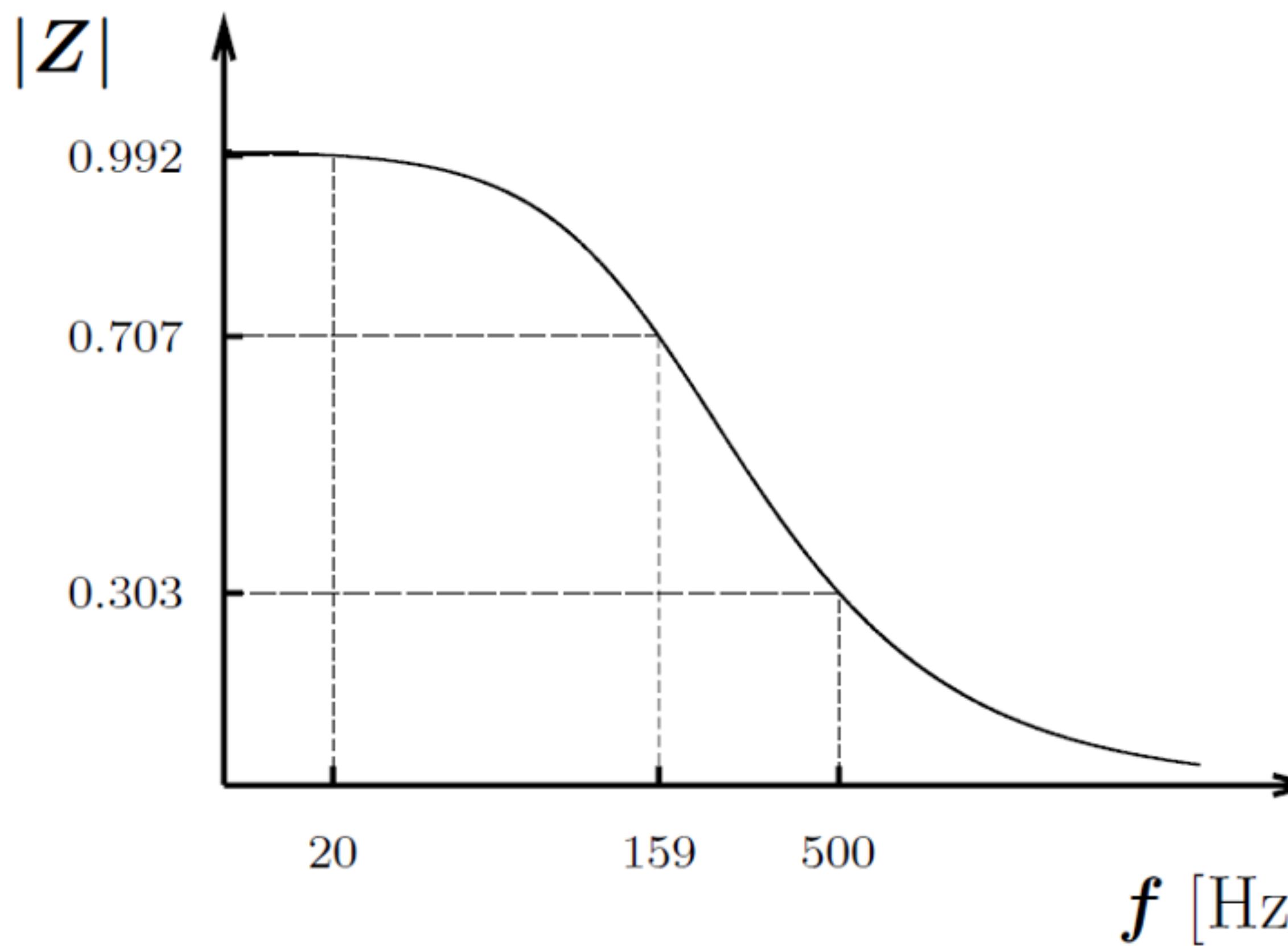


- Low frequency signals pass unchanged
- High frequency signals are damped
- For high frequencies the output signal is delayed in time with respect to the input signal

Low Pass

Frequency Dependence

- Amplitude of output signal depends on frequency.
- Phase depends on frequency.
- The frequency of input and output signal is identical.



$$Z = \frac{1}{\sqrt{1 + (\omega R C)^2}}$$

Brief Excursion: Decibel

Characterizing Filter Properties

Definitions: $10 \log \frac{P_{in}}{P_{out}}$ for power

$20 \log \frac{U_{in}}{U_{out}}$ or $20 \log \frac{I_{in}}{I_{out}}$ for current / voltage

dB	voltage ratio $20 \log \frac{U_{aus}}{U_{ein}}$	power ratio $10 \log \frac{P_{aus}}{P_{ein}}$
100	10^5	10^{10}
40	100	10^4
20	10	100
6,02	2	4
3,01	$\sqrt{2}$	2
0	1	1
-3,01	$\frac{1}{\sqrt{2}}$	$\frac{1}{2}$
-6,02	$\frac{1}{2}$	$\frac{1}{4}$
-20	0,1	10^{-2}
-40	0,01	10^{-4}
-100	10^{-5}	10^{-10}

NB: log = base 10 logarithm

Reminder:

$\log(ab) = \log(a) + \log(b)$:
dB values can be added!

Additional terms:

dBm: dB relative to 1 mW: $10 \log \frac{P[\text{W}]}{1 \text{ mW}}$

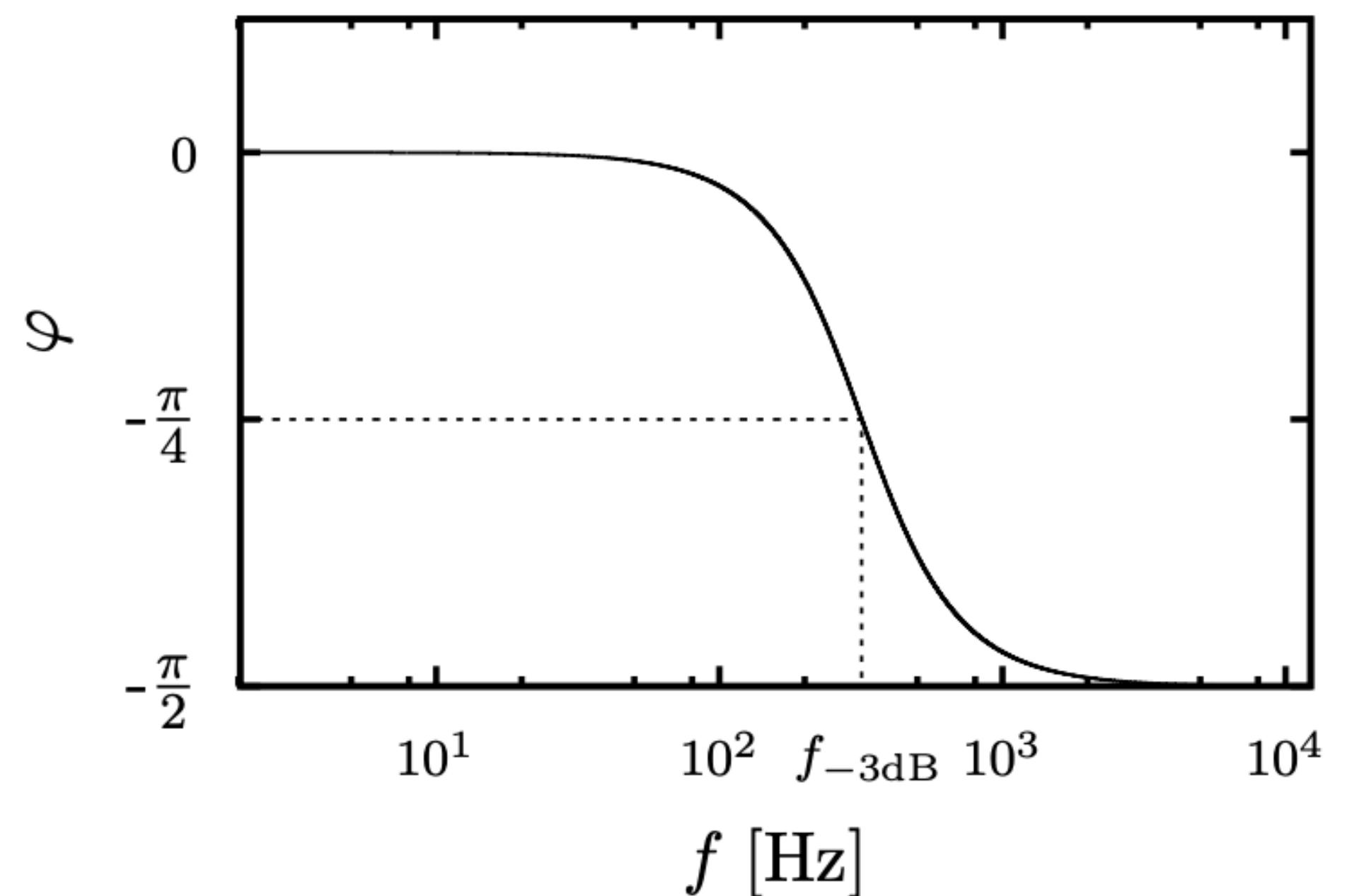
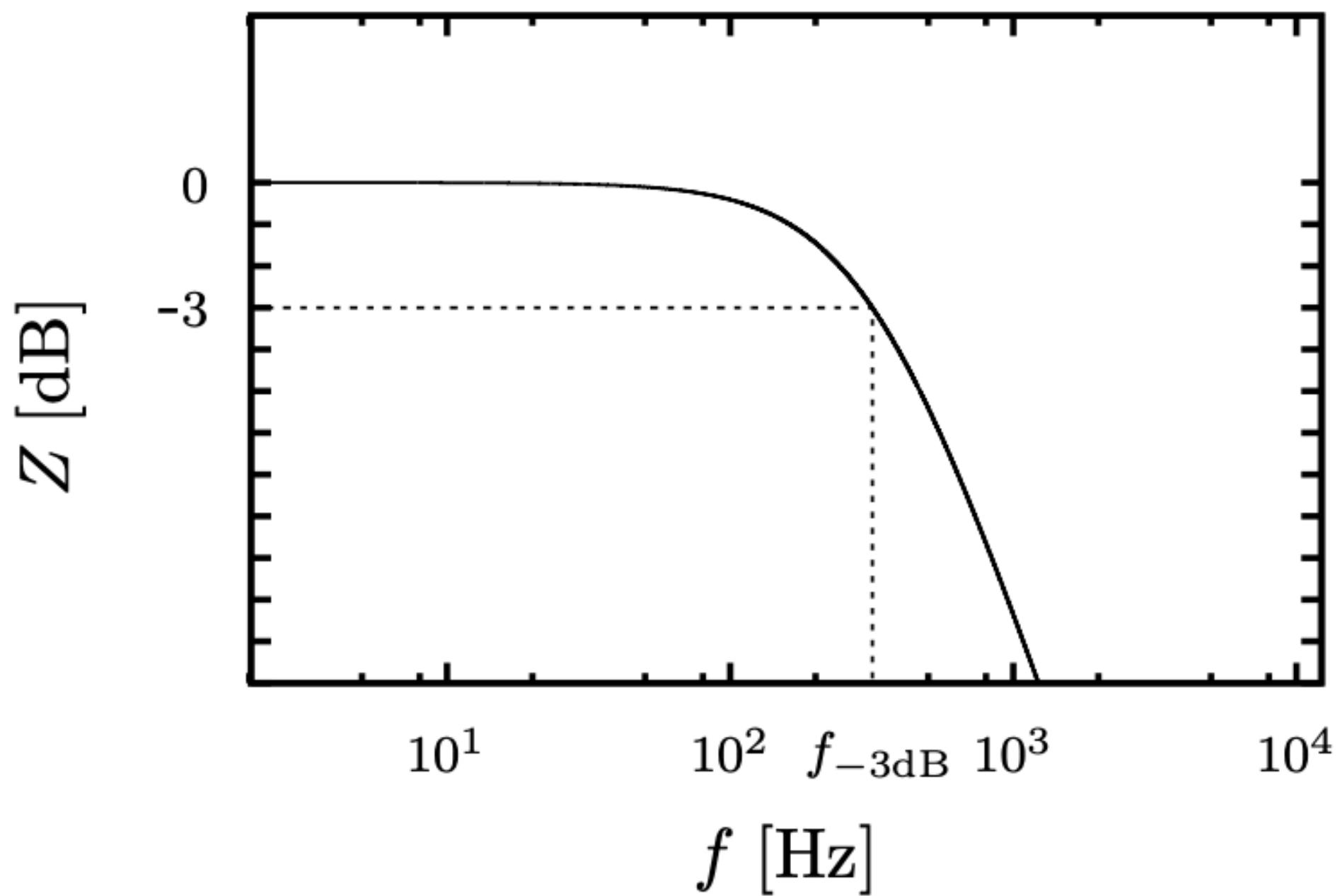
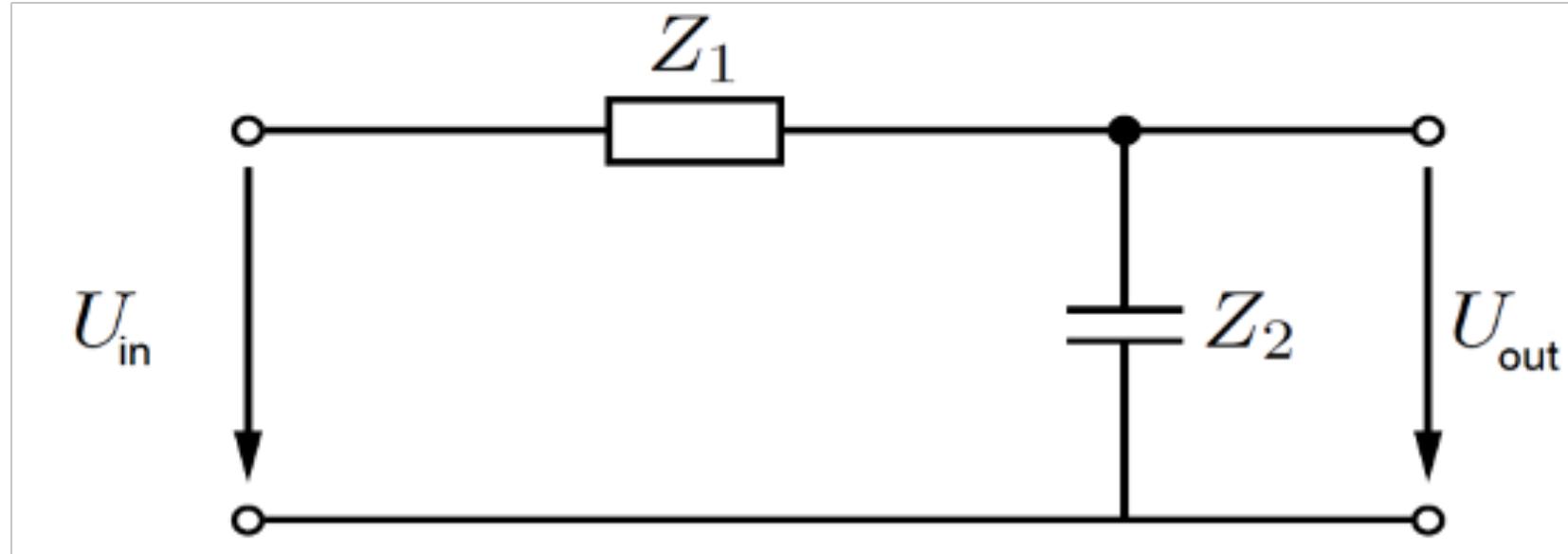
dBmA: dB relative to 1 mA: $20 \log \frac{I[\text{A}]}{1 \text{ mA}}$

Bode Plot: Introduction, Low Pass

Bodediagramm

- A commonly used representation of the transfer function (*komplexe Übertragungsfunktion*) $Z e^{j\varphi}$
- Two plots:
 - Amplitude of transfer function Z in dB vs $\log(f)$
 - Phase φ vs $\log(f)$

$$f = \frac{\omega}{2\pi}$$



$$Z = \frac{1}{\sqrt{1 + (\omega RC)^2}}$$

$$\tan \varphi = -\omega RC$$

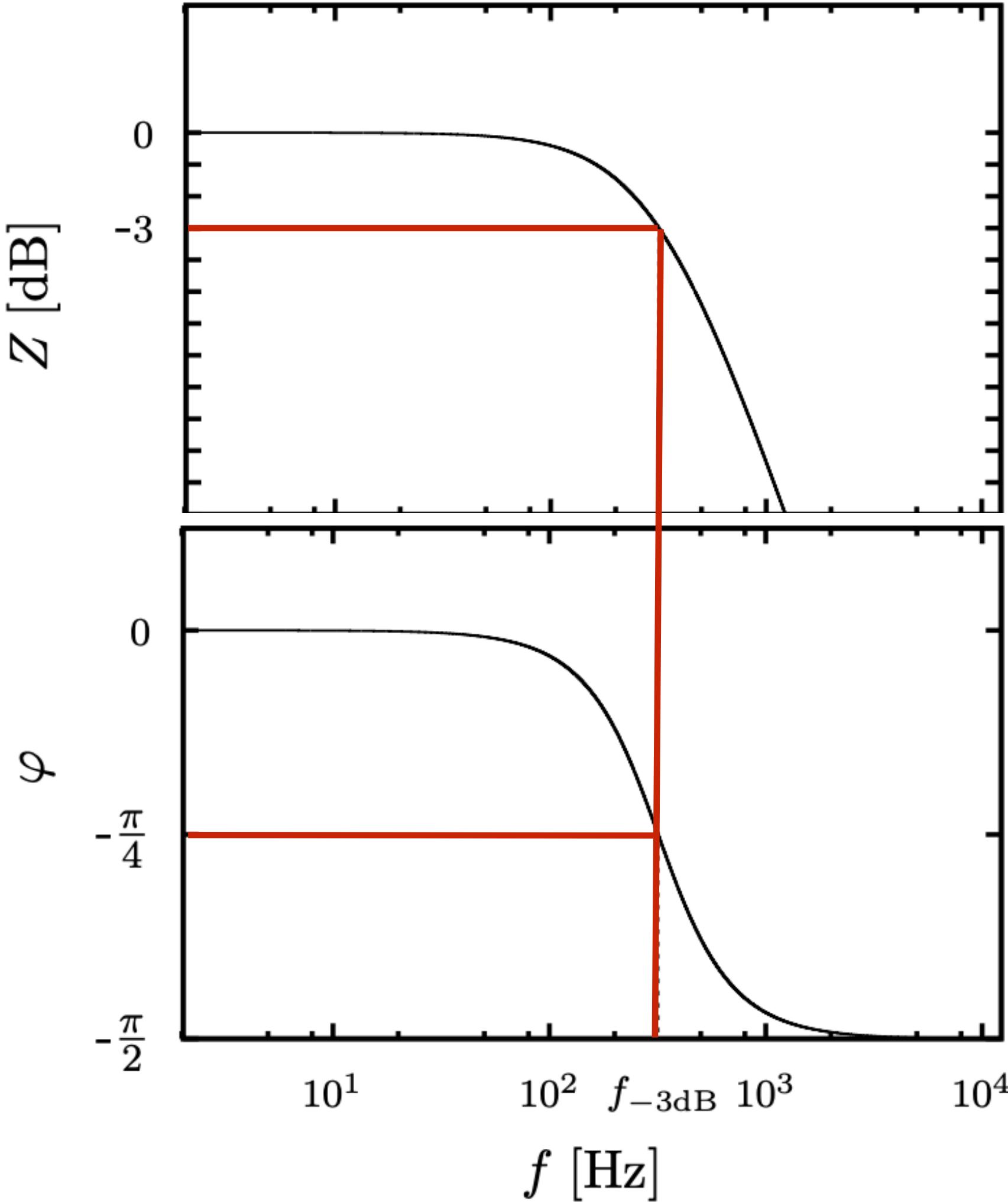
here:

$$R = 10 \text{ k}\Omega$$

$$C = 100 \text{ nF}$$

Bode Plot: Low Pass

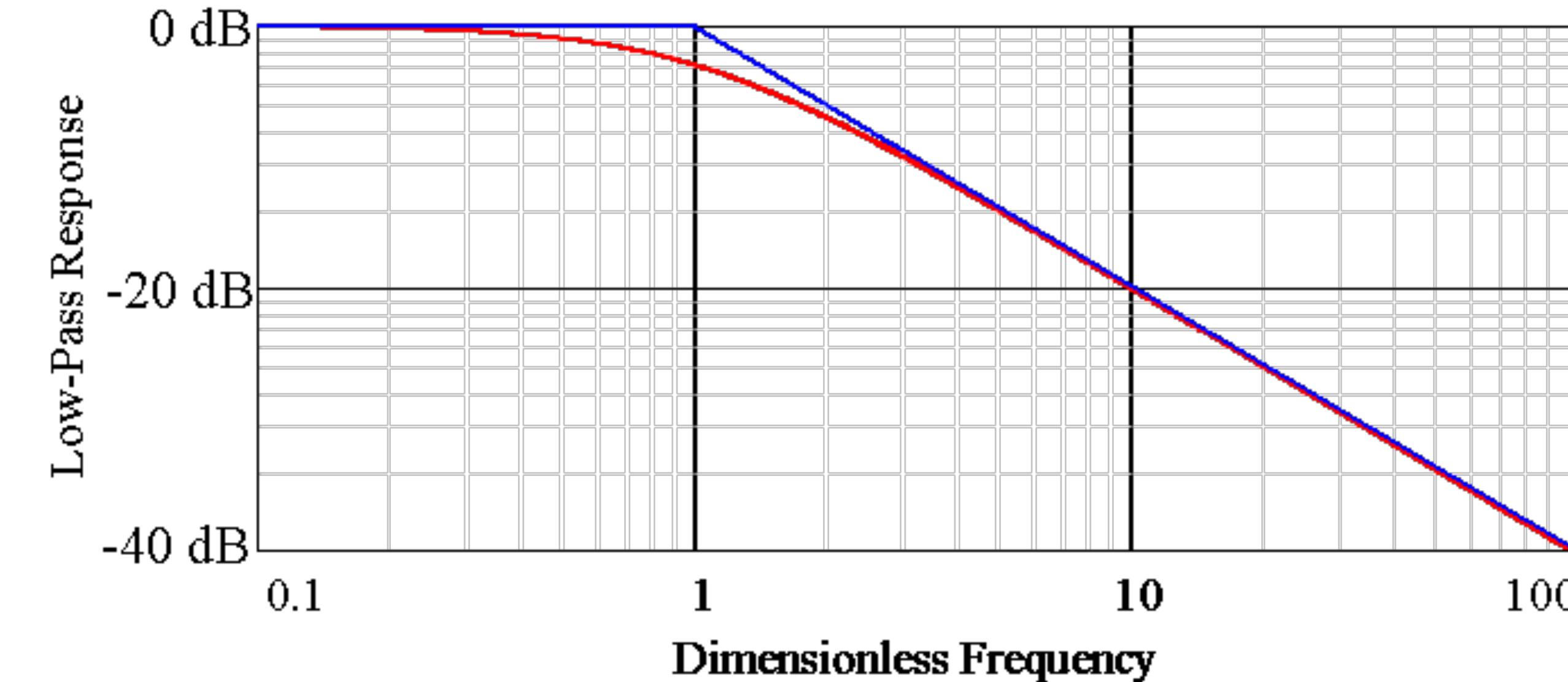
Closer Look



Cutoff frequency: Z has dropped by $1/\sqrt{2}$ (-3 dB)

$$f_{-3\text{ dB}} = \frac{1}{2\pi RC} \quad \omega_{-3\text{ dB}} = \frac{1}{RC}$$

Since $\tan \varphi = -\omega RC$: for critical frequency: -1; $\rightarrow \varphi = -\pi/4$



At high frequencies Z drops by 20 dB per frequency decade.
Corresponds to 6 dB / Octave (frequency doubling / halving)

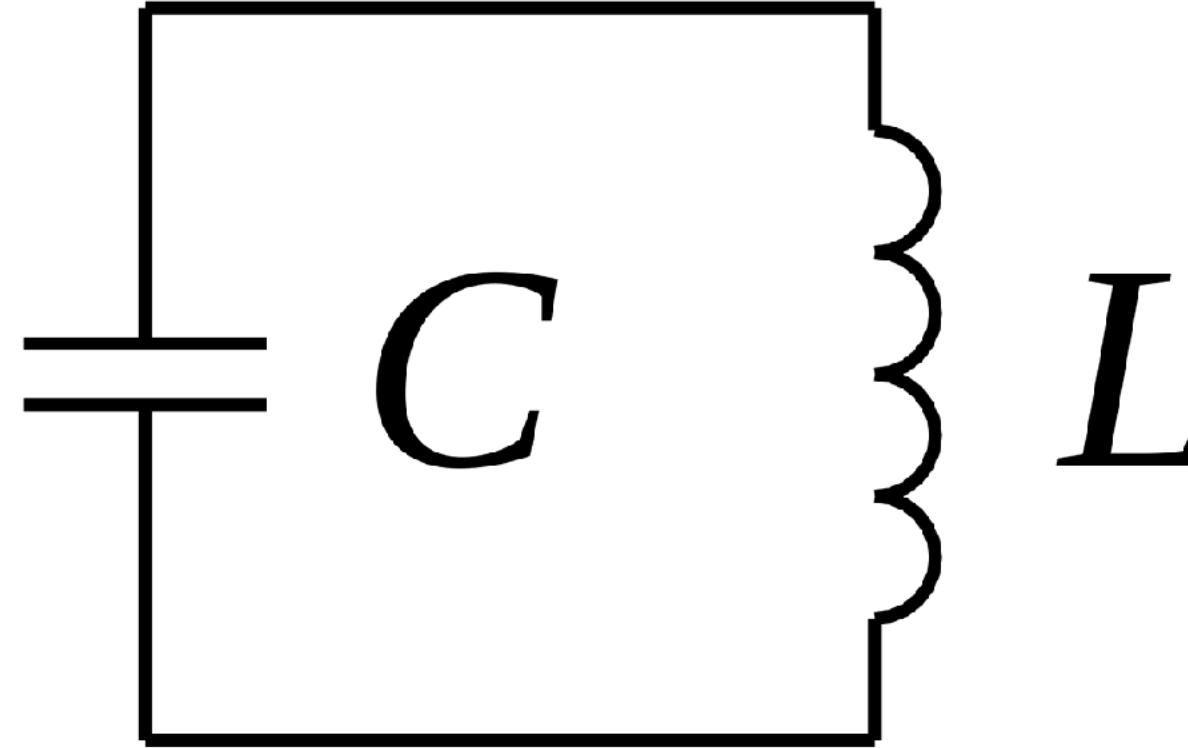
Chapter 2

Oscillators

In: Circuits with R, C, L

Oscillators - Introduction

Schwingkreise



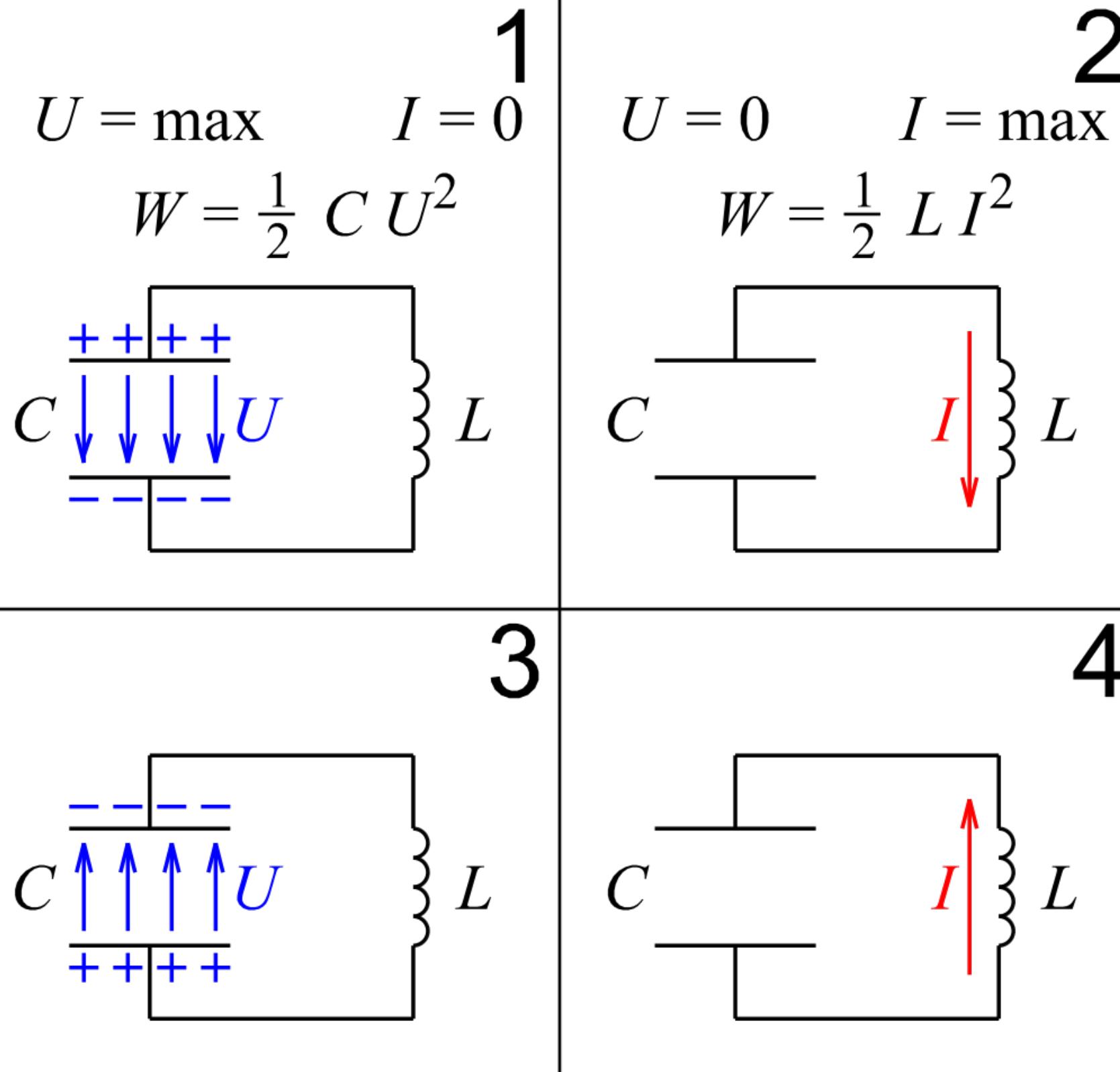
Resonance:

Z is maximal, the imaginary part of \underline{Z} is 0 (Phase $\phi = 0$)

$$\underline{Z} = \frac{1}{\frac{1}{Z_C} + \frac{1}{Z_L}} = \frac{1}{j\omega C - j\frac{1}{\omega L}}$$

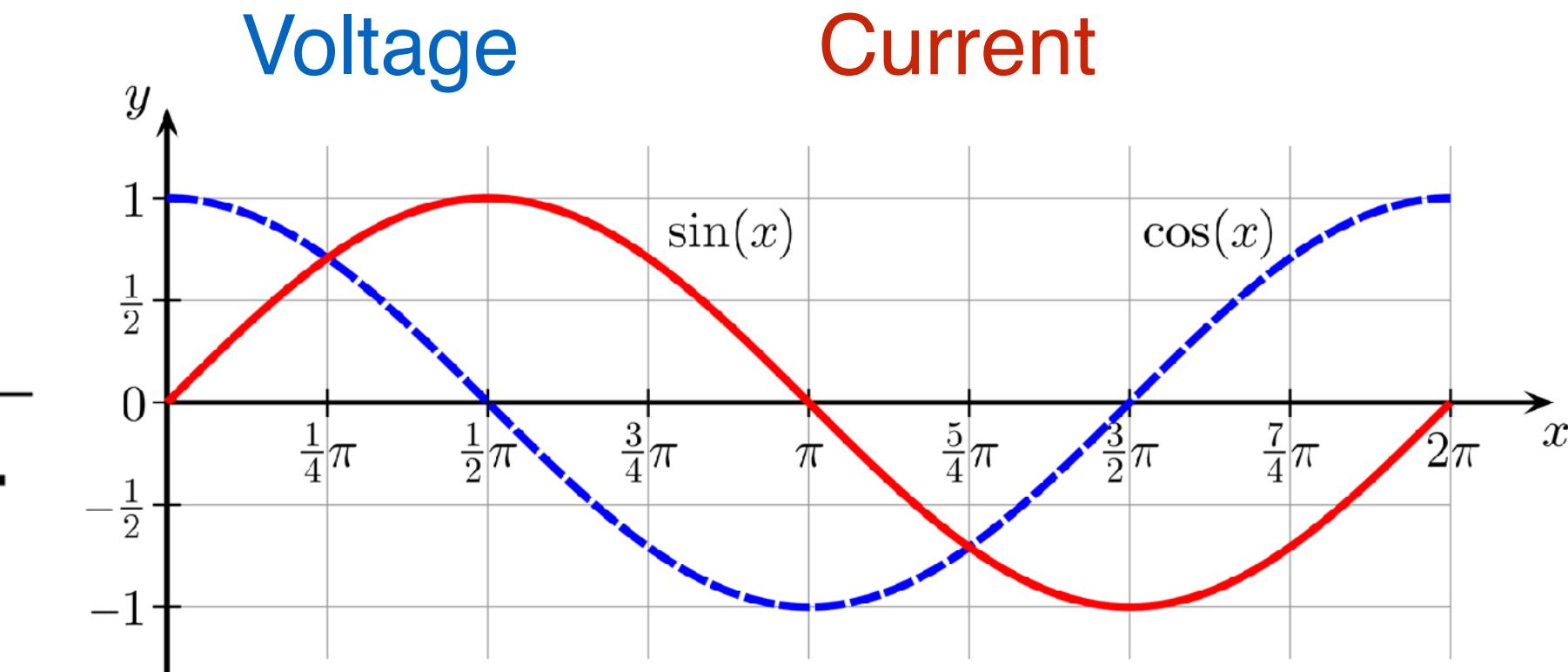
$$= \frac{-j\left(\omega C - \frac{1}{\omega L}\right)}{\left(\omega C - \frac{1}{\omega L}\right)^2}$$

\underline{Z} is real for



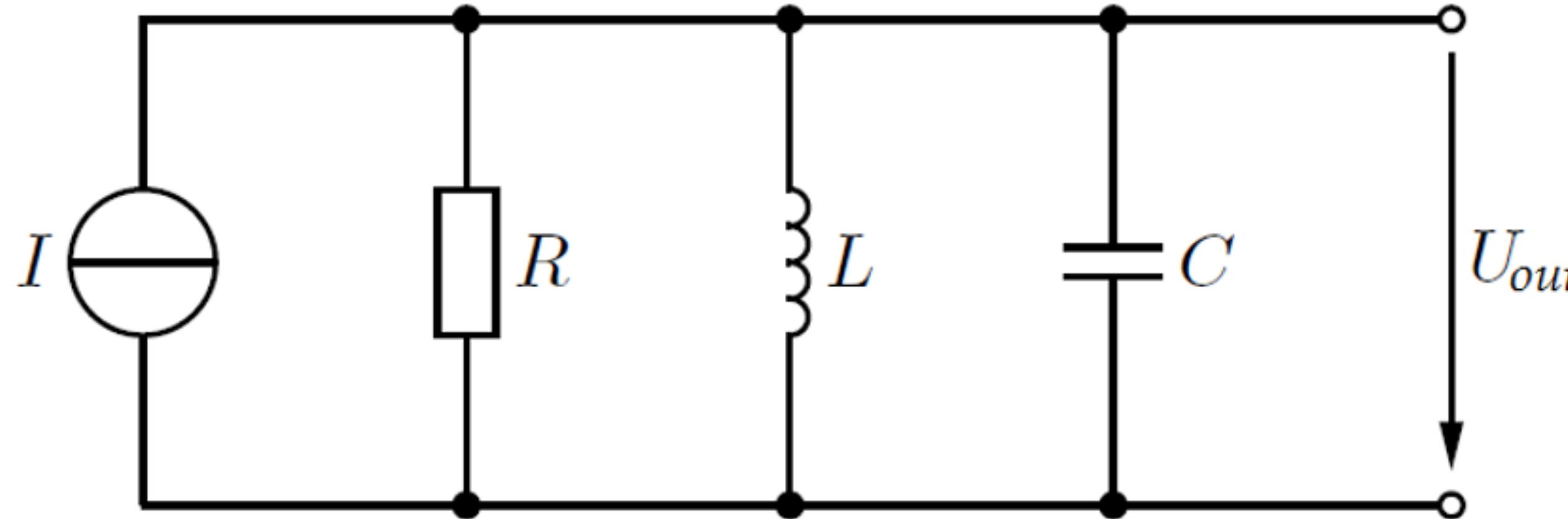
$$\omega C = \frac{1}{\omega L} \Rightarrow \omega_0 = \frac{1}{\sqrt{LC}}$$

resonance frequency



RLC Oscillator: Extension with Resistor

Schwingkreis



- Parallel oscillator with R:
 - “Driven” by current from current source

$$\underline{Z} = \frac{1}{\frac{1}{Z_R} + \frac{1}{Z_C} + \frac{1}{Z_L}} = \frac{1}{\frac{1}{R} + j\omega C - j\frac{1}{\omega L}} = \frac{\frac{1}{R} - j(\omega C - \frac{1}{\omega L})}{\frac{1}{R^2} + (\omega C - \frac{1}{\omega L})^2}$$

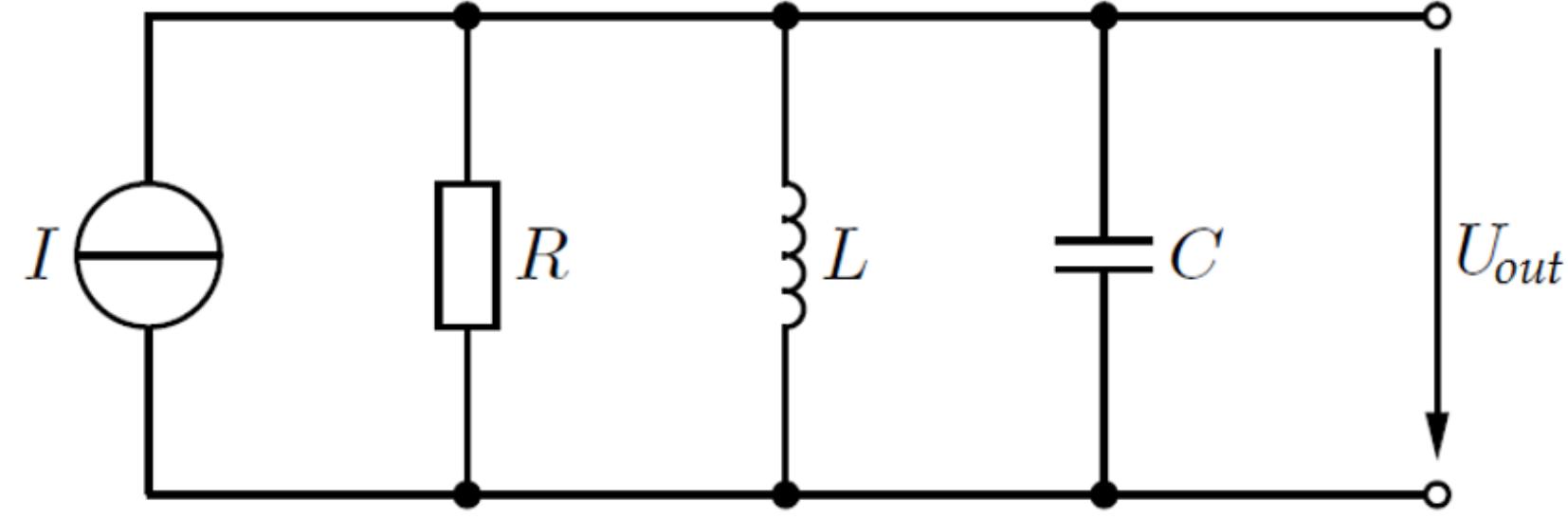
$$Z = \frac{1}{\sqrt{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2}}$$

$$\tan \varphi = \left(\frac{1}{\omega L} - \omega C \right) R$$

=> Resonance frequency identical to idealized pure LC circuit!

RLC Oscillator

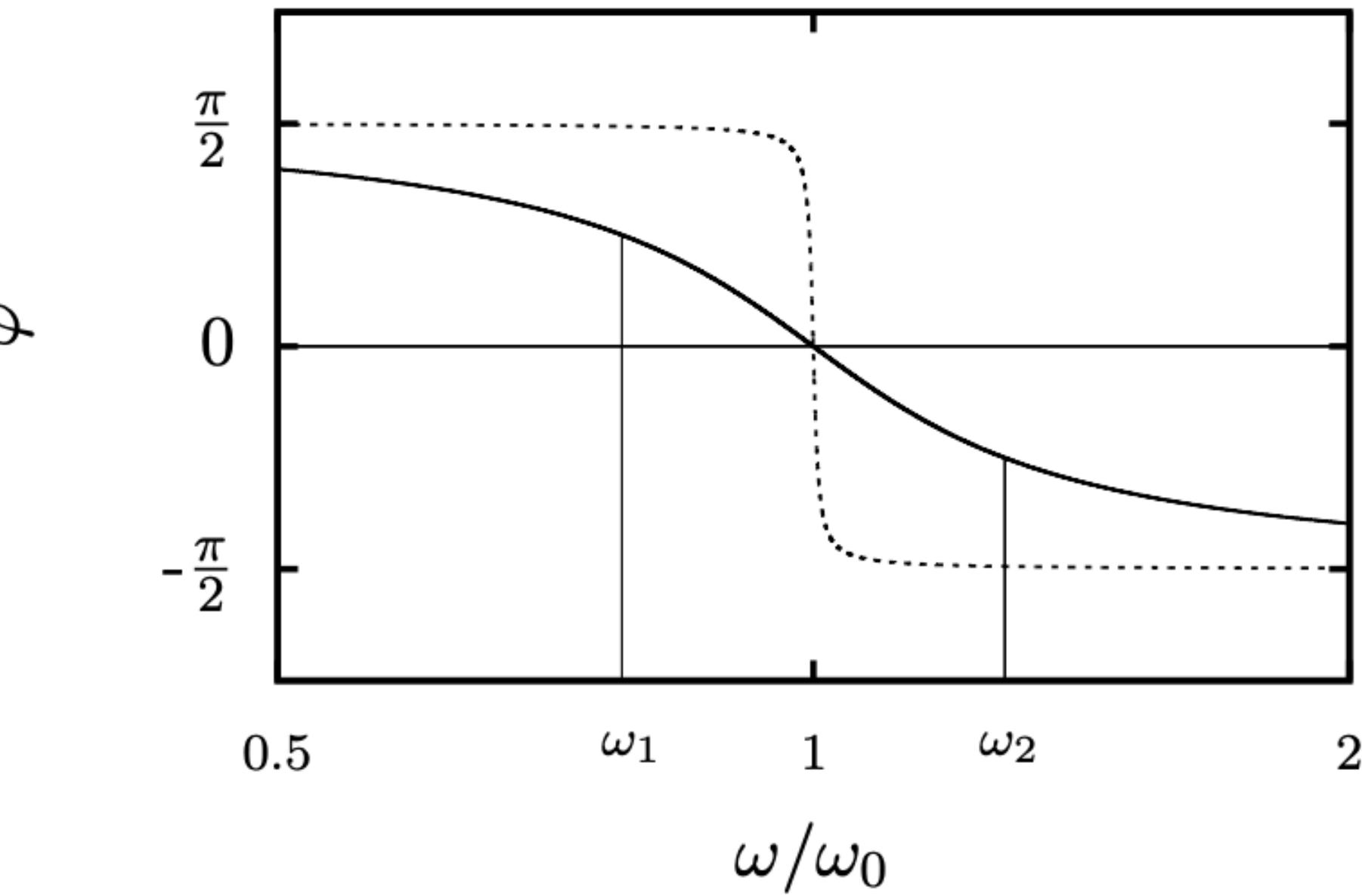
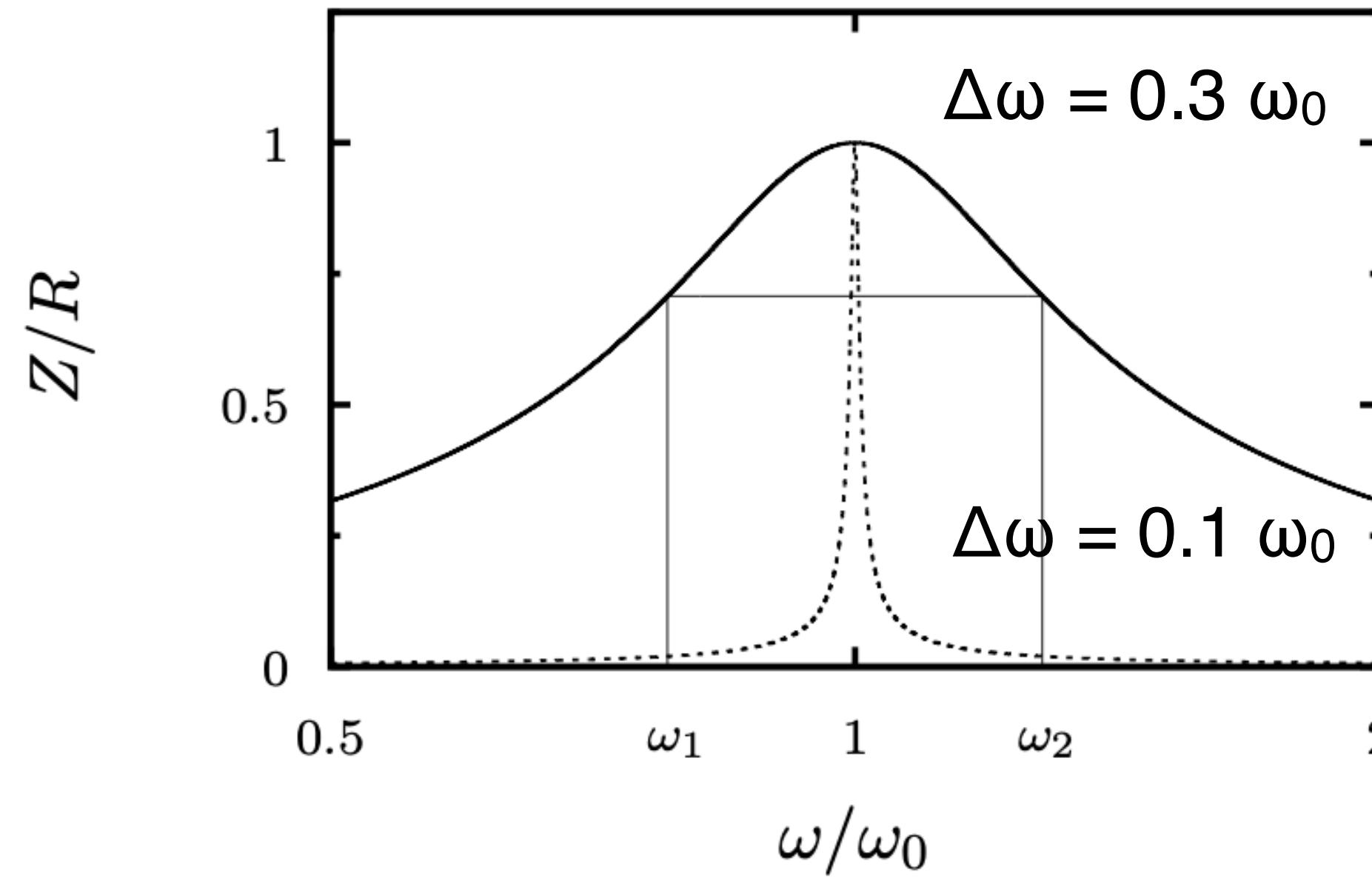
Behavior



Basic considerations:

- small output signal for very small and very large ω
- for small ω : Inductor shorts the circuit;
for large ω : Capacitor shorts the circuit

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

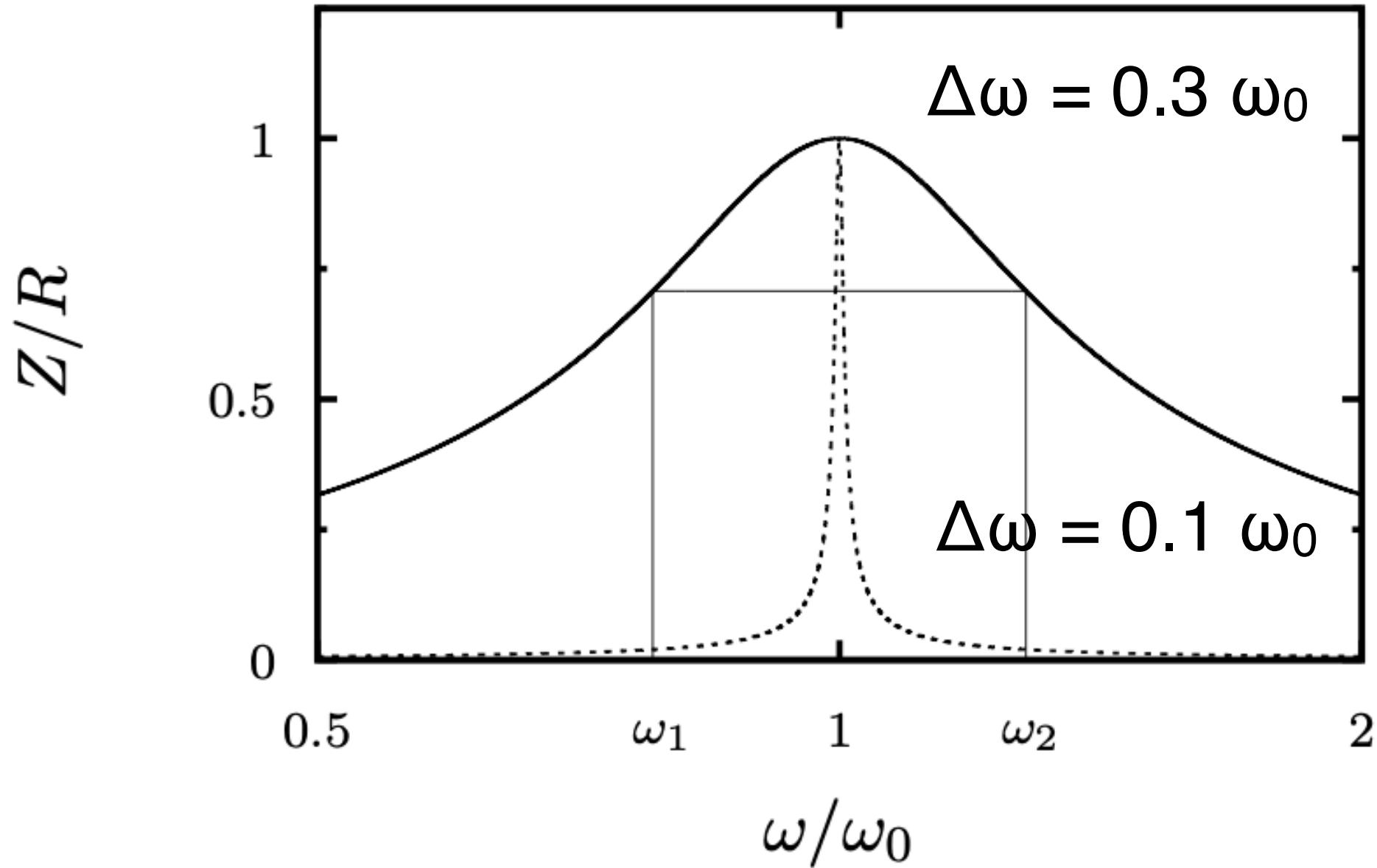


Precise behavior
as a function of ω
depends on R !

RLC Oscillator

Bandwidth and Q factor

- Crucial quantity: The bandwidth (*Bandbreite*)



$$\pm \left(\omega^2 - \frac{1}{LC} \right)^2 - \frac{\omega}{RC} = 0$$

Q factor ("Güte"):

$$Q = \frac{\omega_0}{\Delta\omega} = \frac{\omega_0}{\omega_2 - \omega_1}$$

positive solutions:

$$\omega_1 = -\frac{1}{2RC} + \sqrt{\frac{1}{(2LC)^2} + \frac{1}{LC}} \quad \omega_1 = \frac{1}{2RC} + \sqrt{\frac{1}{(2LC)^2} + \frac{1}{LC}}$$

here: $Q_P = \frac{RC}{\sqrt{LC}} = R\sqrt{\frac{C}{L}}$

bandwidth: $\Delta\omega = \omega_2 - \omega_1$; ω_1, ω_2 : amplitude $1/\sqrt{2}$ below maximum
(corresponds to a phase $\phi_{1,2} = \pm 45^\circ$)

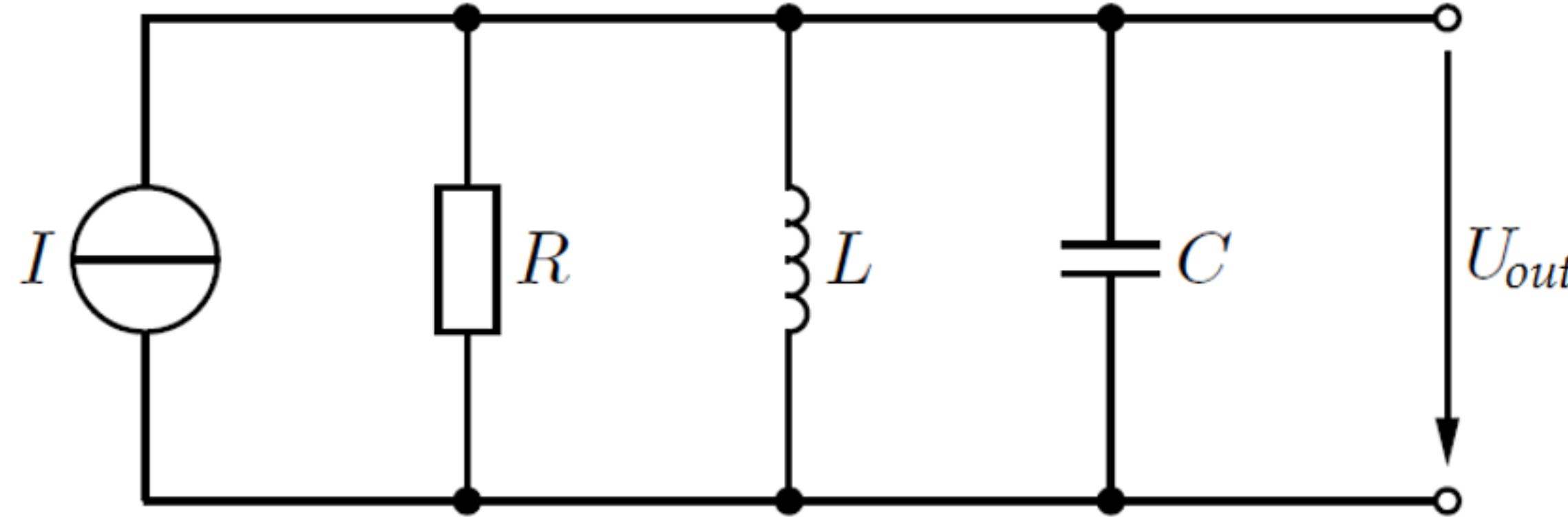
$$Z = \frac{1}{\sqrt{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L} \right)^2}}$$

Z maximal for ω_0 : $Z = R$

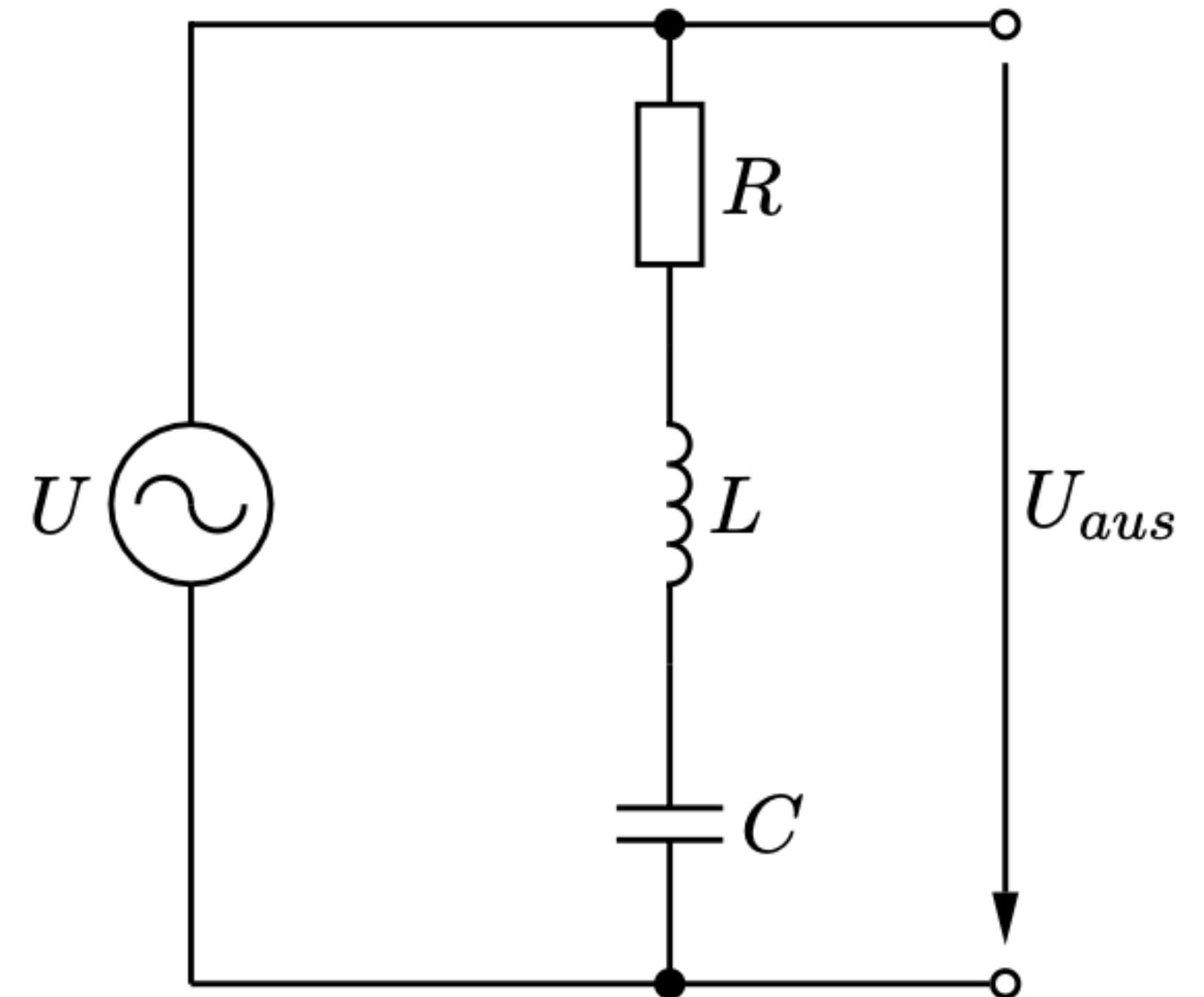
Results in: $Z_{1,2}$ for $\left(\omega C - \frac{1}{\omega L} \right)^2 = \frac{1}{R^2}$

RLC Oscillators: Compact Summary

Series and Parallel



Parallel



Series

	ω_0	$\Delta\omega$	Q
Series oscillator	$\frac{1}{\sqrt{LC}}$	$\frac{R}{L}$	$\frac{1}{R} \sqrt{\frac{L}{C}}$
Parallel oscillator	$\frac{1}{\sqrt{LC}}$	$\frac{1}{RC}$	$R \sqrt{\frac{C}{L}}$

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Chapter 3

Diodes

- Basic Properties
- Semiconductor Basics
- Diode Circuits - Examples

Overview

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Chapter 3.1

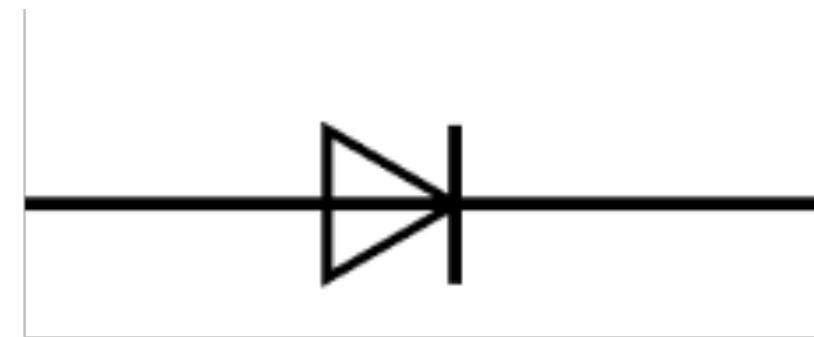
Basic Properties

In: Diodes

The Diode

Diode

- A passive, non-linear component.



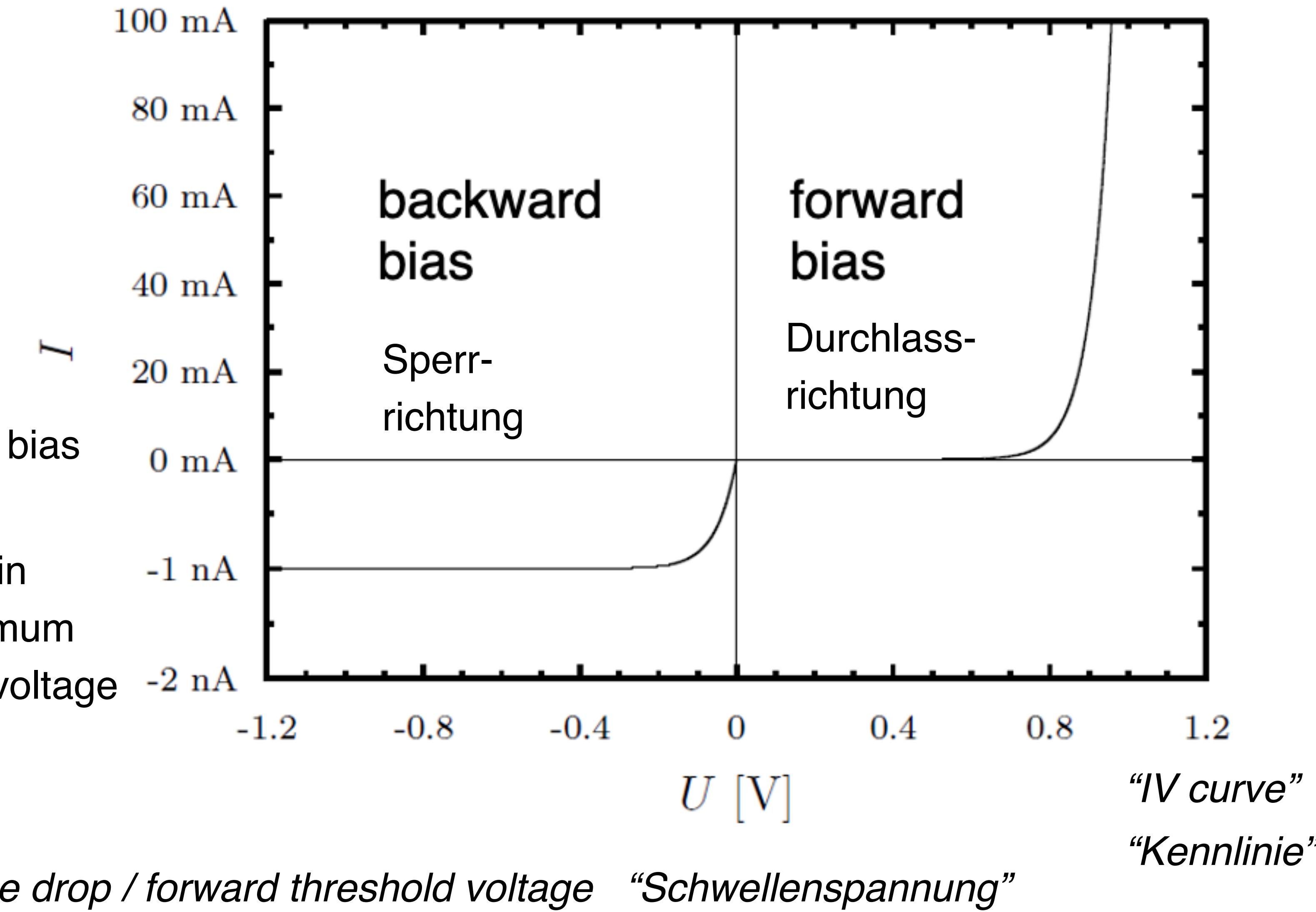
Basic behavior:

Large current for forward bias.

Minimum leakage current for reverse bias

For a constant, not too small current in forward direction ($\sim 10\%$ of the maximum current of the component) there is a voltage drop of U_s over the diode, (almost) independent of the current.

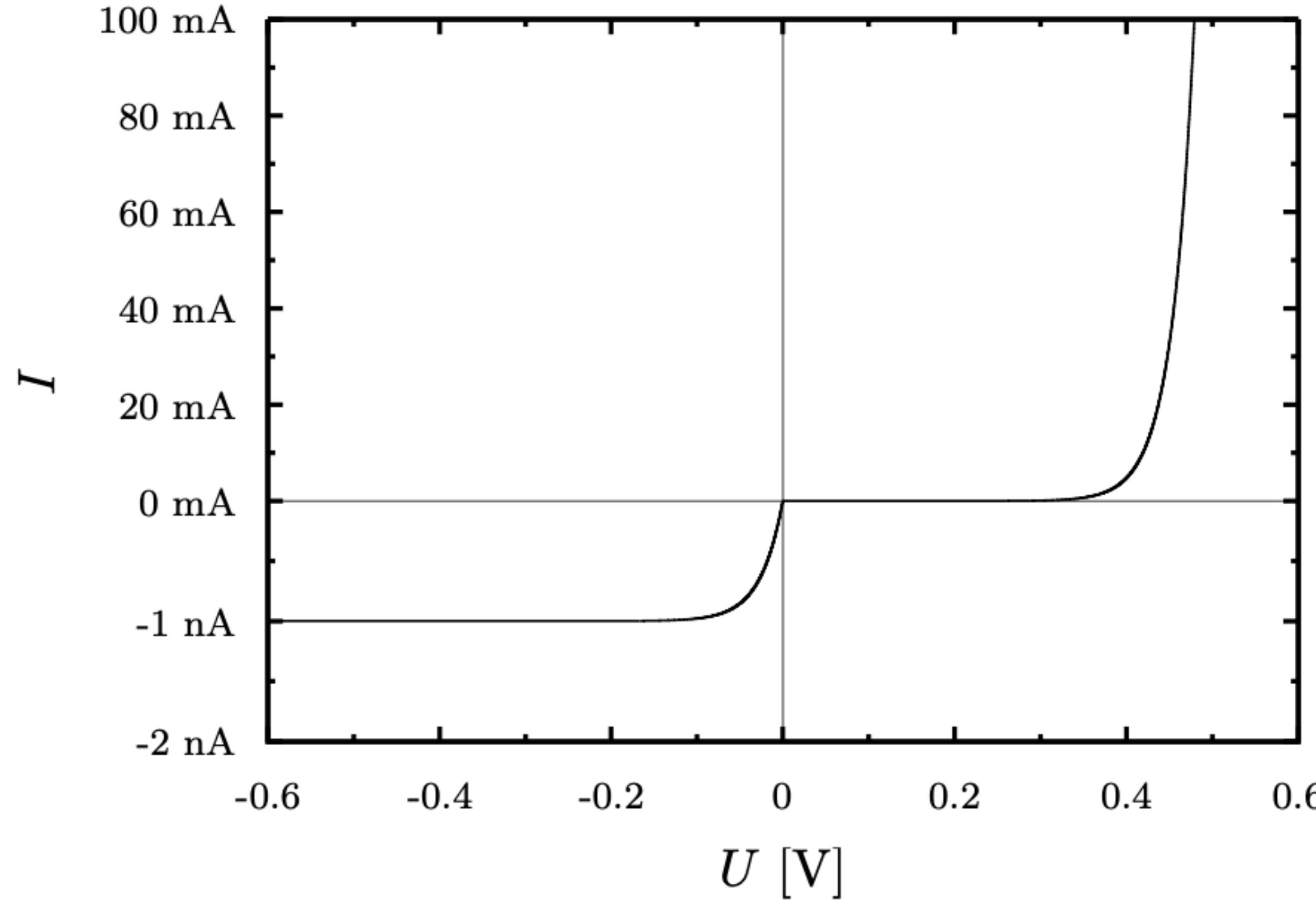
For Si diodes: $U_s \sim 0.7 \text{ V}$



Behavior of Diodes

Shockley Diode Equation

- Description of the IV Curve of a Diode: **Shockley diode equation**



$$I = I_S \left[e^{\frac{q_e U}{k T}} - 1 \right] = I_S \left[e^{\frac{U}{U_T}} - 1 \right]$$

I_S : reverse bias saturation current “Sperrstrom”
(often also “leakage current”)

$$\frac{k T}{q_e} = U_T \quad \rightarrow \sim 26 \text{ mV at } 300 \text{ K}$$

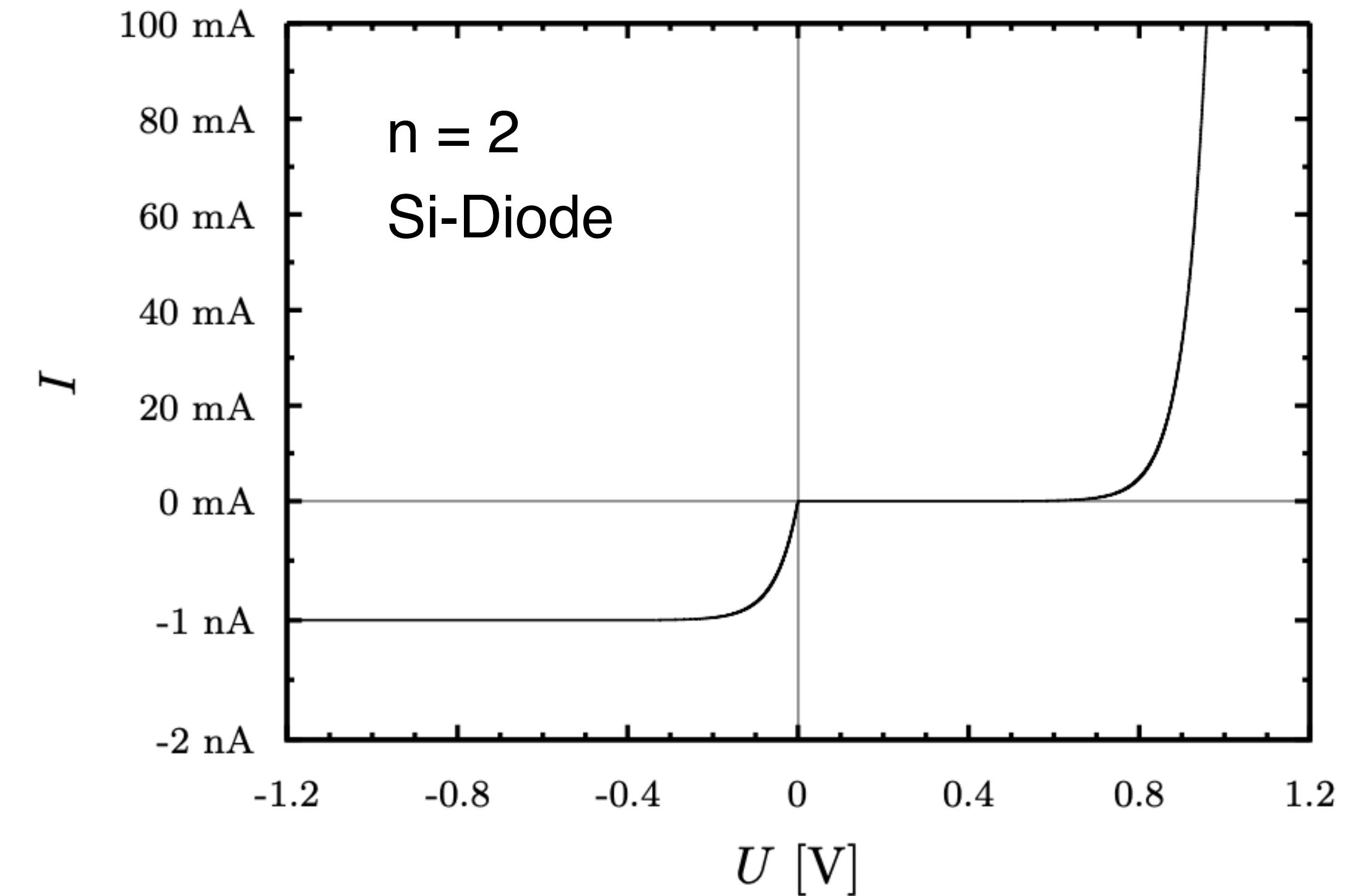
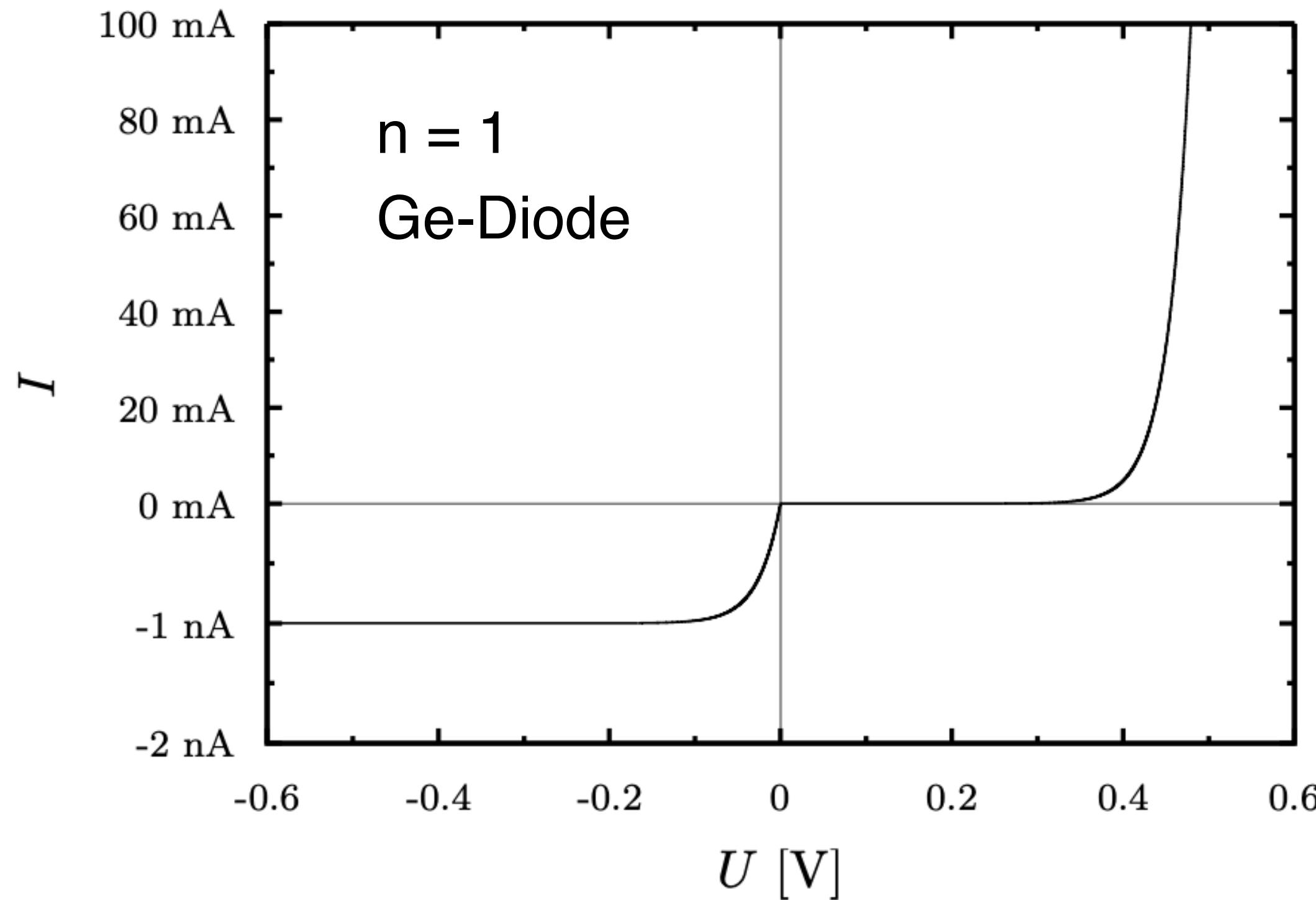
k : Boltzmann constant
 q_e : elementary charge

Behavior of Diodes

Extension of the Shockley Equation

- Depending on material diodes show different behavior:
Cannot be described by the simple Shockley equation.

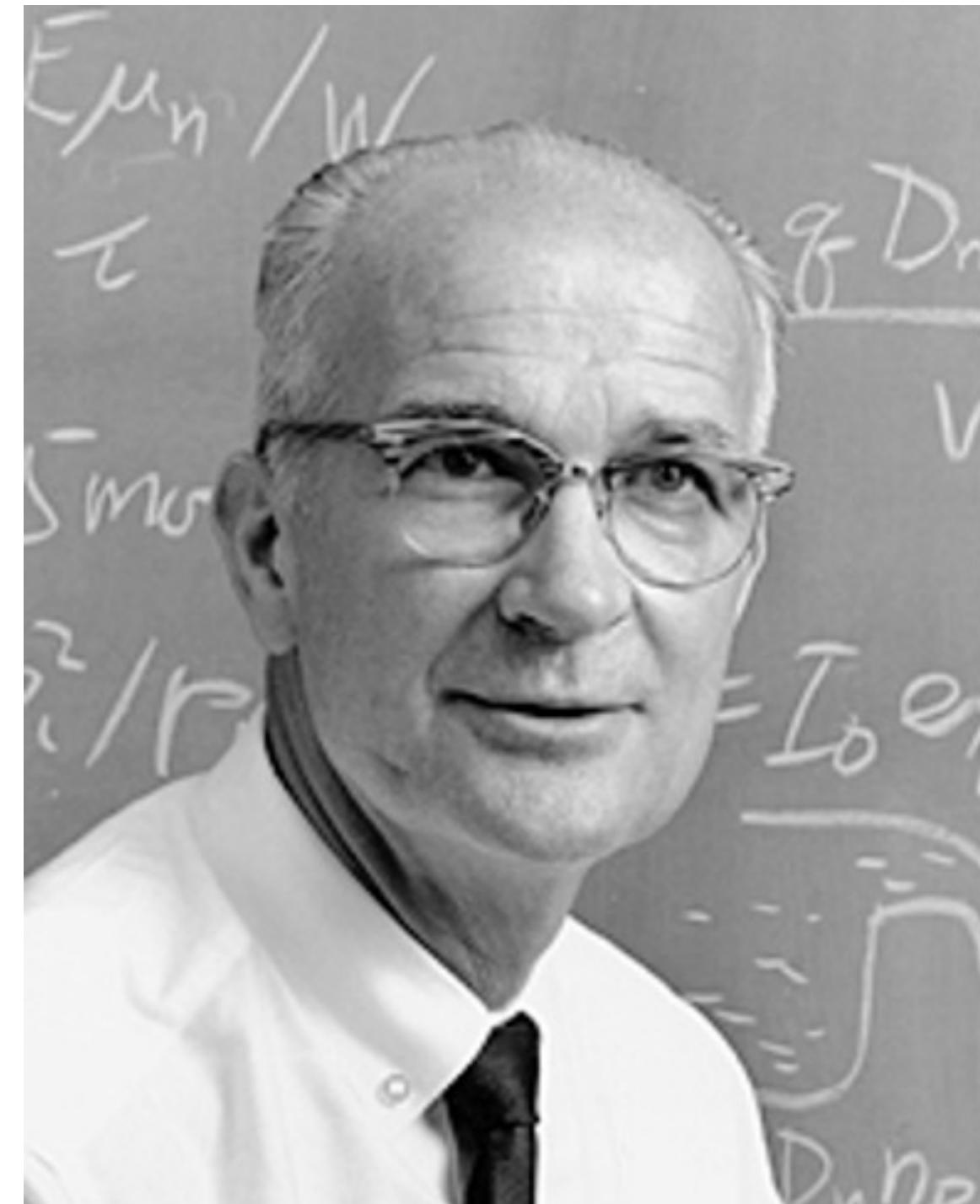
$$I = I_S \left[e^{\frac{q_e U}{kT}} - 1 \right] = I_S \left[e^{\frac{U}{U_T}} - 1 \right] \Rightarrow I = I_S \left[e^{\frac{U}{nU_T}} - 1 \right] \quad n = 1 \dots 2$$



Historical Perspective

William B. Shockley

- Physicist and electrical engineer
- Nobel Prize in physics 1956 (together with Bardeen, Brattain)
“for their researches on semiconductors and their discovery of the transistor effect”



One of the “founders” of Silicon Valley
(but also a very controversial person)

Chapter 3.2

Semiconductor Basics

In: Diodes

Semiconductors

Halbleiter

- The basis for diodes (and transistors,...): semiconductors.
Characterized by a (small) band gap between the (filled) valence and (empty) conduction band.
Electrons move from valence into the conduction band via thermal excitation -> “holes” in valence band.

Semiconductors: Elements of the IV main group: Si, Ge, C (as diamond); but also compounds:
GaN, GaN, SiC, HgCdTe, CdZnTe, ...

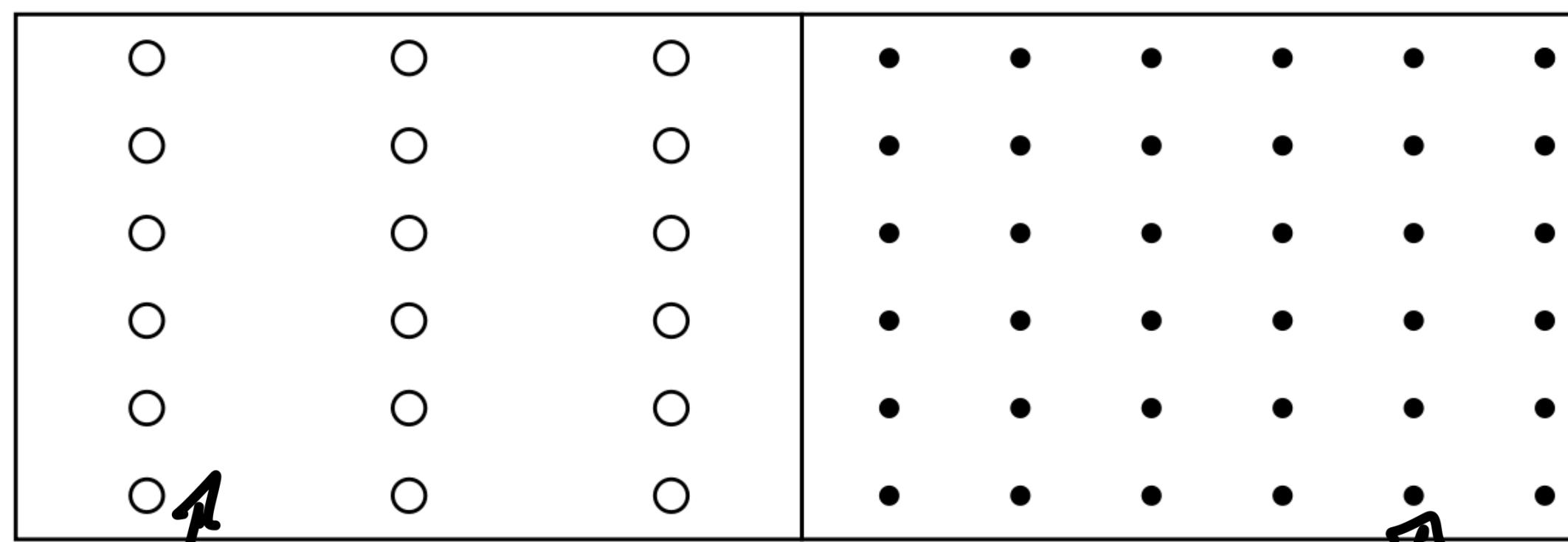
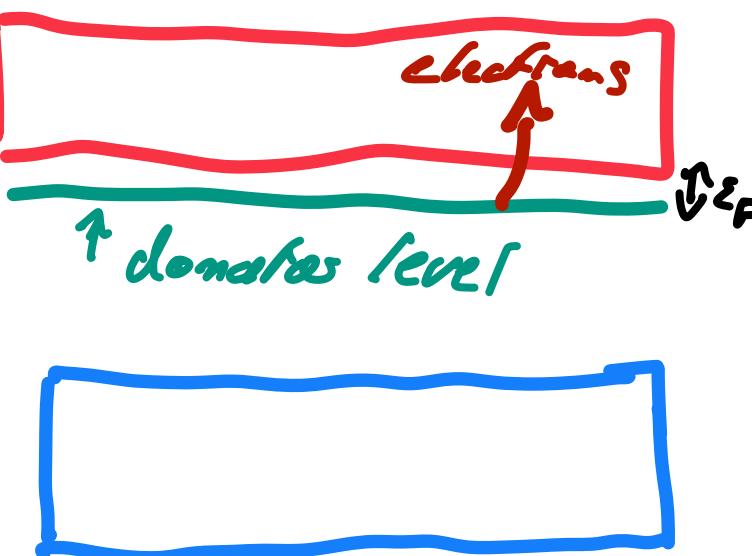
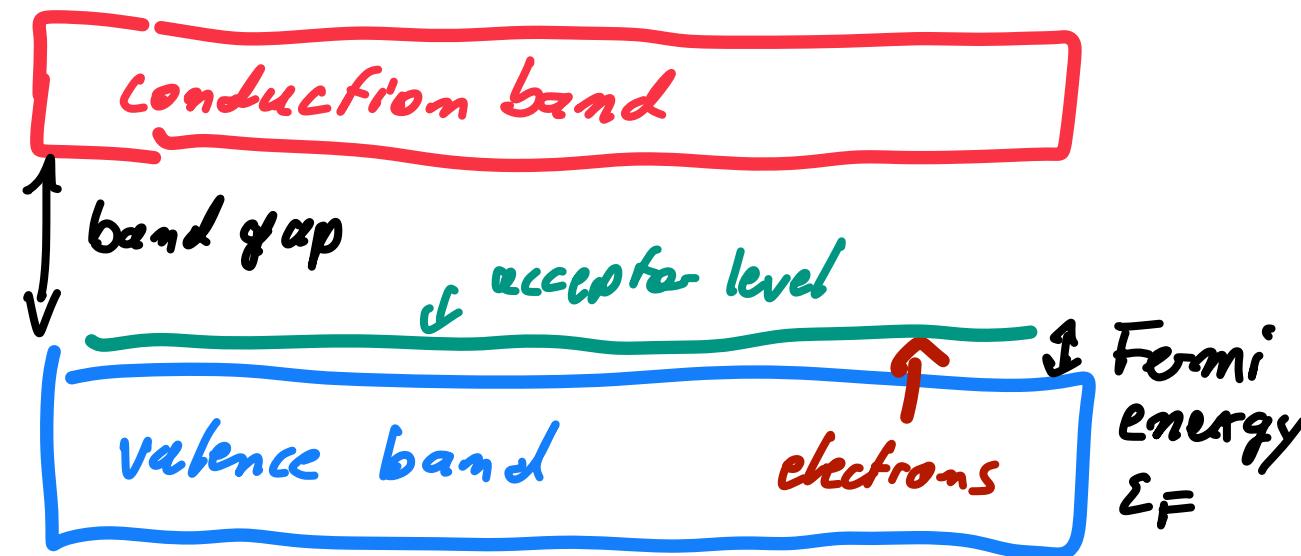
Typical values at room temperature

	Si	Ge	GaAs	Diamond	GaN
Band gap	E_G [eV]	1, 12	0, 67	1, 42	5, 5
Intrinsic charge density (due to thermal excitation)	n_i [cm^{-3}]	$1, 1 \cdot 10^{10}$	$2, 4 \cdot 10^{13}$	$1, 8 \cdot 10^6$	2×10^{-10}

Doping, PN Junctions

Dotierte Halbleiter und PN-Übergänge

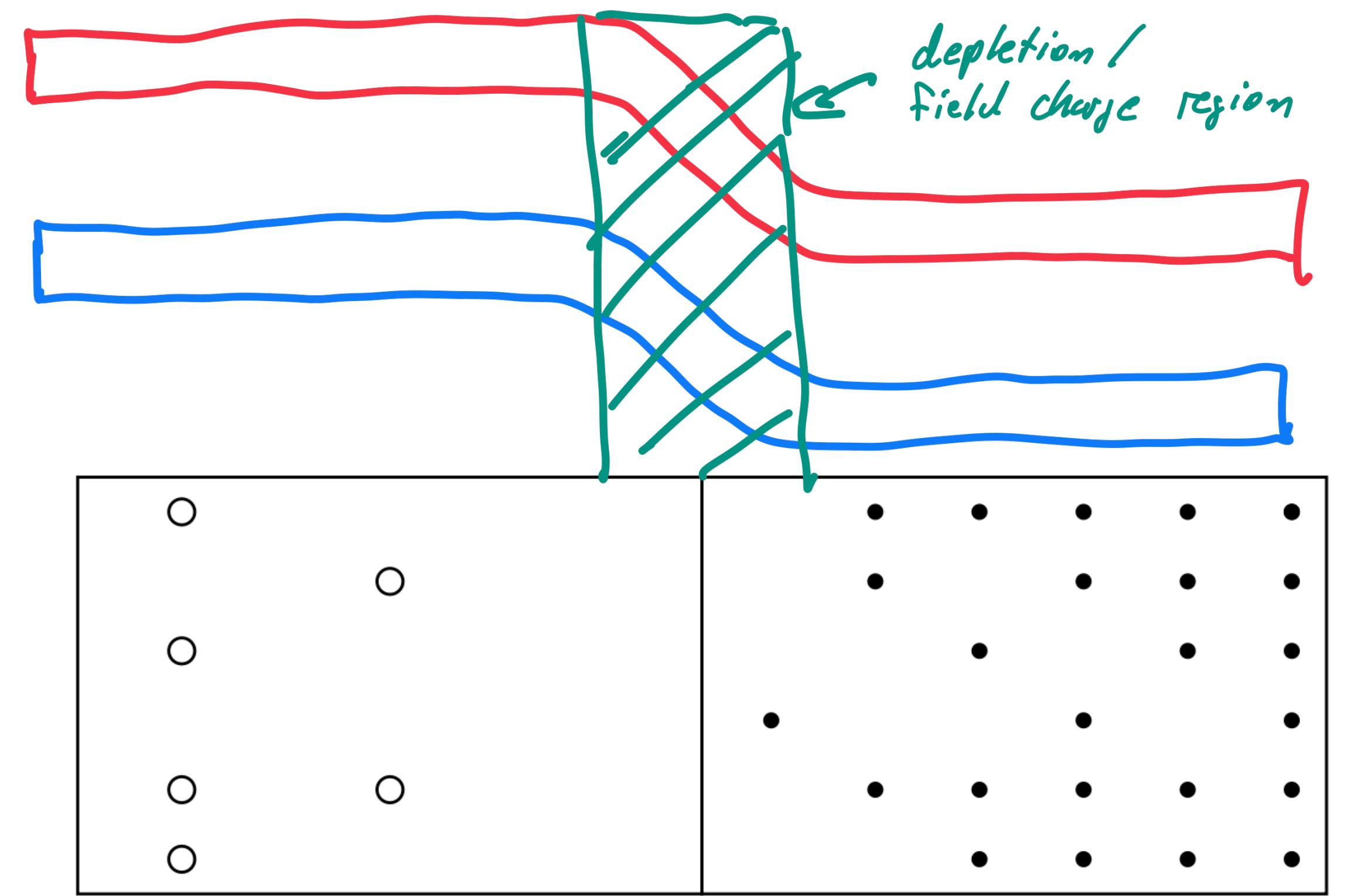
- Doping: Providing additional electrons (V main group, such as P ($Z=15$), n-type doping) or holes (III main group, such as B ($Z = 5$), p-type doping).



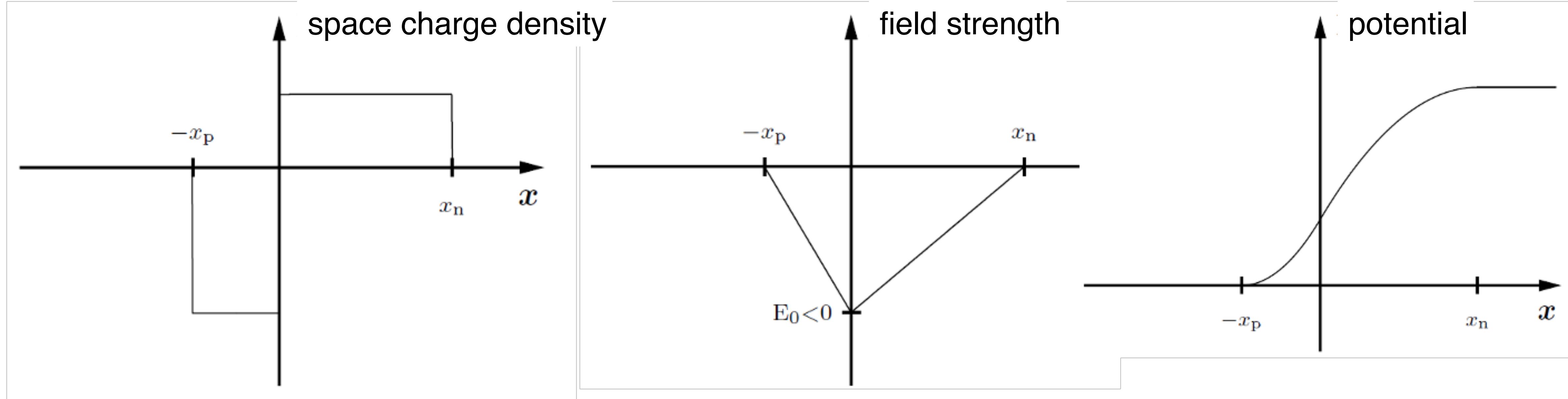
p-doping: excess holes

n-doping: excess electrons

Increases the charge carrier density by several orders of magnitude



Electric Fields in Diodes

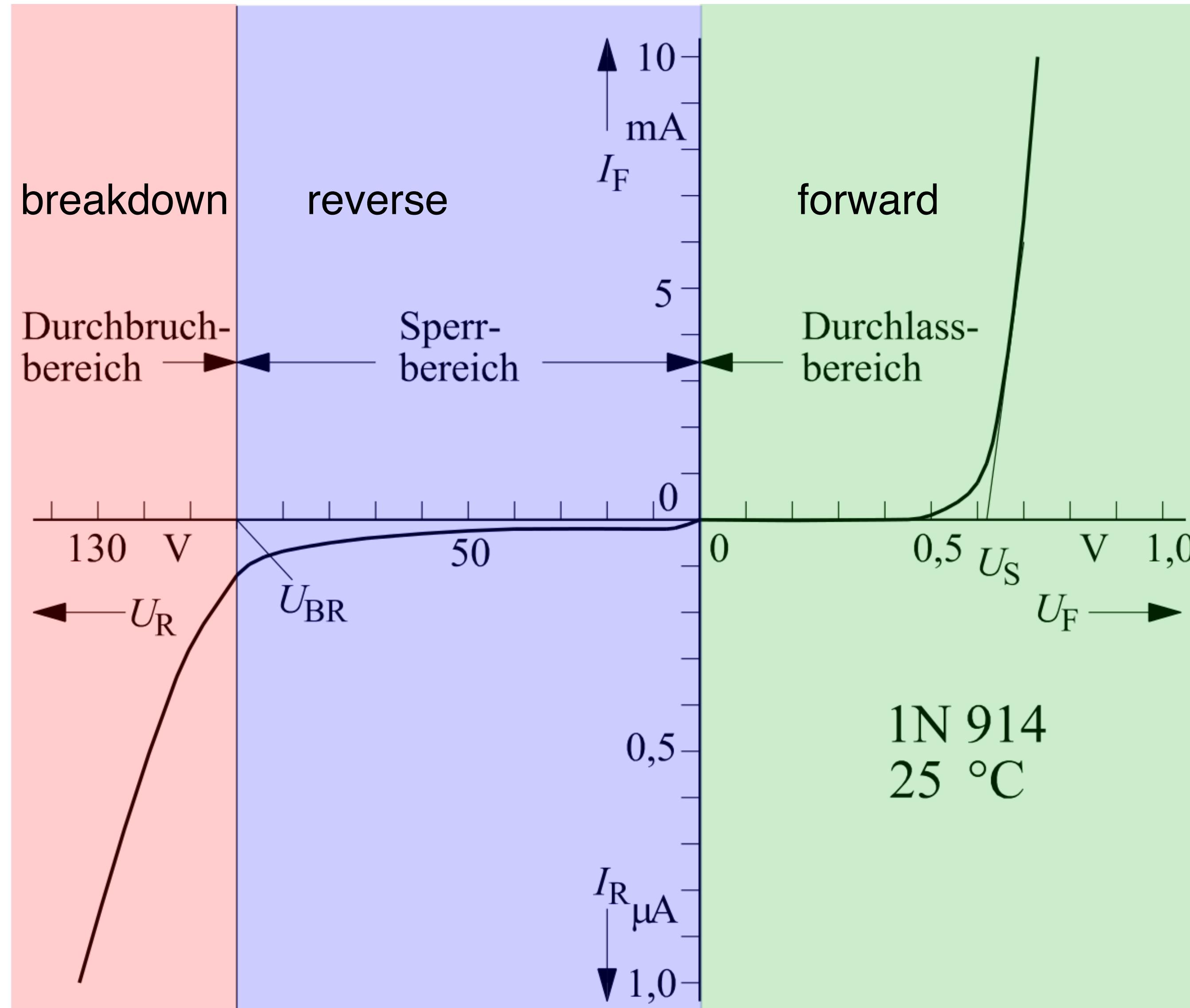


◦	◦	◦	◦	◦	◦	◦
◦	◦	◦	◦	◦	◦	◦
◦	◦	◦	◦	◦	◦	◦
◦	◦	◦	◦	◦	◦	◦
◦	◦	◦	◦	◦	◦	◦

Potential difference between n side (higher due to positive net charge) und p side (lower due to negative net charge), depending (among others) on doping concentration. In silicon typically 0.6 V - 0.7 V.

Extreme Reverse Bias Voltage: Breakdown

Durchbruchspannung



- A diode cannot hold arbitrarily high reverse bias!

Above: Breakdown

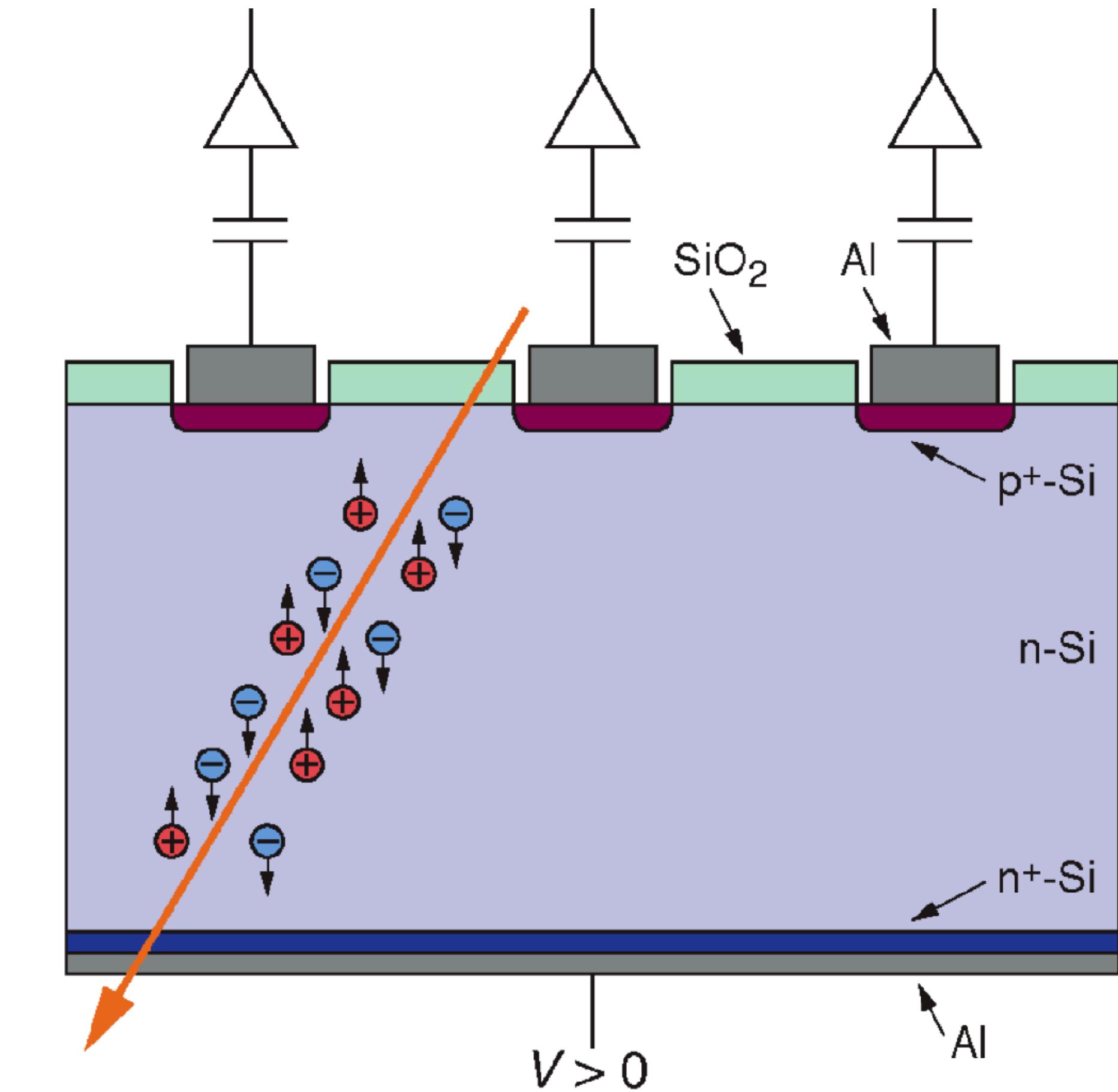
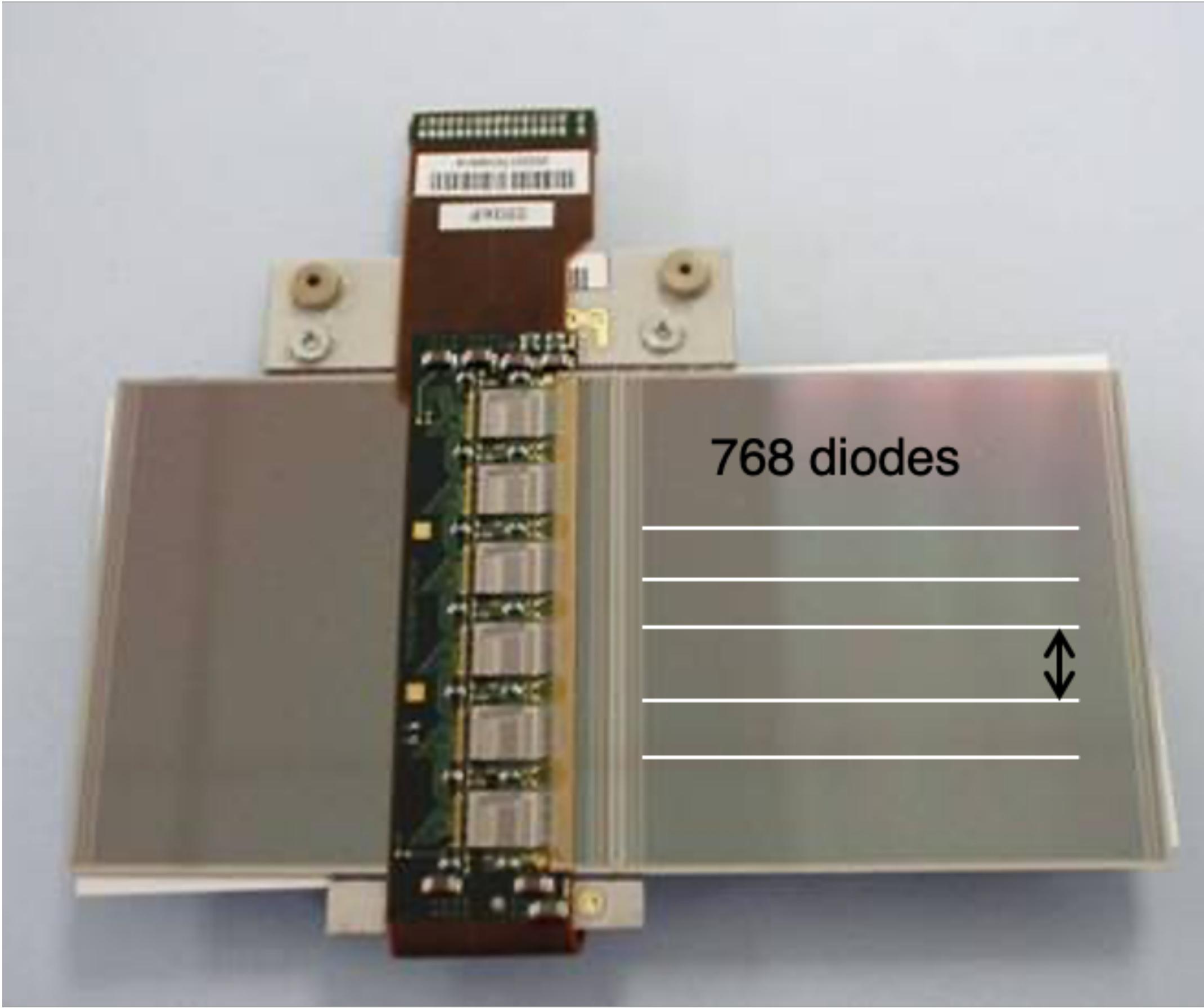
Normally unwanted:
High currents, power dissipation,
temperature results in destruction of the
diode.

But: There are exceptions:
Zener diodes
avalanche diodes (avalanche amplification!)

Diodes beyond Electronics Components

A wide Range of Applications

- Silicon detectors in particle physics.

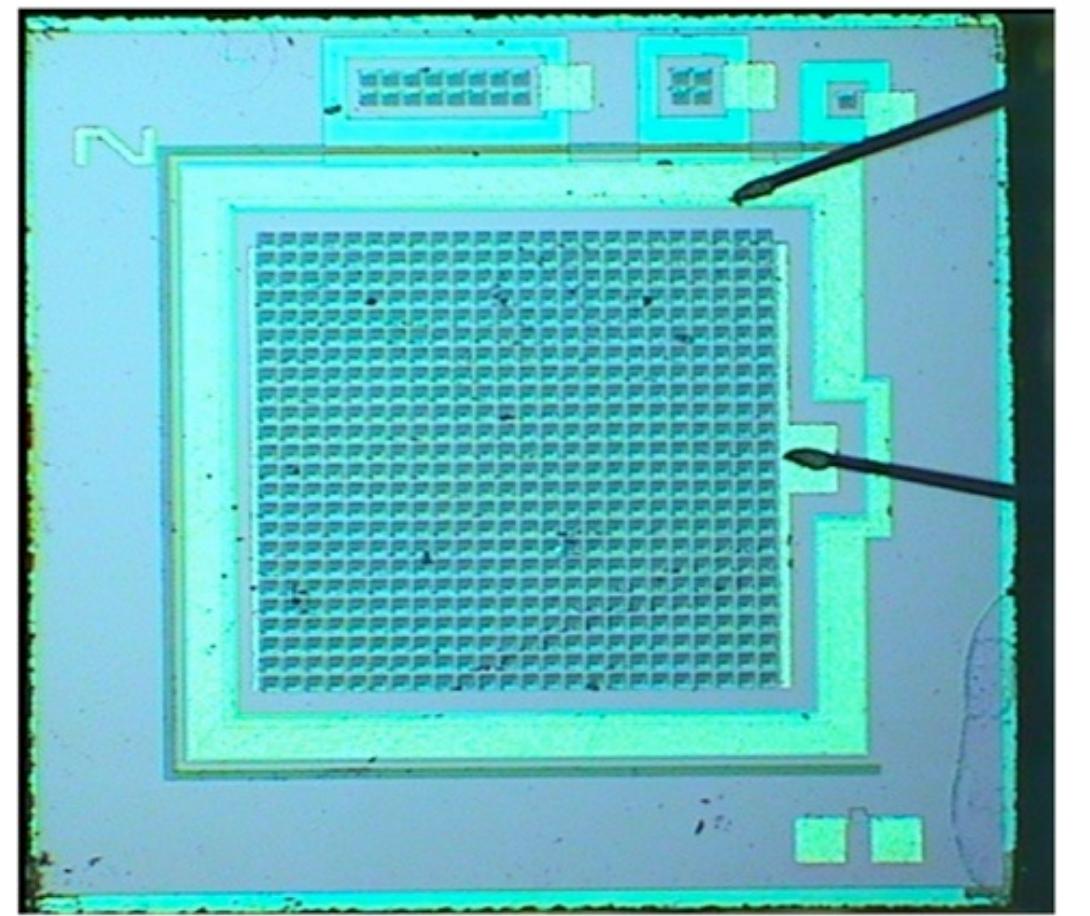
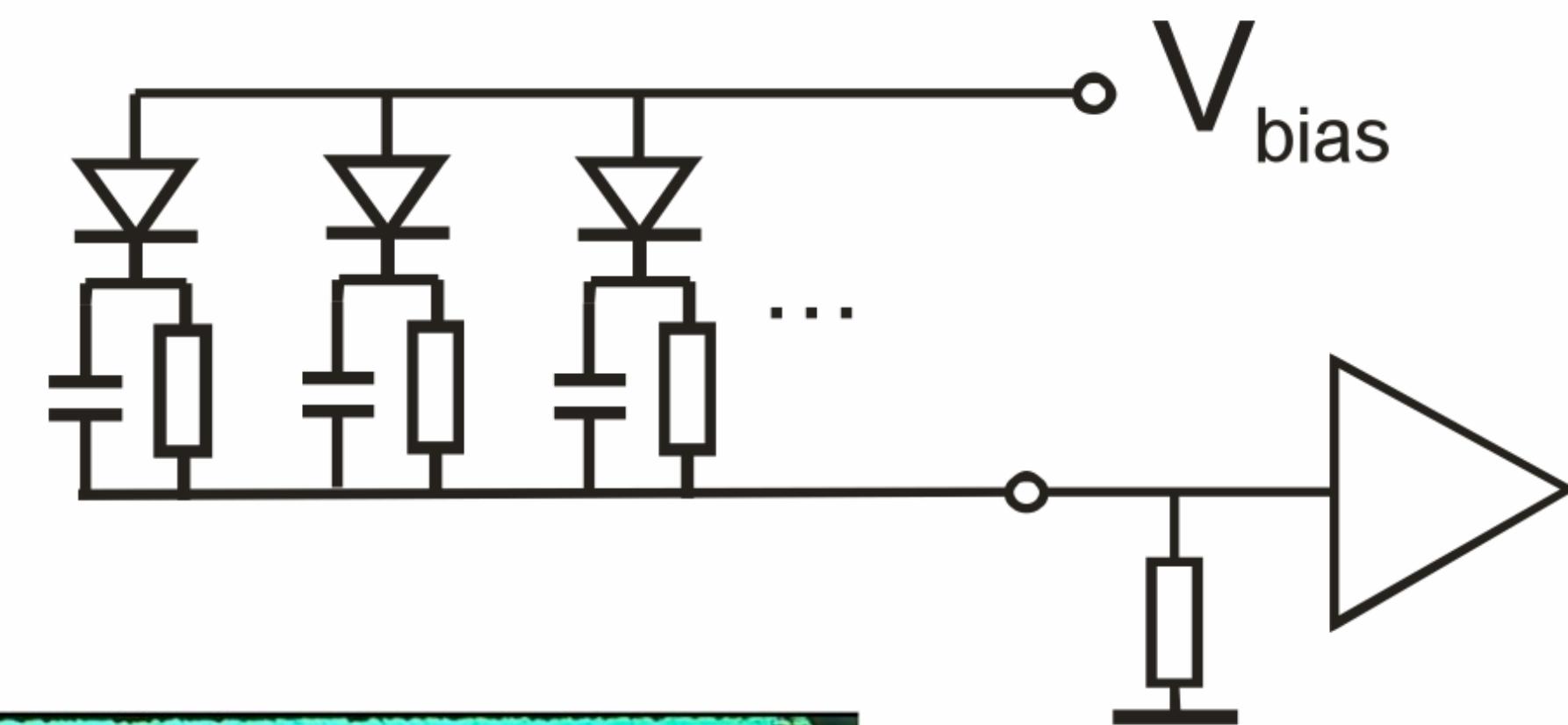
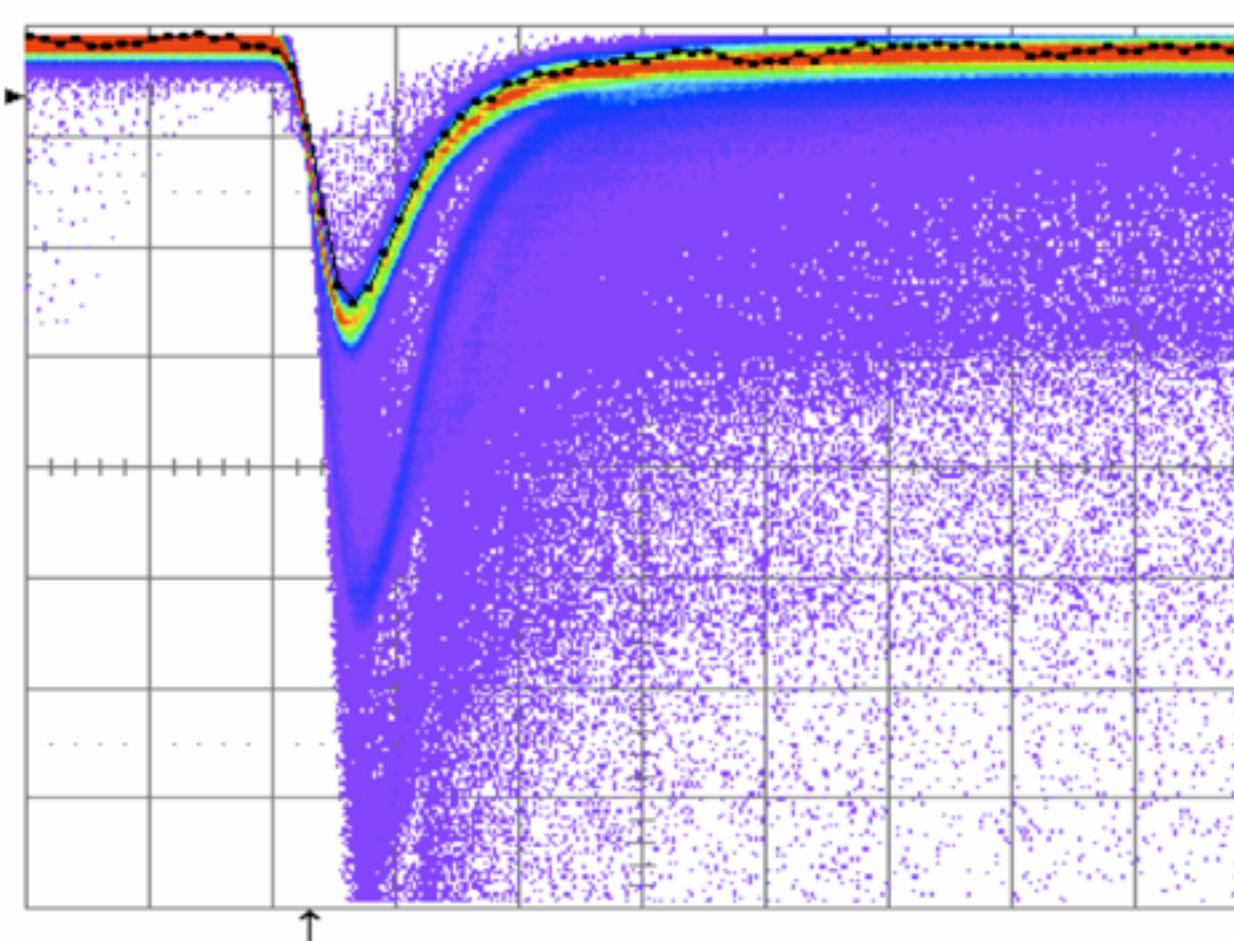
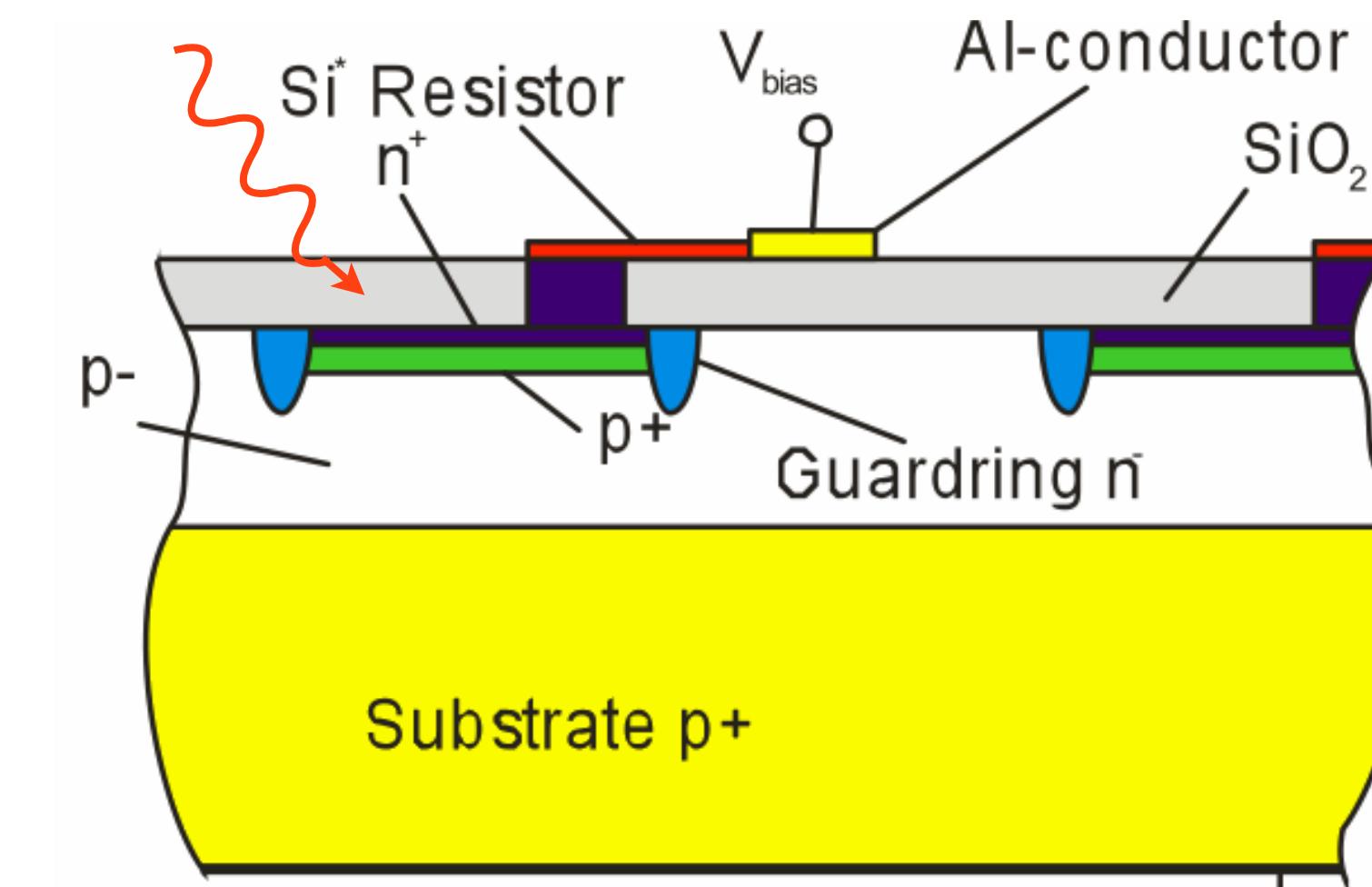
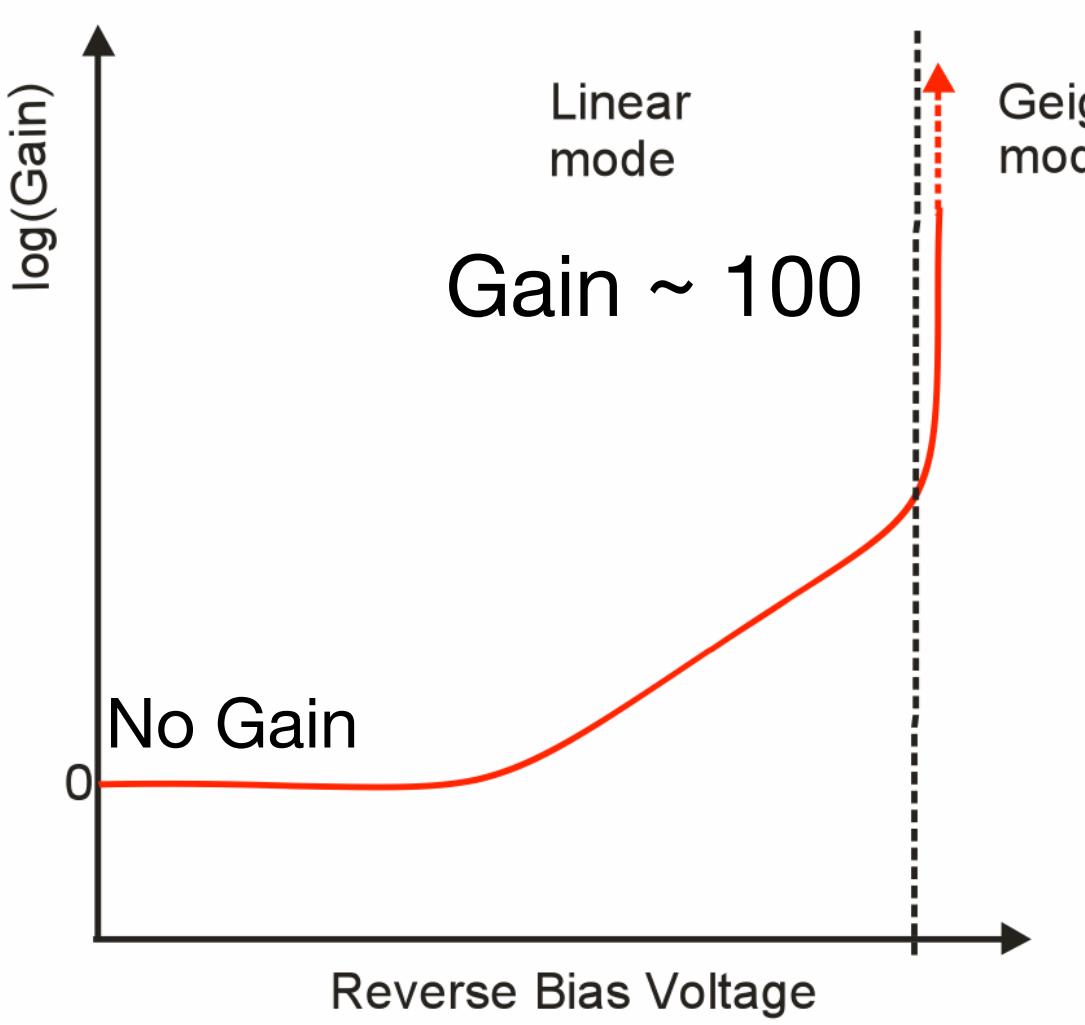


Diodes beyond Electronics Components

A wide Range of Applications

- Silicon Photomultiplier (SiPM)

Avalanche Photo Diode APD



Temperature Dependence of Diodes

Temperaturabhängigkeit

- The properties of diodes depend on temperature.

Two main effects:

- Intrinsic charge carrier density - thermal excitation
- Dependence on U_T (IV curve / Shockley equation)

$$\frac{kT}{q_e} = U_T$$

Forward bias

$$\frac{dU}{dT} = \frac{U_S - U_G - 3U_T}{T}$$

$U_G \sim 1.12 \text{ V}$ (band gap) =>

$$\frac{dU}{dT} = -1,87 \frac{\text{mV}}{\text{°C}}$$

(at 300 K)

in reverse bias:

$$I_S \sim T^{\frac{3}{2}} e^{-\frac{q_e U_G}{2kT}}$$

Current grows with increasing temperature - doubling every $\sim 7 \text{ K}$.

Risk of a “thermal run-away”!

Next Lectures:

Digital - Thursday, November 16 & Tuesday Nov. 21

Analog 06 - Chapters 03, 04 - Thursday, Nov. 23

Time Plan for Next Lectures

A few Changes coming up!

Calender Week	Tuesday	Thursday
45	07.11. Analog	09.11. Digital
46	14.11. Analog	16.11. Digital
47	21.11. Digital	23.11. Analog
48	28.11. Digital	30.11. Digital
49	05.12. Digital	07.12. Analog
50	12.12. Digital	14.12. Analog
51	19.12. Analog	21.12. Digital
2	09.01. Analog	11.01. Analog
3	16.01. Digital	18.01. Digital
4	23.01. Analog	25.01. Digital
5	30.01. Analog	01.02. Digital
6	06.02. Analog	08.02. Digital
7	13.02. Analog	15.02. Digital

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