

Electronics for Physicists

Analog Electronics

Chapter 8; Lecture 14

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08.02.2024

KIT, Winter 2023/24

Chapter 8

Additional Topics

- Filters and Voltage Regulators
- Noise

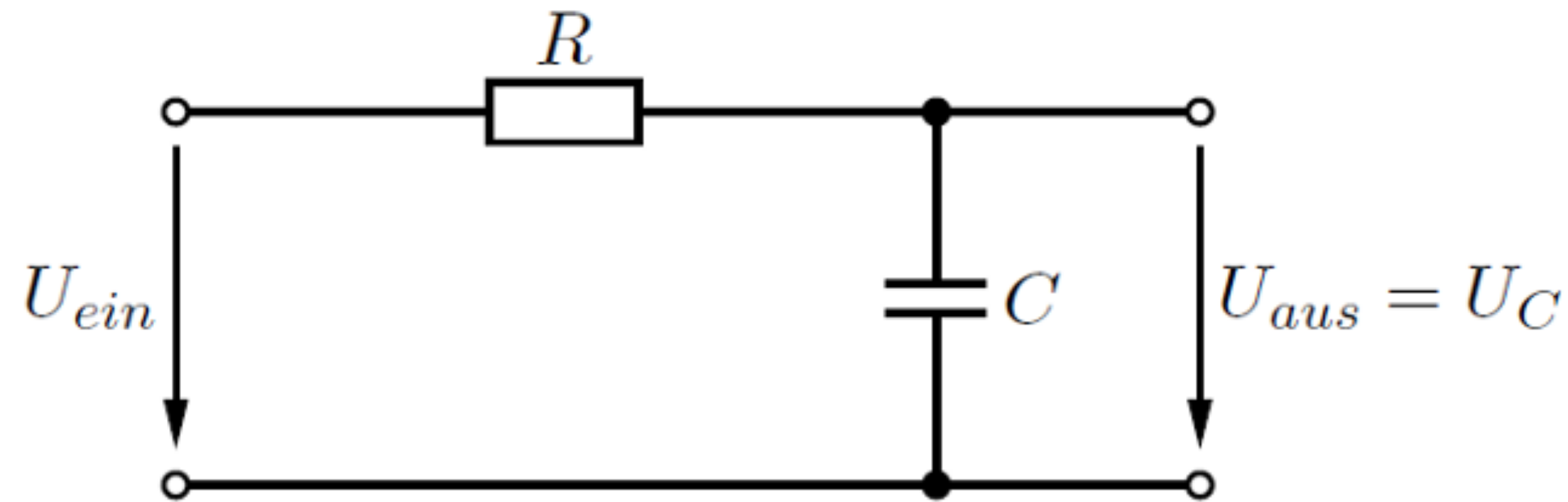
Overview

1. Basics
2. Circuits with R, C, L with Alternating Current
3. Diodes
4. Operational Amplifiers
5. Transistors - Basics
6. 2-Transistor Circuits
- 7. Field Effect Transistors**
8. Additional Topics
 - Filters
 - Voltage Regulators
 - Noise

Active Filters

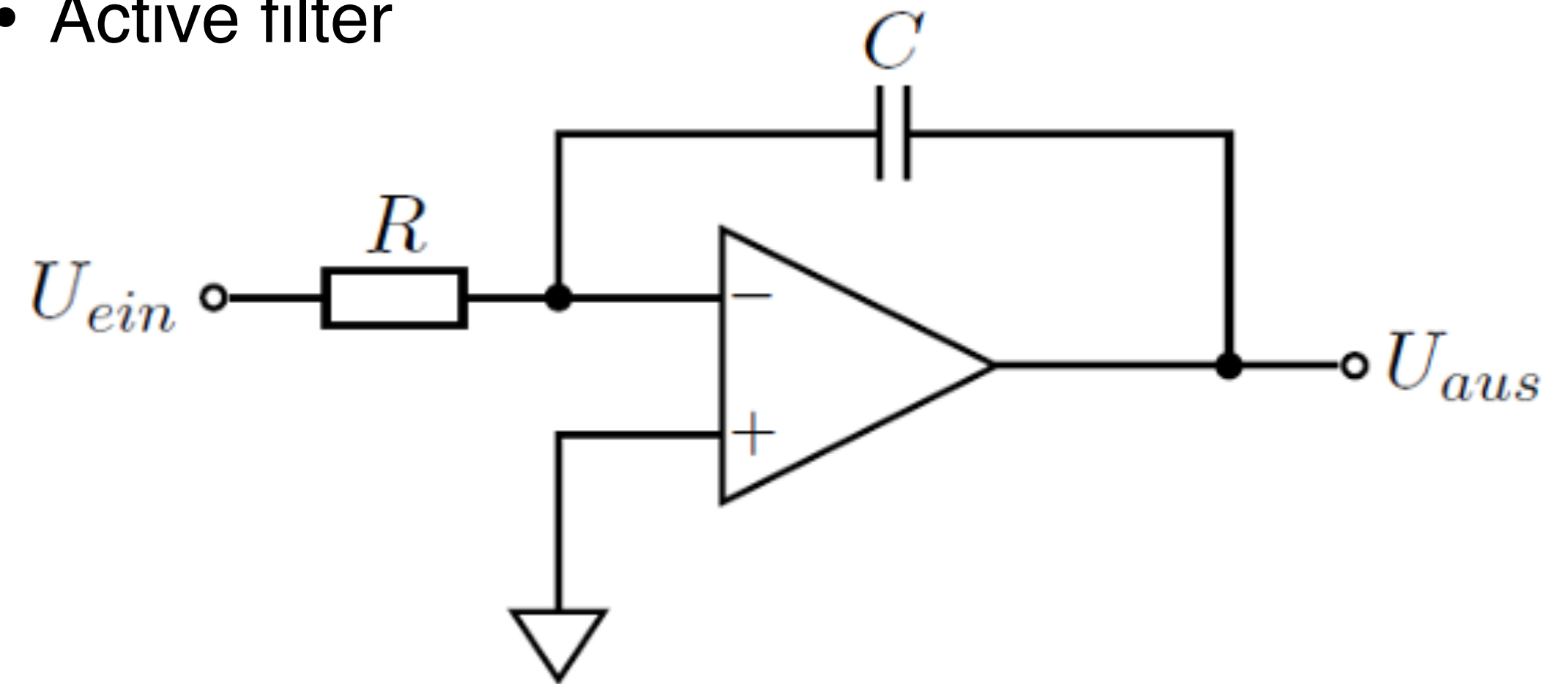
In: Chapter 8 - Additional Topics

- Passive filter



Low pass: $\frac{U_{aus}}{U_{ein}} = -\frac{Z}{R} = -\frac{1}{\omega RC}$

- Active filter



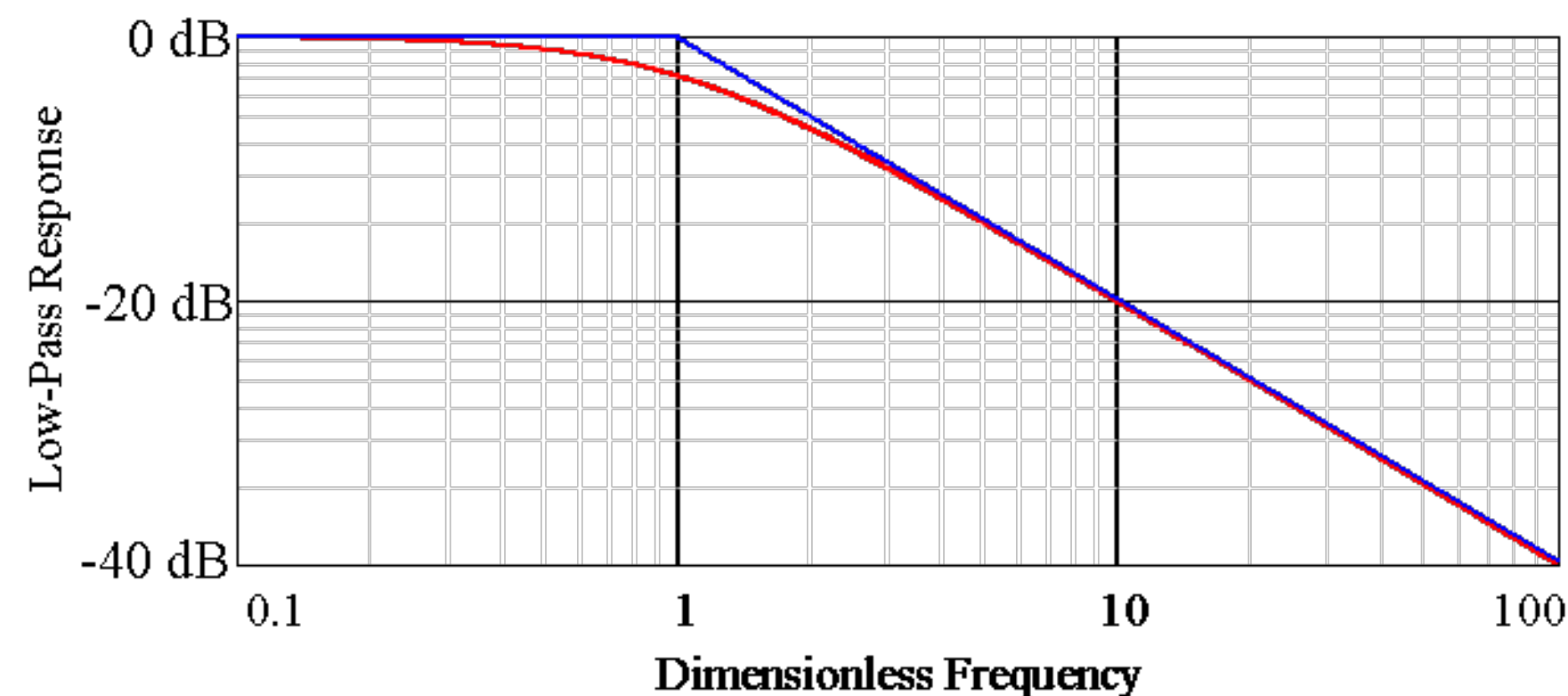
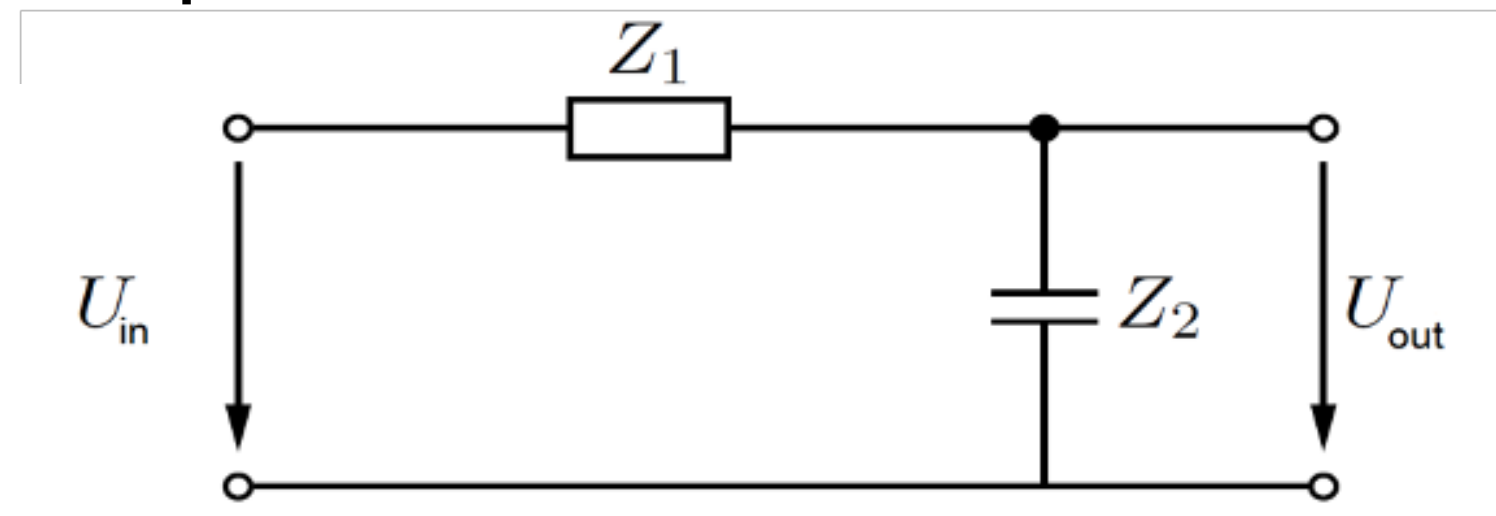
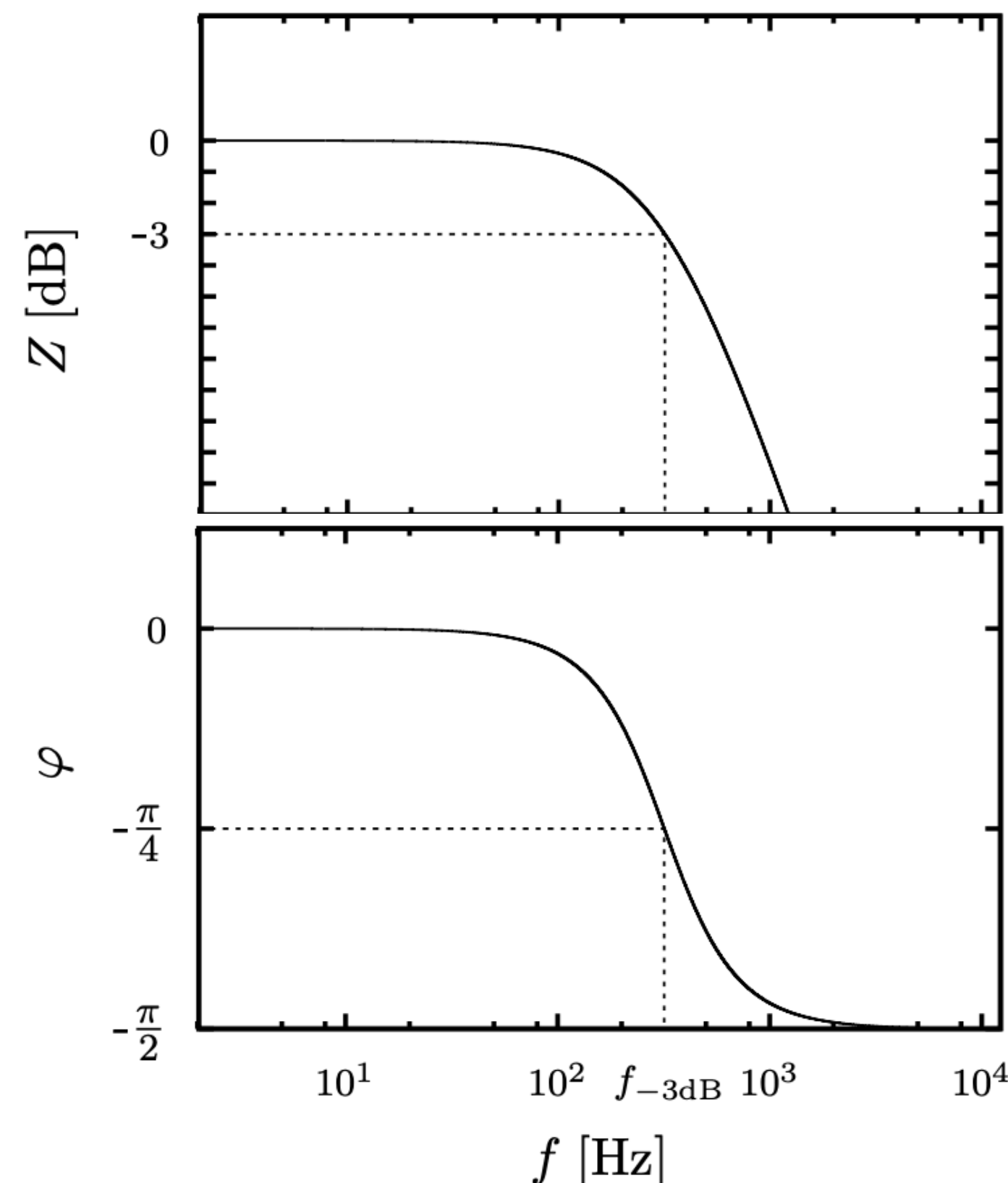
Integrator: $U_{aus} = -\frac{1}{RC} \int U_{ein} dt$

- Active filters: Op-Amps, R, C
 - Requires power - but built-in amplification prevents load on input / intermediate stages for multi-stage filters.

- Order of filters: Defines loss of amplification / dampening (“rolloff rate”) for frequencies far above (low pass) / far below (high pass) the critical frequency.

Reminder: Chapter 2

Low pass



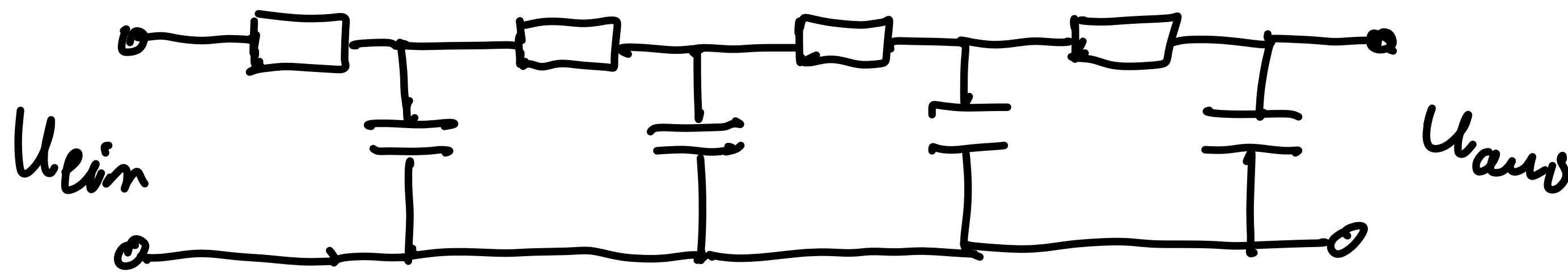
For high frequencies:

Z drops with 20 dB per frequency decade /
6 dB / octave (frequency $\times 2$ / $\times 0.5$)

\Rightarrow Filter of 1st order !

- Order of filters: Defines loss of amplification / dampening (“rolloff rate”) for frequencies far above (low pass) / far below (high pass) the critical frequency.

The easiest path to higher orders - and steeper flanks / higher rolloff rate:
Cascading of RC low passes



In general:

dampening of $n \times 20$ dB / decade

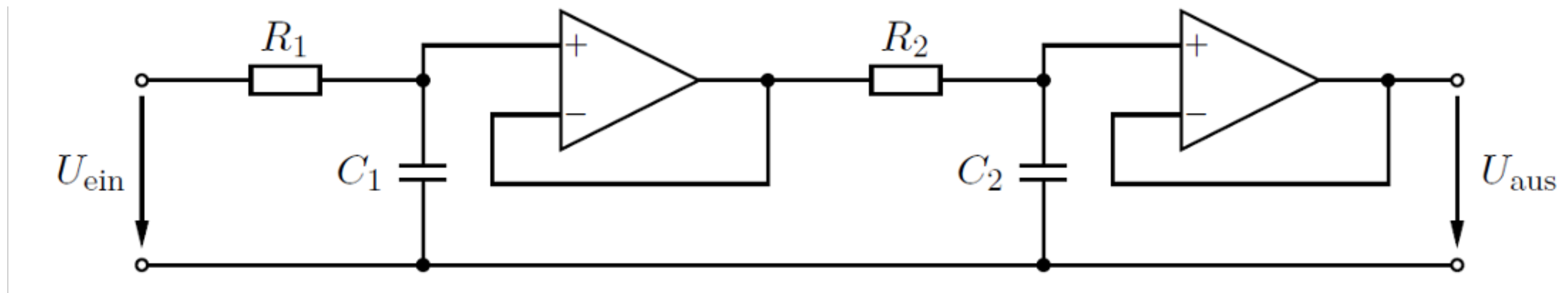
n = order of filter

Active Filter: 2nd Order Filter

The naive Approach - Cascading

- Cascading of filters provides higher orders - lossless due to active components
- Enables compact construction - inductors can be replaced with capacitors and OPVs

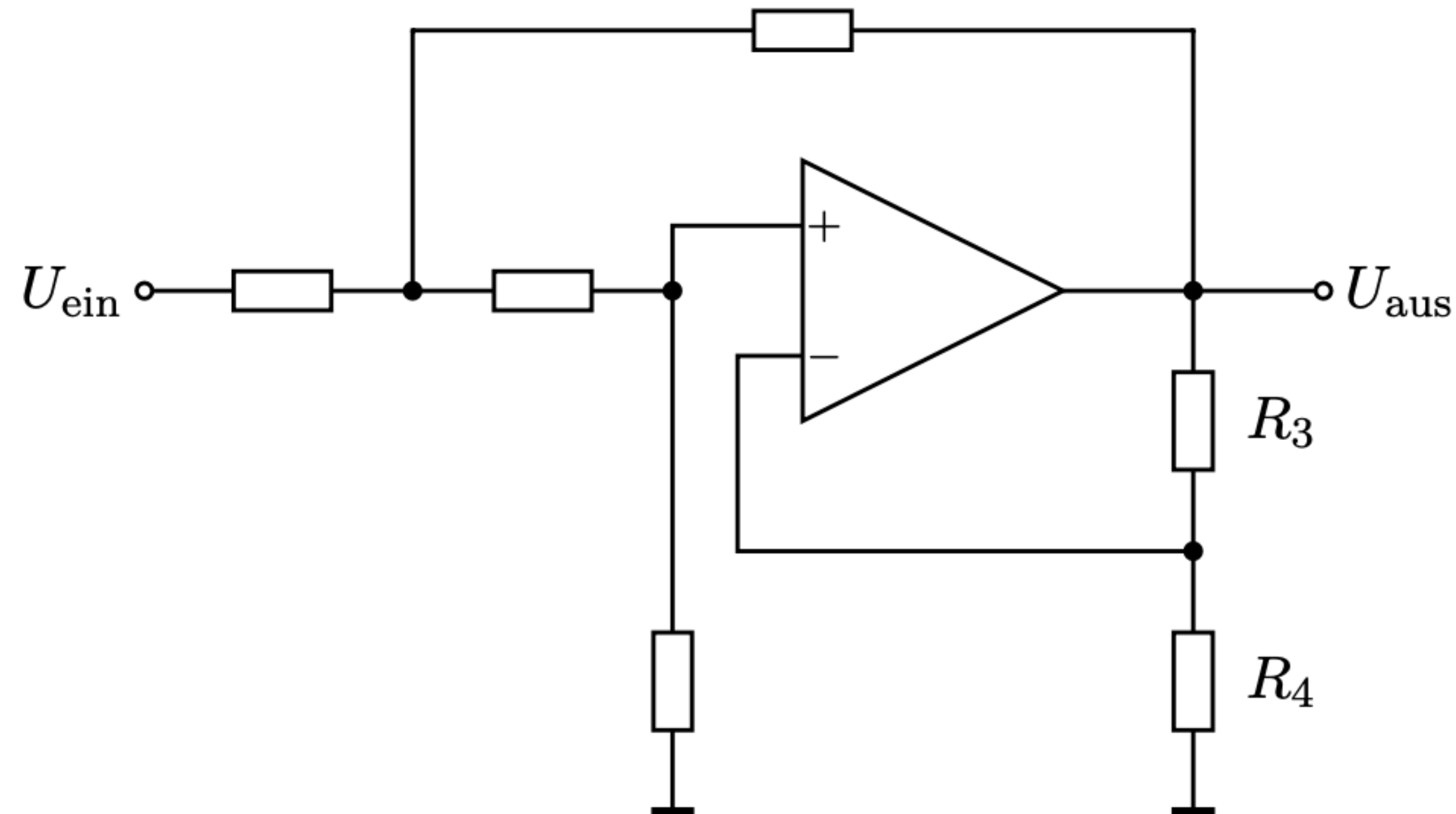
Naive solution for a 2nd order low pass



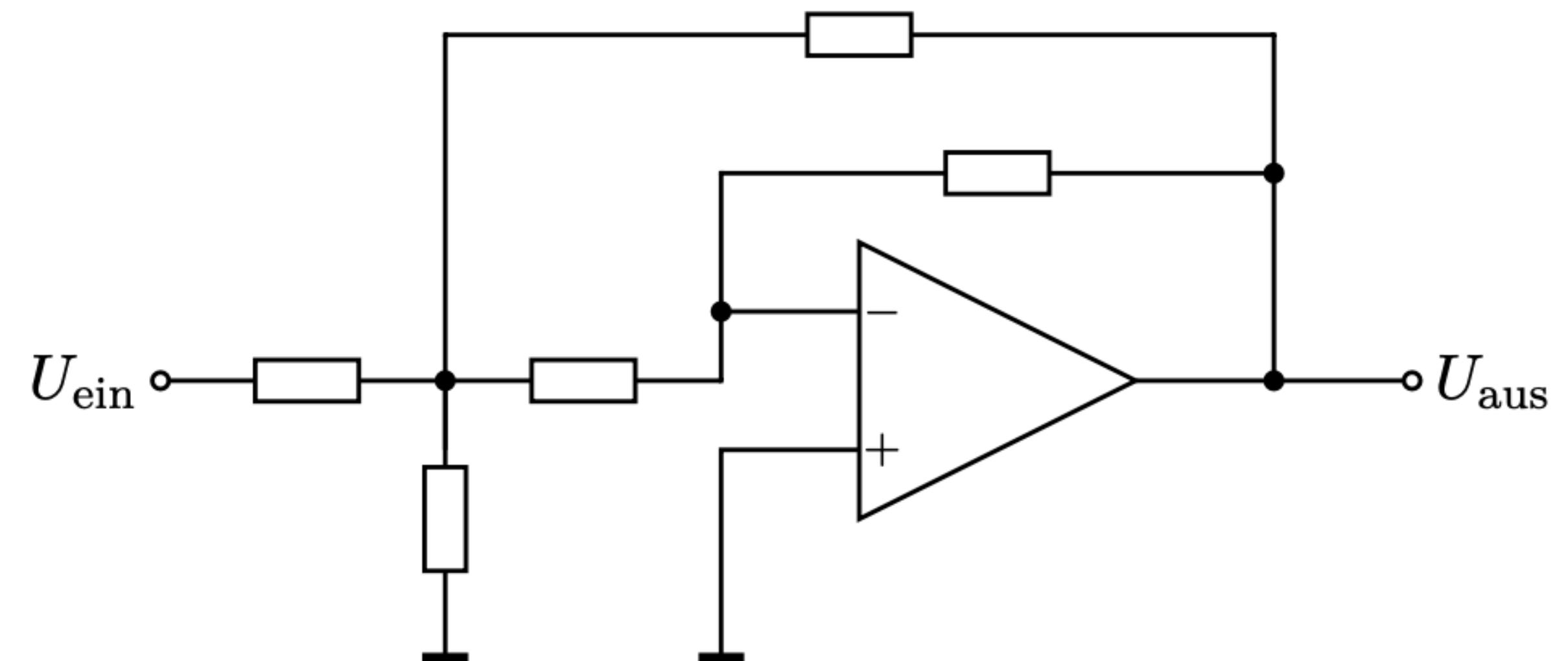
2x passive RC filter, 2 x OpAmp as buffer

Active Filter: 2nd Order Filter

Two common Topologies



- Generic Sallen-Key filter
(R. P. Sallen and E. L. Key, MIT, 1955)
- Simple structure, minimal number of components.



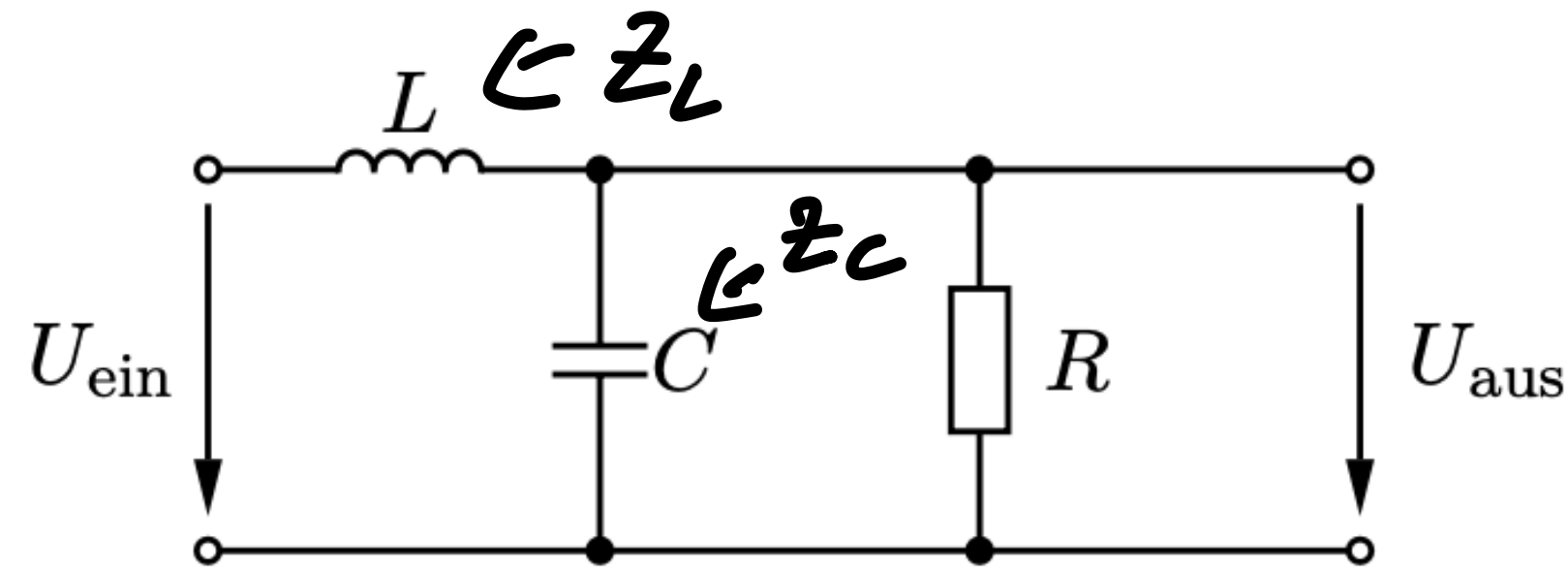
- Generic multi-feedback filter

Turning these into filters: two of the unnumbered resistors replaced by capacitors - the choice determines the type of filter.

Insert: Transfer Function 2nd Order Filter

Passive Filters

- Passive low pass 2nd order



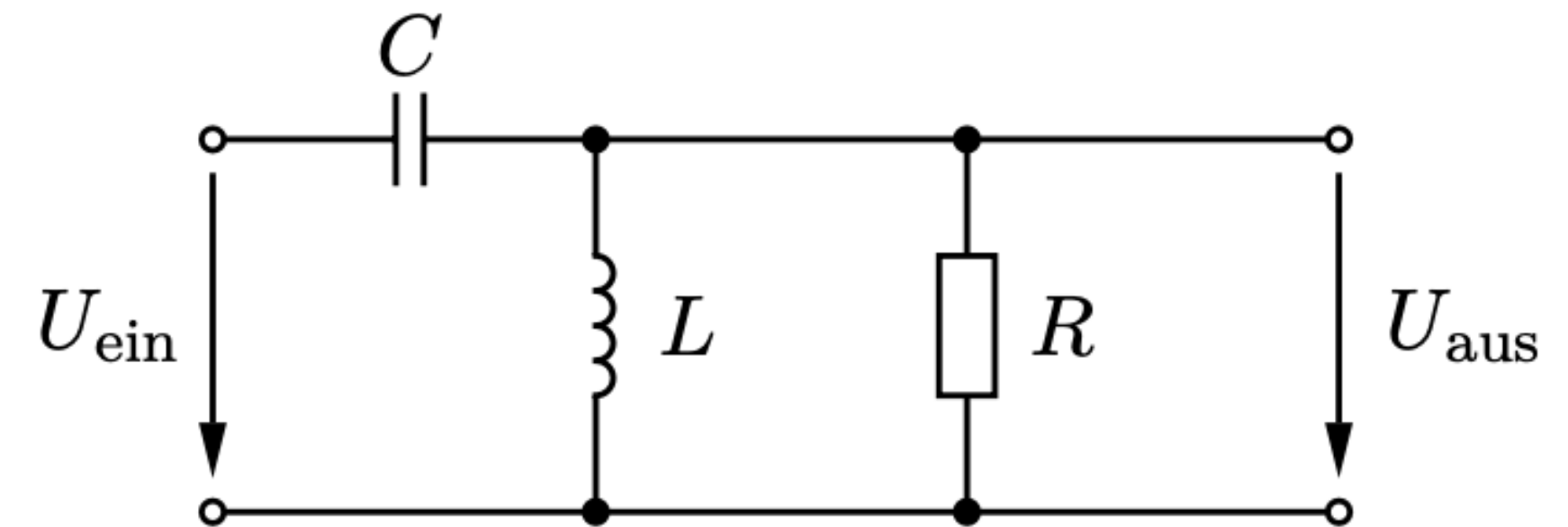
Def.: $s \hat{=} j\omega$

Transfer function:

$$Z = \frac{Z_C \parallel R}{Z_L + Z_C \parallel R} = \frac{R \frac{1}{sC}}{sL + \frac{R \frac{1}{sC}}{R + \frac{1}{sC}}} = \frac{R}{s^2 RCL + sL + R}$$

General: $Z(s) = \frac{1}{as^2 + bs + 1}$

- Passive high pass 2nd order

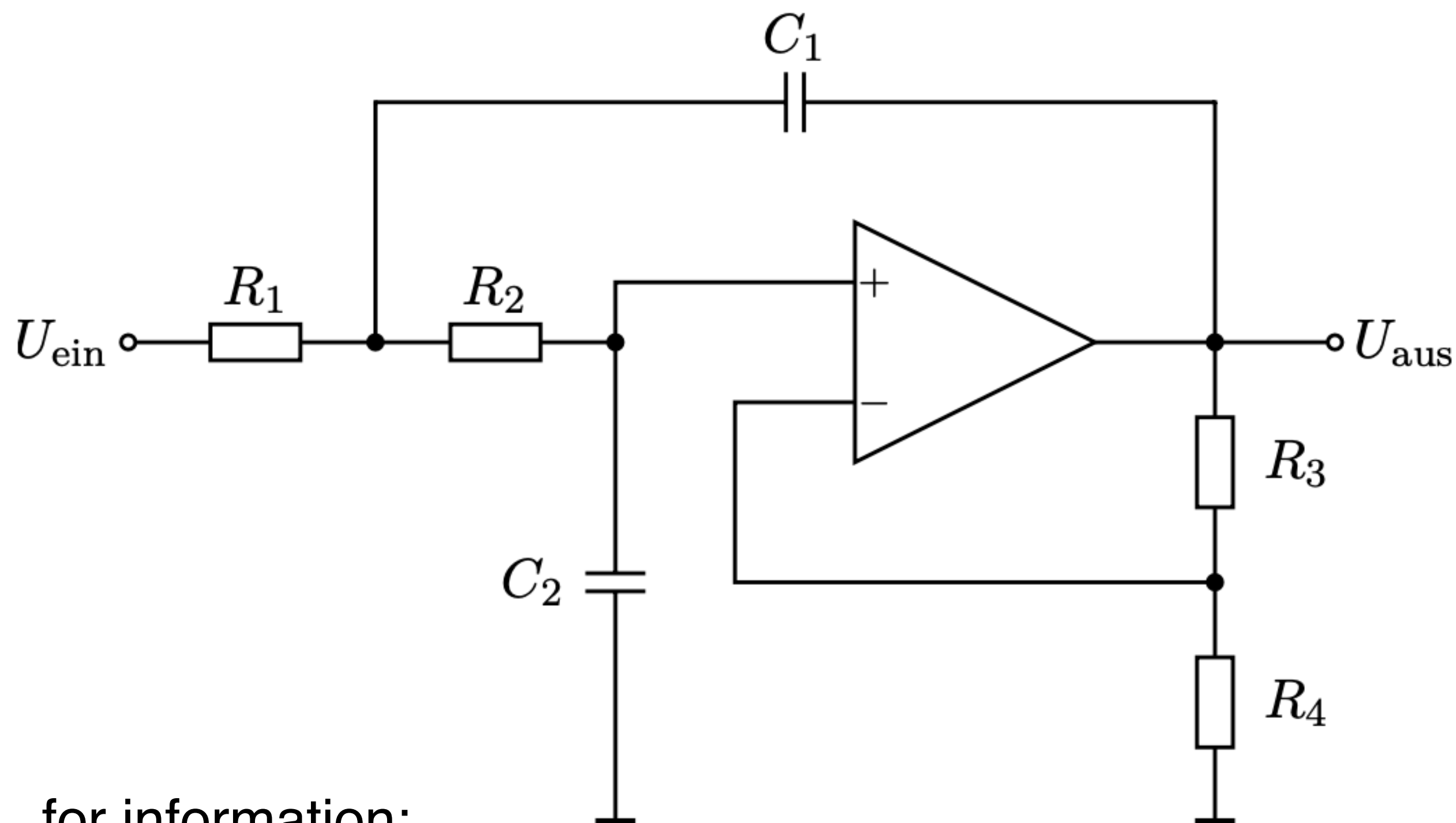


Same principle:

$$Z = \frac{sL \parallel R}{\frac{1}{sC} + sL \parallel R} = \frac{s^2 RCL}{s^2 RCL + sL + R}$$

$Z(s) = \frac{s^2}{s^2 + as + b}$

Sallen-Key Low Pass



for information:

$$Z(s) = \frac{1}{as^2 + bs + 1} \quad Q = \frac{\sqrt{R_1 R_2 C_1 C_2}}{C_2 (R_1 + R_2)} \quad 2\pi f_c = \omega_c = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}}$$

$$a = C_1 C_2 R_1 R_2 = \frac{1}{\omega_c^2} \quad , \quad b = C_2 \cdot (R_1 + R_2) = \frac{1}{\omega_c Q}$$

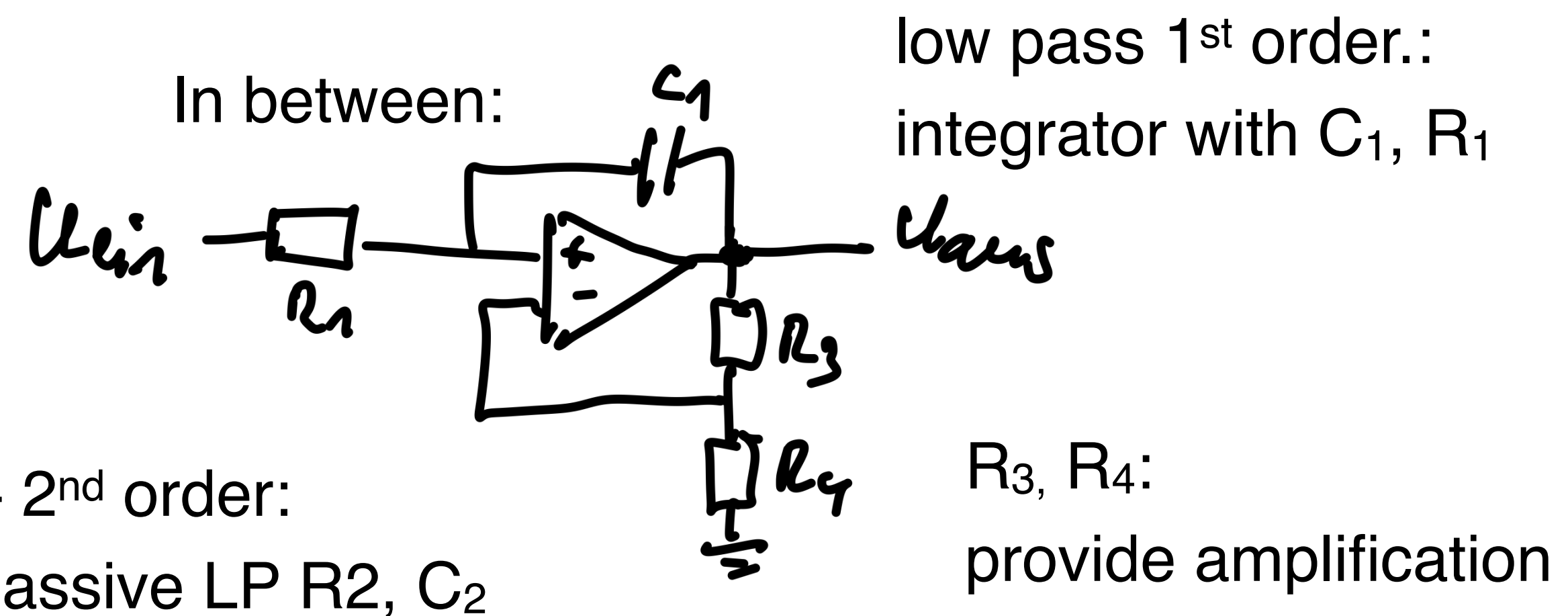
- Why does this circuit act as a low pass?

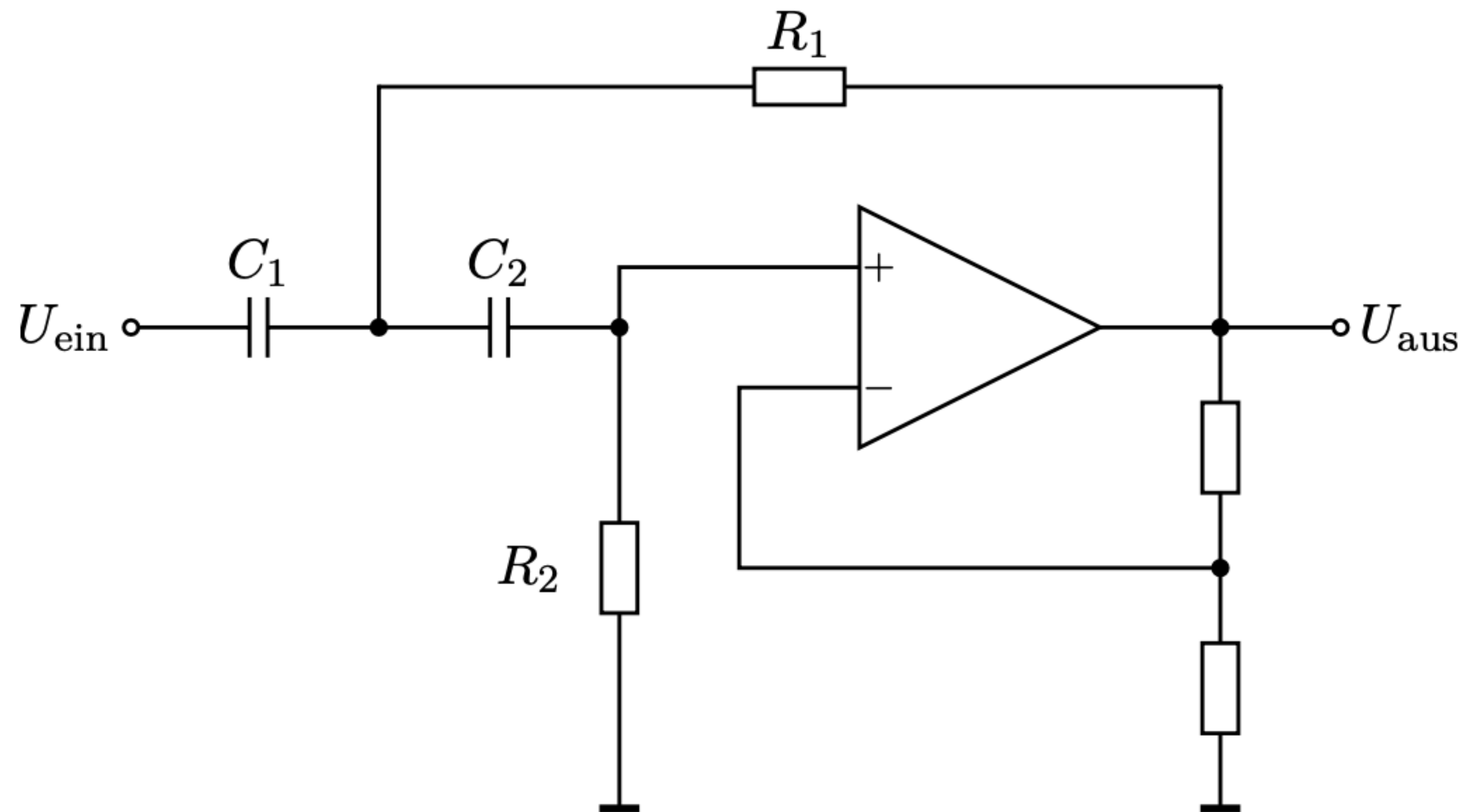
For small frequencies: C_1, C_2 “open”:

Op-Amp “passing through” $\Rightarrow Z = 1$

For high frequencies: C_2 “shorted”:

Op-Amp “+” input on ground, with golden rules
 $U_{aus} = 0$.





- Analogous to low pass:
High frequencies passed by C_1 and C_2 .
Low frequencies blocked by C_1 , R_1 and C_2 , R_2 .

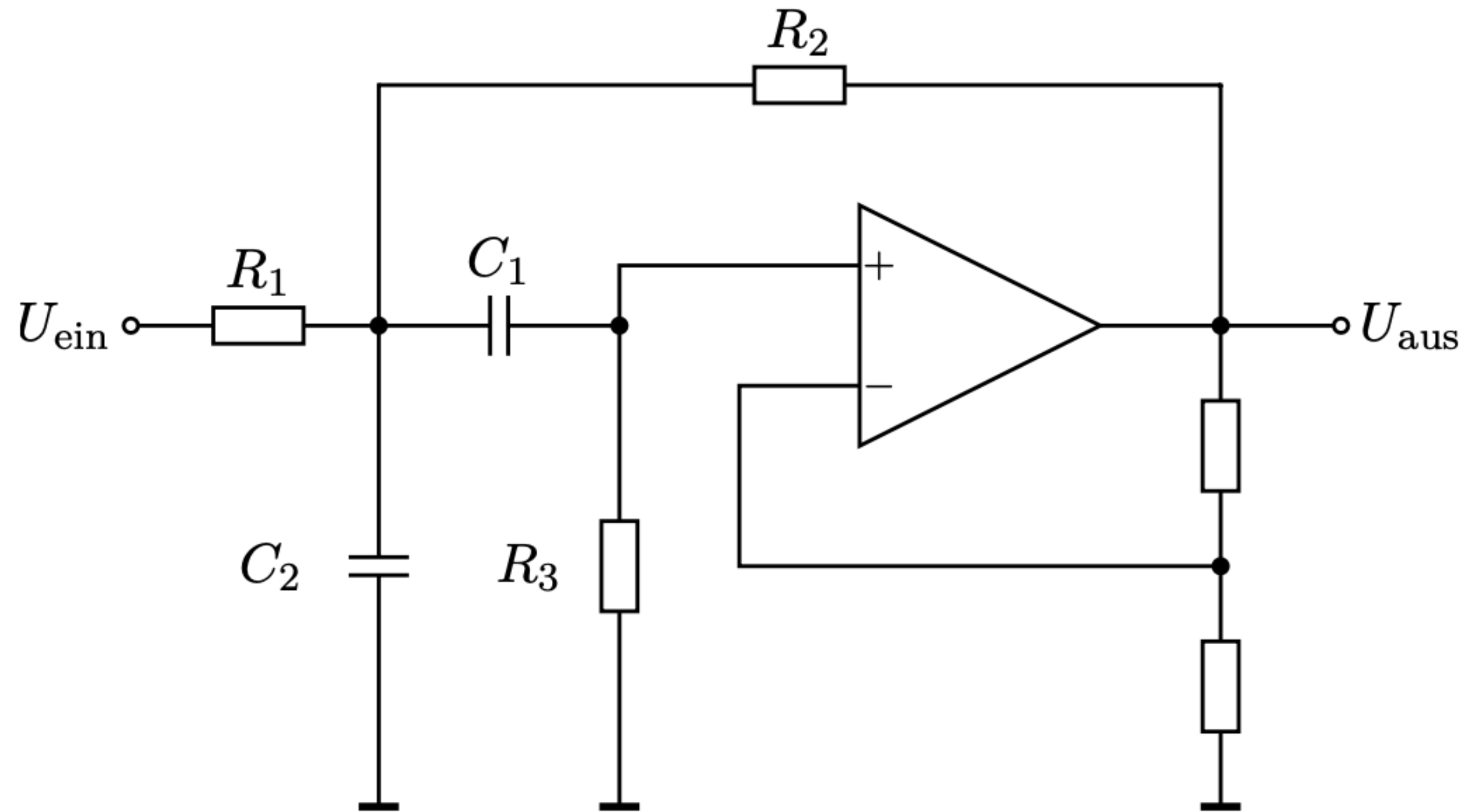
For information:

$$Z(s) = \frac{s^2}{s^2 + as + b}$$

$$a = \frac{1}{R_2 C_1} + \frac{1}{R_2 C_2} \quad , \quad b = \frac{1}{R_1 R_2 C_1 C_2}$$

$$2\pi f_c = \omega_c = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}} \quad \text{und} \quad Q = \frac{\sqrt{R_1 R_2 C_1 C_2}}{R_2 (C_1 + C_2)}$$

Sallen Key Band Pass



- High pass via C_1
- Low pass via C_2

- The behavior of filters is described by polynomials of corresponding order in s ($= j\omega$)

Generalized complex transfer function:

$$Z(s) = Z_0 \cdot \frac{s^n + \alpha_{n-1}s^{n-1} \dots + \alpha_1s + \alpha_0}{s^n + \beta_{n-1}s^{n-1} \dots + \beta_1s + \beta_0}$$

Highest power of s
defines filter order n

Filter of higher order can be built by cascading several filters of lower order.
Mathematically: Decomposition into polynomials with the appropriate factors:

$$\begin{aligned} &= \frac{(s^2 + a_1s + b_1)(s^2 + a_2s + b_2) \dots}{(s^2 + c_1s + d_1)(s^2 + c_2s + d_2) \dots} \\ &= \frac{(s - z_0)(s - z_1)(s - z_2) \dots (s - z_n)}{(s - p_0)(s - p_1)(s - p_2) \dots (s - p_n)} \end{aligned}$$

As example:

Filter of 4th order:

=> two 2nd order filters

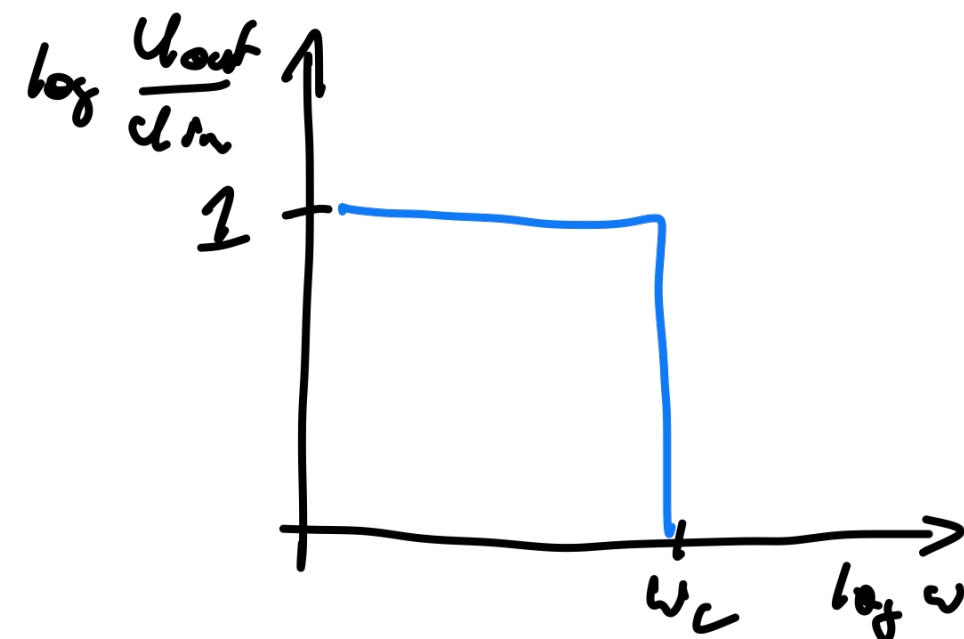
5th order:

=> add one more 1st order filter

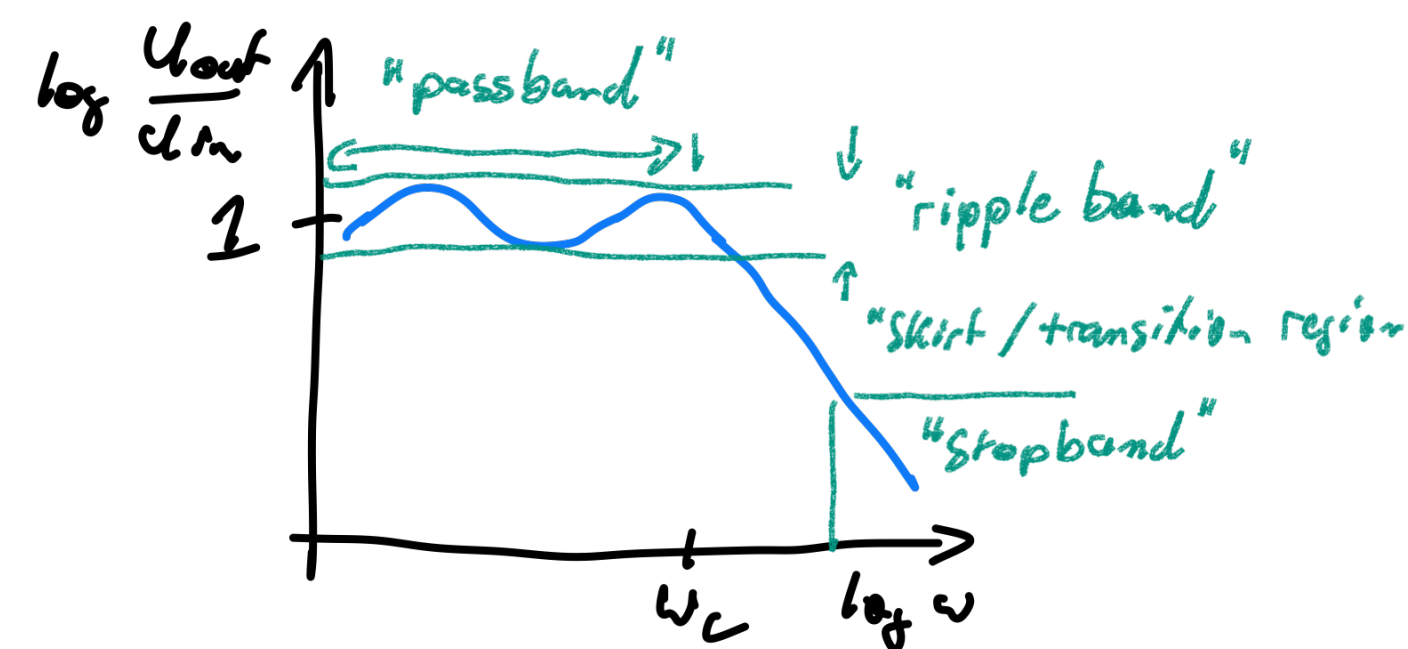
- The choice of the coefficients a_i, b_i, \dots define the behavior of the filter.
Components have to be chosen accordingly for the circuit implementation.

idealized expectation:

Example:
low pass



real situation:



pass band ("*Durchlassbereich*")

ripple in the pass band

skirt / transition region

stop band ("*Sperrbereich*")

Central property (independent of concrete implementation):

- The *cutoff frequency* ω_c defines the end of the pass band (typ. -3 dB)
- In the stop band the amplitude drops as $n \times 20$ dB per frequency decade

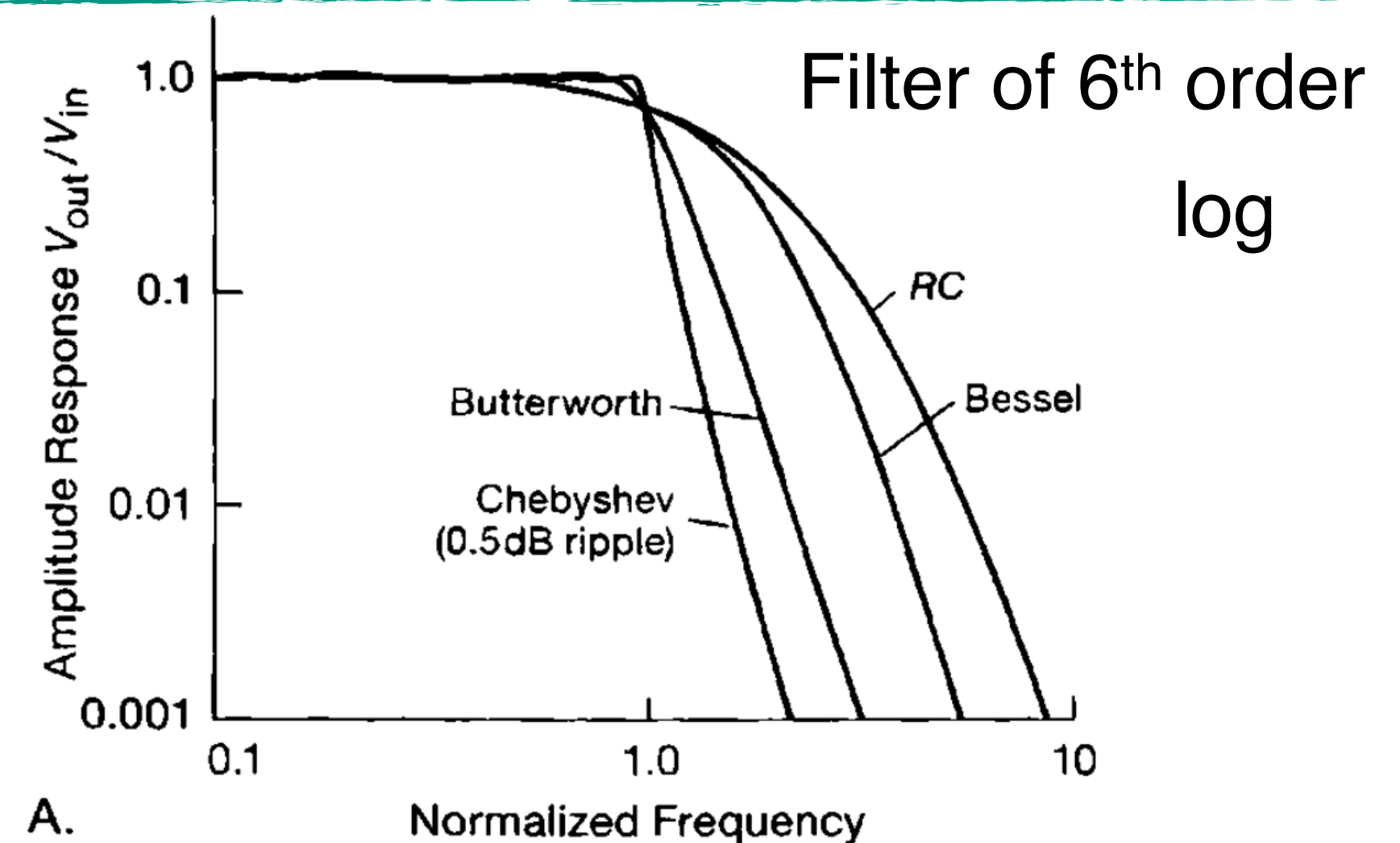
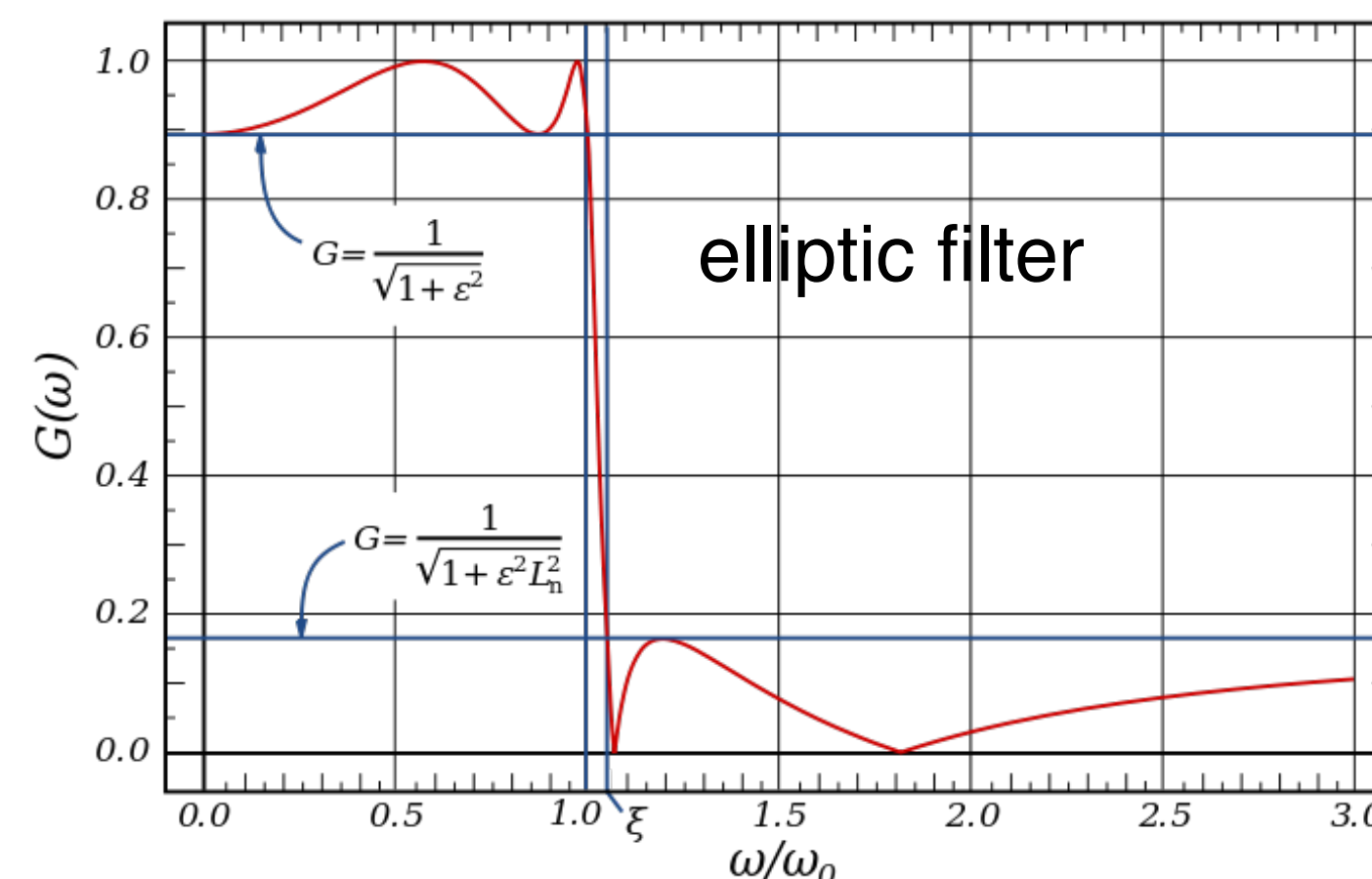
The concrete implementation defines - among others:

- Exact shape of the transfer function as a function of frequency (and the phase phase shift)
- Transition from pass band to stop band

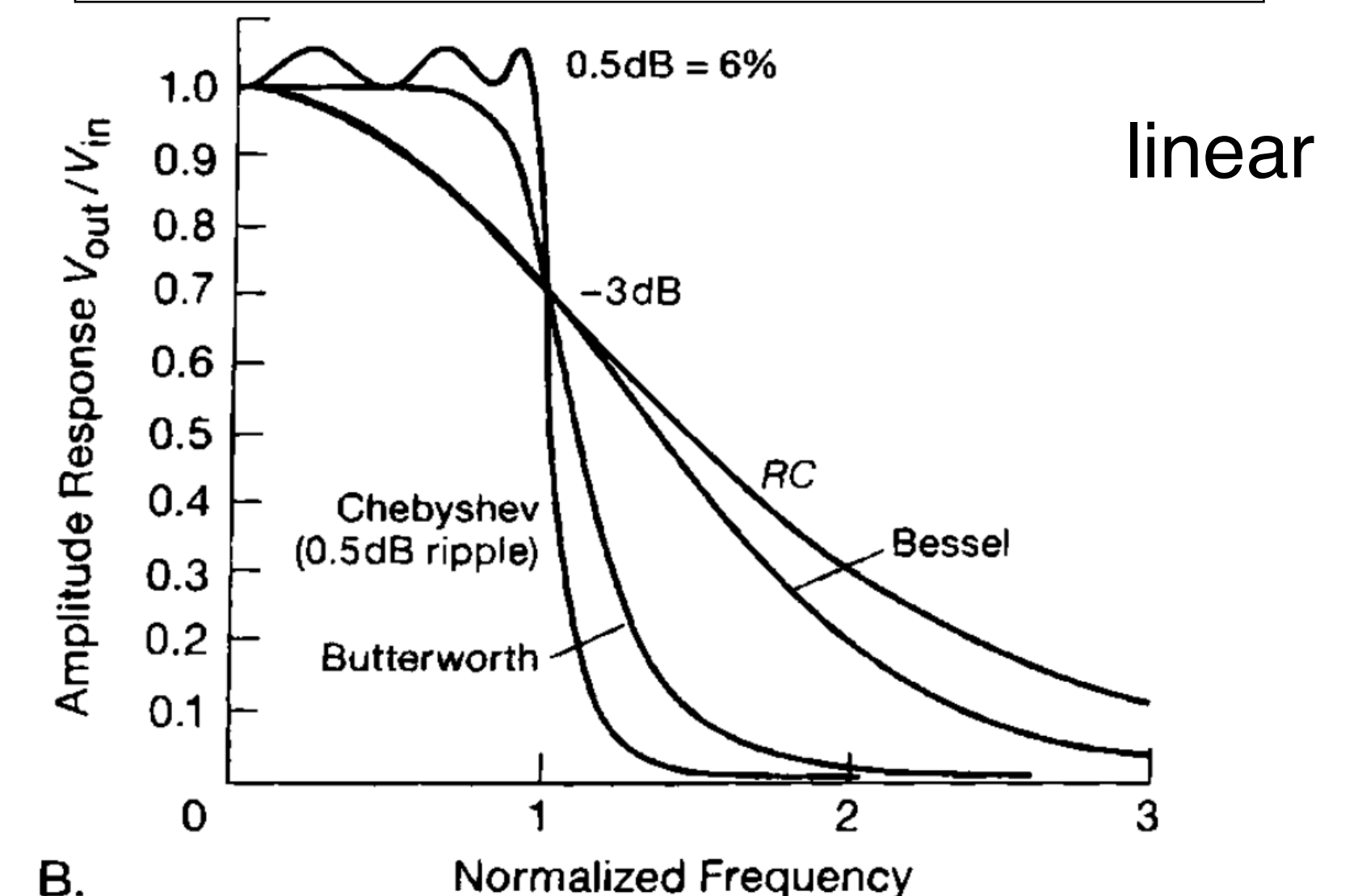
Filter Types

4 common basic types

- Differences in behavior in different regions and in phase
- Butterworth Filter:** Minimal ripple in pass band, smooth transition, monotone dampening in stop band.
- Tschebyscheff Filter:** Ripple in pass band, steep transition.
- Bessel Filter:** Slow transition, phase depends linearly on frequency: Minimal distortions.
- Elliptic Filter:** Very steep transition, but ripple in pass band and stop band.

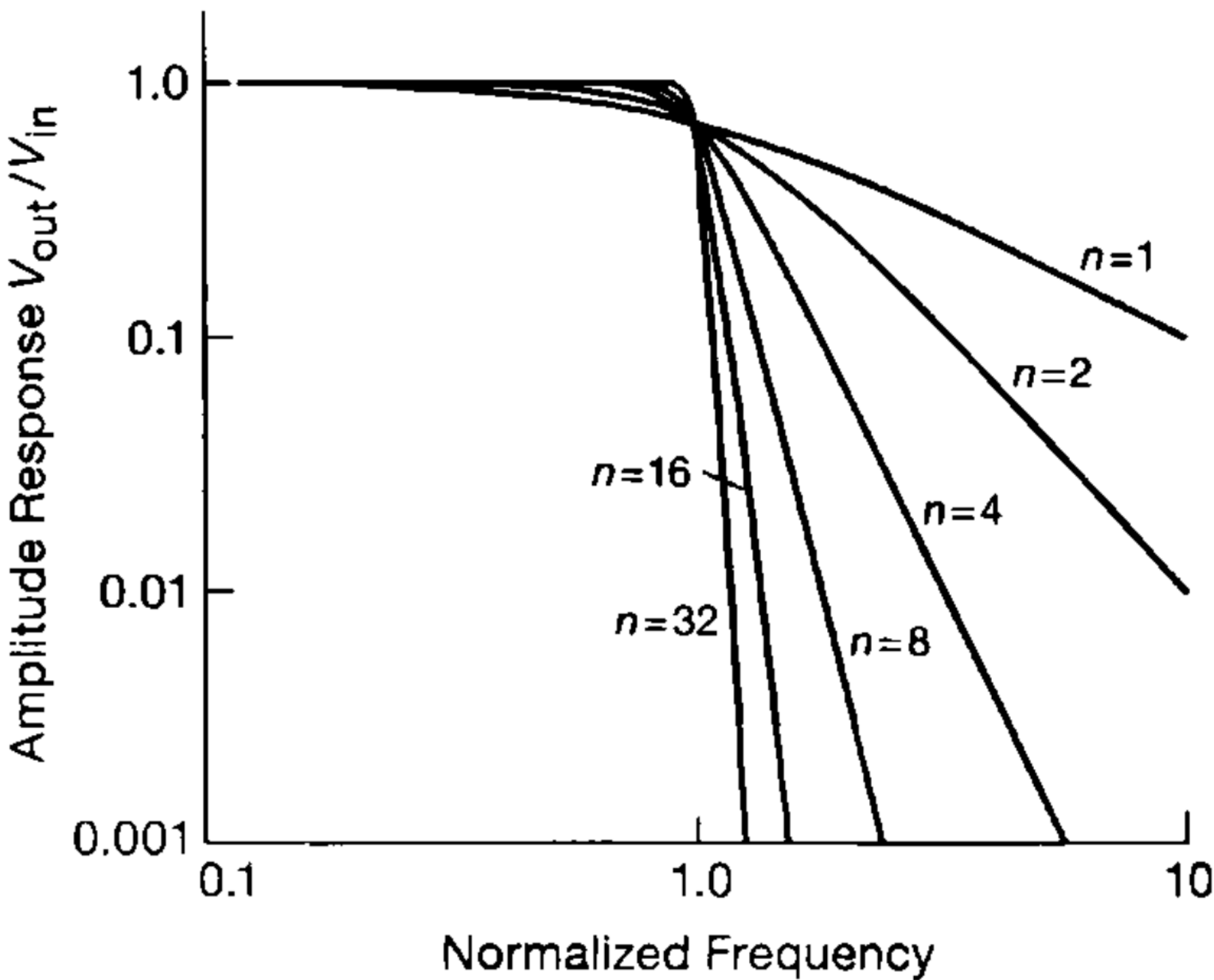


from: Horowitz, Hill "The art of electronics"



Butterworth Filter

Impact of Order



from: Horowitz, Hill “The art of electronics”

In general:

Coefficients of the transfer function taken from tables, component properties derived from this.

Mathematical description:

n	
1	$(1 + s)$
2	$(1 + 1.414s + s^2)$
3	$(1 + s)(1 + s + s^2)$
4	$(1 + 0.765s + s^2)(1 + 1.848s + s^2)$
5	$(1 + s)(1 + 0.618s + s^2)(1 + 1.618s + s^2)$
6	$(1 + 0.518s + s^2)(1 + 1.414s + s^2)(1 + 1.932s + s^2)$
7	$(1 + s)(1 + 0.445s + s^2)(1 + 1.247s + s^2)(1 + 1.802s + s^2)$
8	$(1 + 0.390s + s^2)(1 + 1.111s + s^2)(1 + 1.663s + s^2)(1 + 1.962s + s^2)$
9	$(1 + s)(1 + 0.347s + s^2)(1 + s + s^2)(1 + 1.532s + s^2)(1 + 1.879s + s^2)$
10	$(1 + 0.313s + s^2)(1 + 0.908s + s^2)(1 + 1.414s + s^2)(1 + 1.782s + s^2)(1 + 1.975s + s^2)$

From this: Transfer function for 3rd order:

$$Z(s) = \frac{1}{(s + 1)(s^2 + s + 1)}$$

for ex.: $a = C_1 C_2 R_1 R_2$ $b = C_2 \cdot (R_1 + R_2)$

(for Sallen-Key LP
2nd order
[S. 10])

Voltage Converters

In: Chapter 8 - Additional Topics

- Here: DC-DC Converters / Regulators

- Two basic types

switched-mode regulator (*Schaltregler / Schaltnetzteile*)

- most common type
- high efficiency
- Always a residual ripple on output
- Noise source
- Can increase and reduce voltages

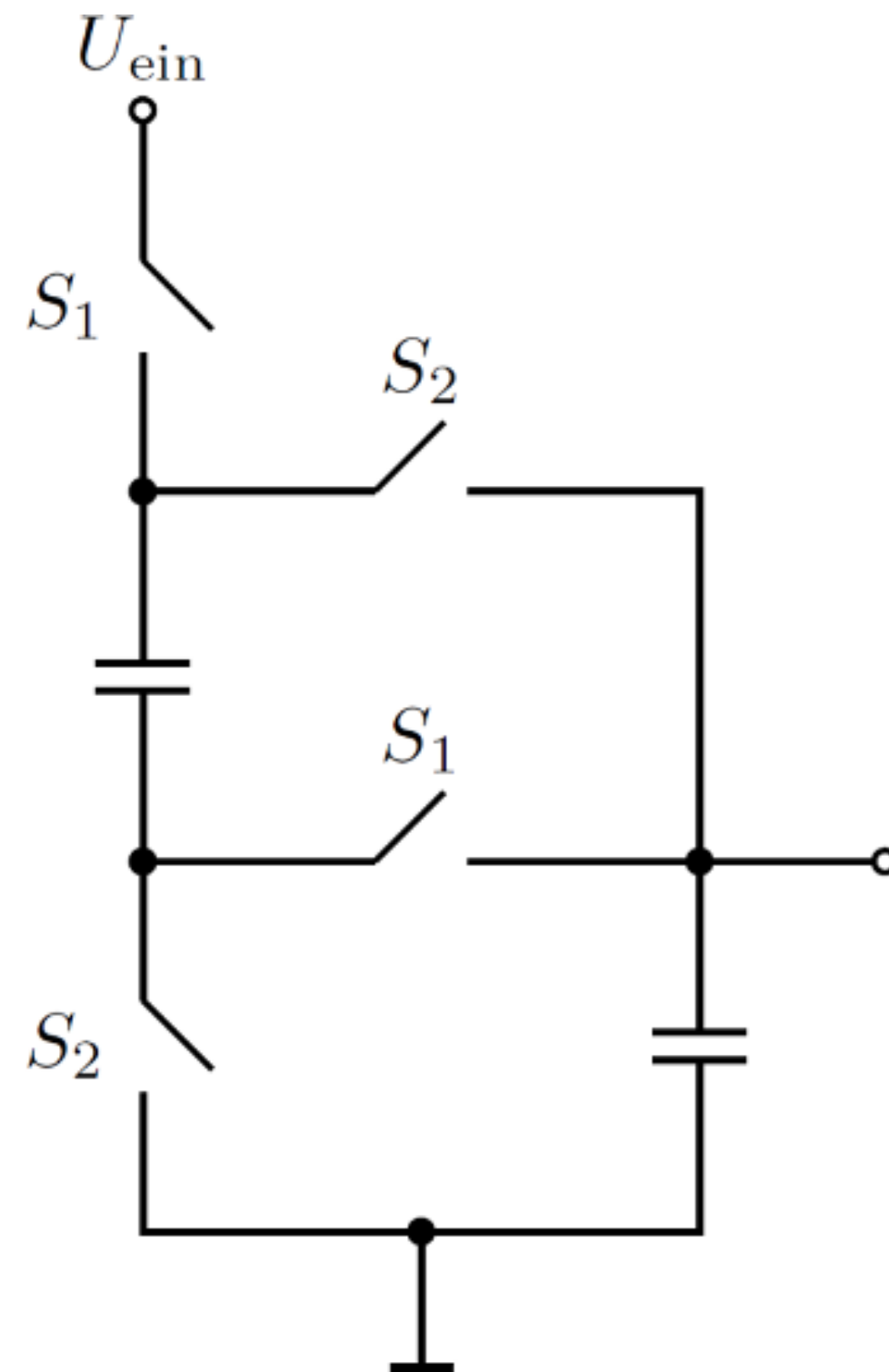
Linear regulator (*Linearregler*)

- Low efficiency
- Can only reduce voltages
- “Quiet” output

DC-DC Step-Down Converter

Simple voltage regulator

Switch S_i
in real life:
transistors

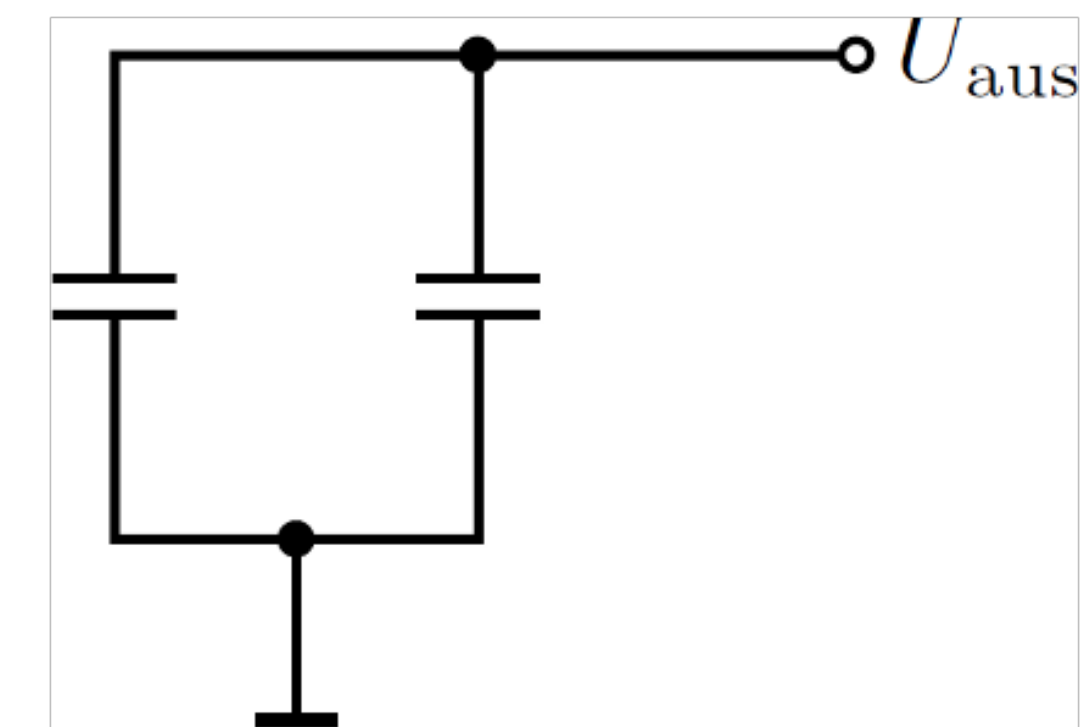
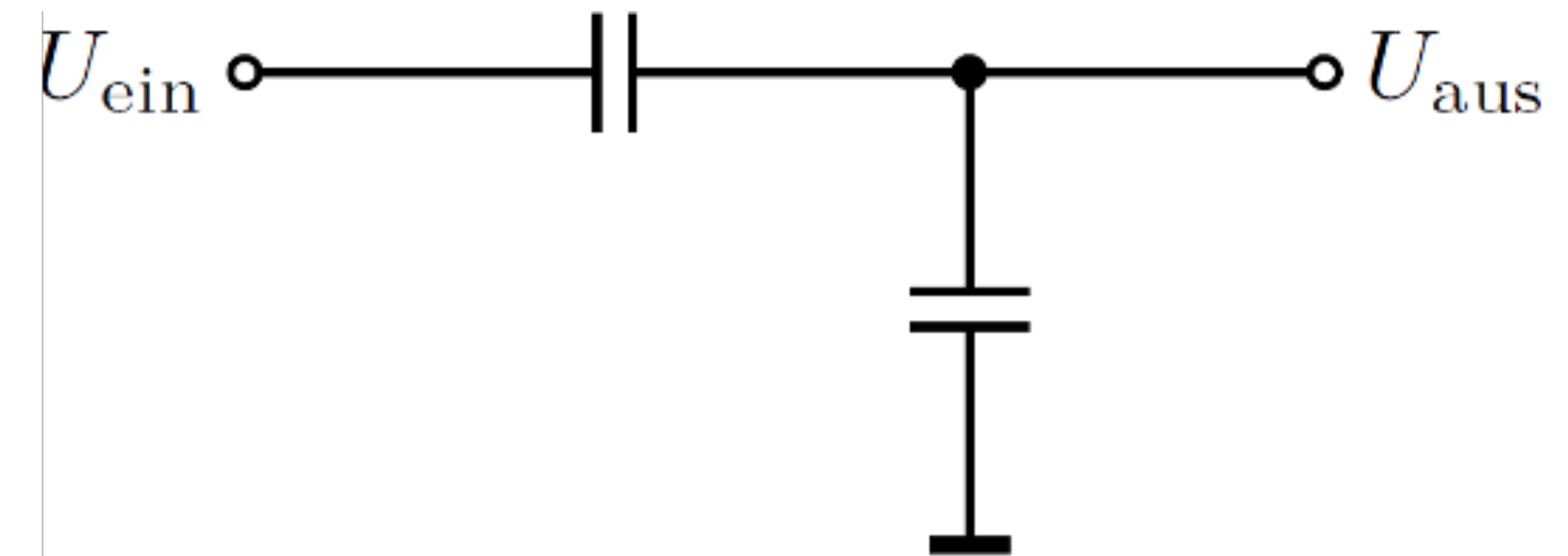


Charging:

S_1 closed,
 S_2 open

Discharging:

S_1 open,
 S_2 closed



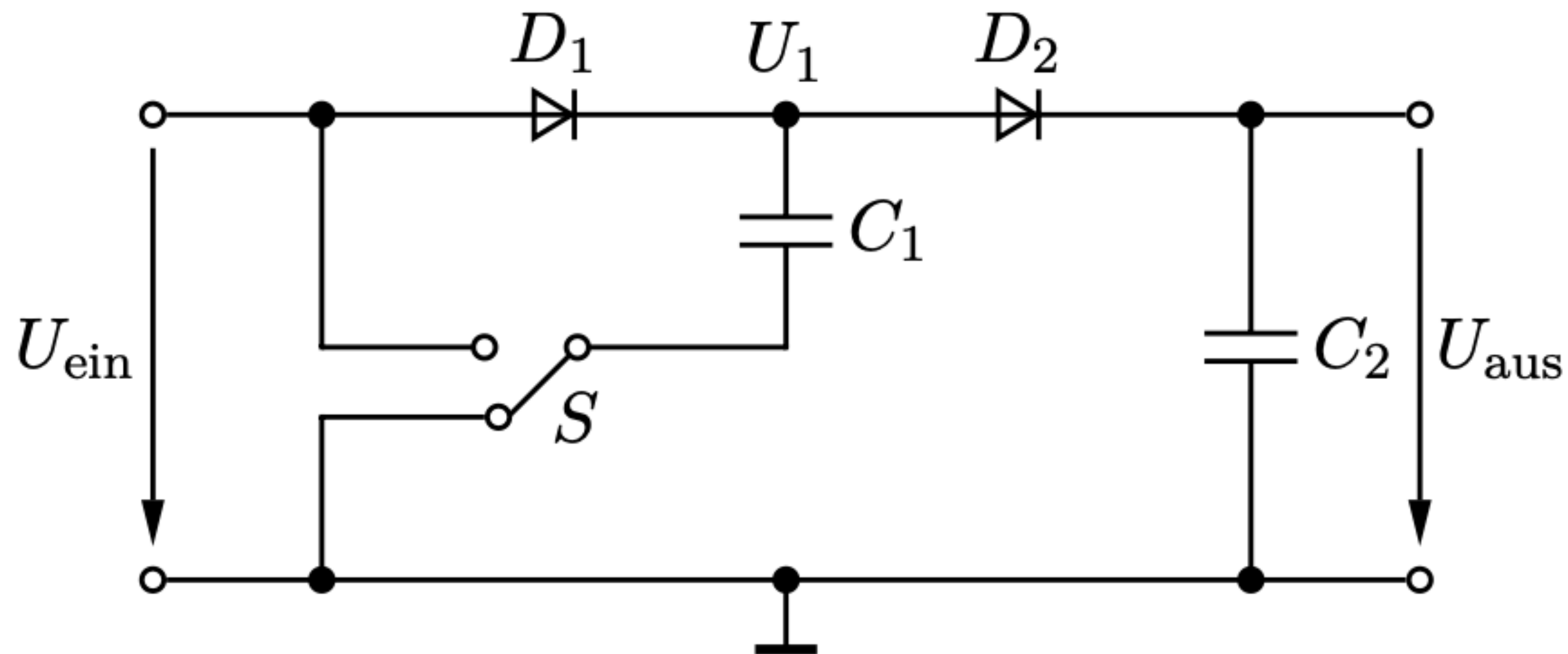
high switching frequency to achieve low fluctuations
in output voltage:
typically kHz - MHz

Here: $U_{aus} = 0.5 \times U_{ein}$
with more capacitors and switches other ratios can
also be achieved.

Charge Pump

Voltage Multiplication

- Similar to Greinacher Circuit for AC input (chapter 03).



$$U_{\text{aus}} = 2 \times U_{\text{ein}} - 2 \times U_D$$

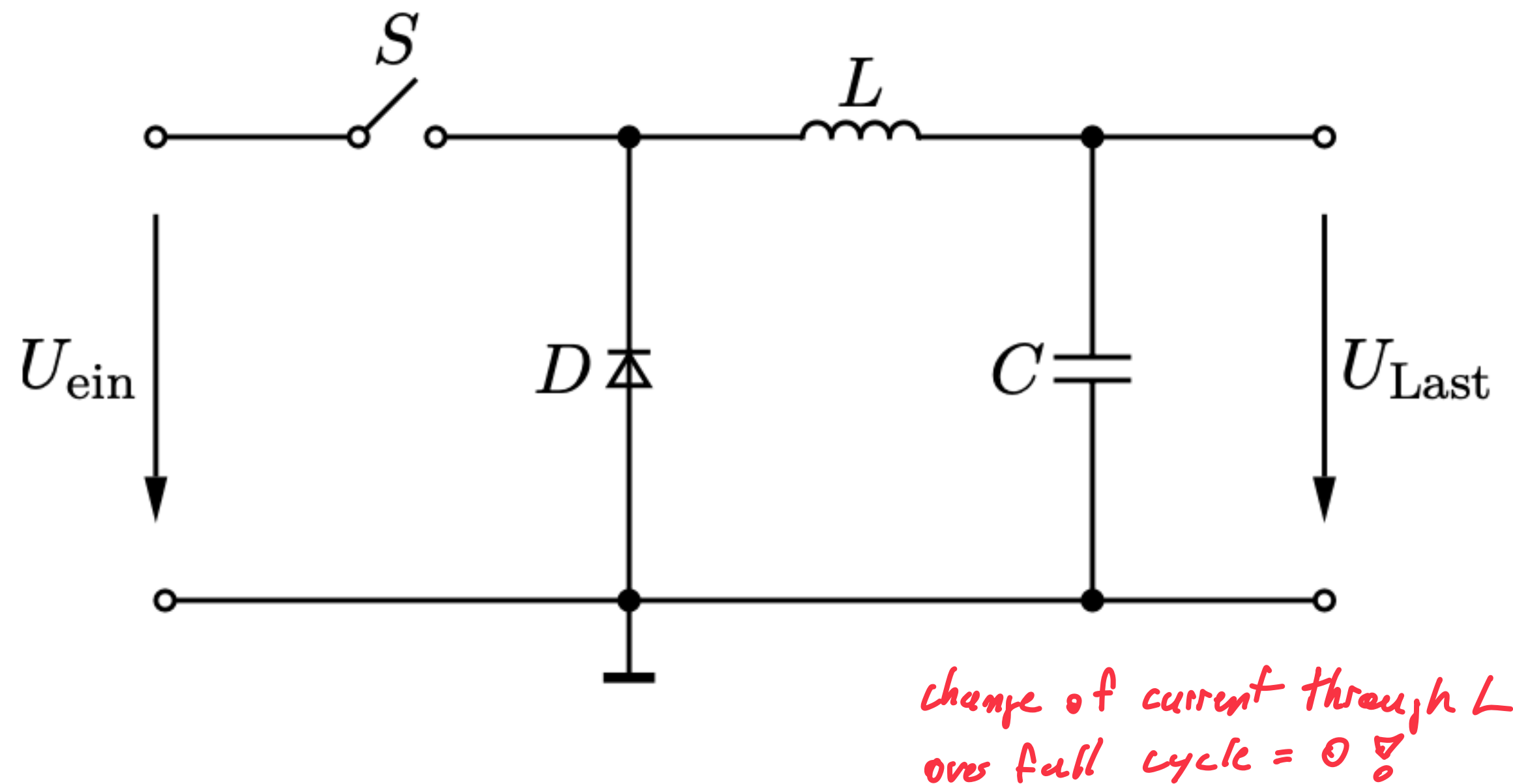
C_1 : “pump capacitor”

C_2 : “smoothing capacitor”

Buck Converter / Step-Down Converter

Down conversion - a classic circuit

- Inductor and capacitor



How it works

Switch S (in real life a transistor) is switched on and off with period T .

$$\text{duty cycle } D = T_{\text{on}} / T$$

Switch closed

$U_L = U_{\text{ein}} - U_{\text{Last}}$, diode in reverse bias

Switch open:

$U_L = -U_{\text{Last}}$, diode forward biased, inductor provides output

$$\int_0^{T_{\text{on}}} \frac{U_L}{L} dt + I_0 \approx \frac{U_{\text{ein}} - U_{\text{Last}}}{L} T_{\text{on}} + I_0 \stackrel{\text{red arrow}}{=} \int_0^T \frac{U_L}{L} dt + I_0 \approx \frac{U_{\text{Last}}}{L} (T - T_{\text{on}}) + I_0 = \frac{U_{\text{Last}}}{L} T_{\text{aus}} + I_0$$

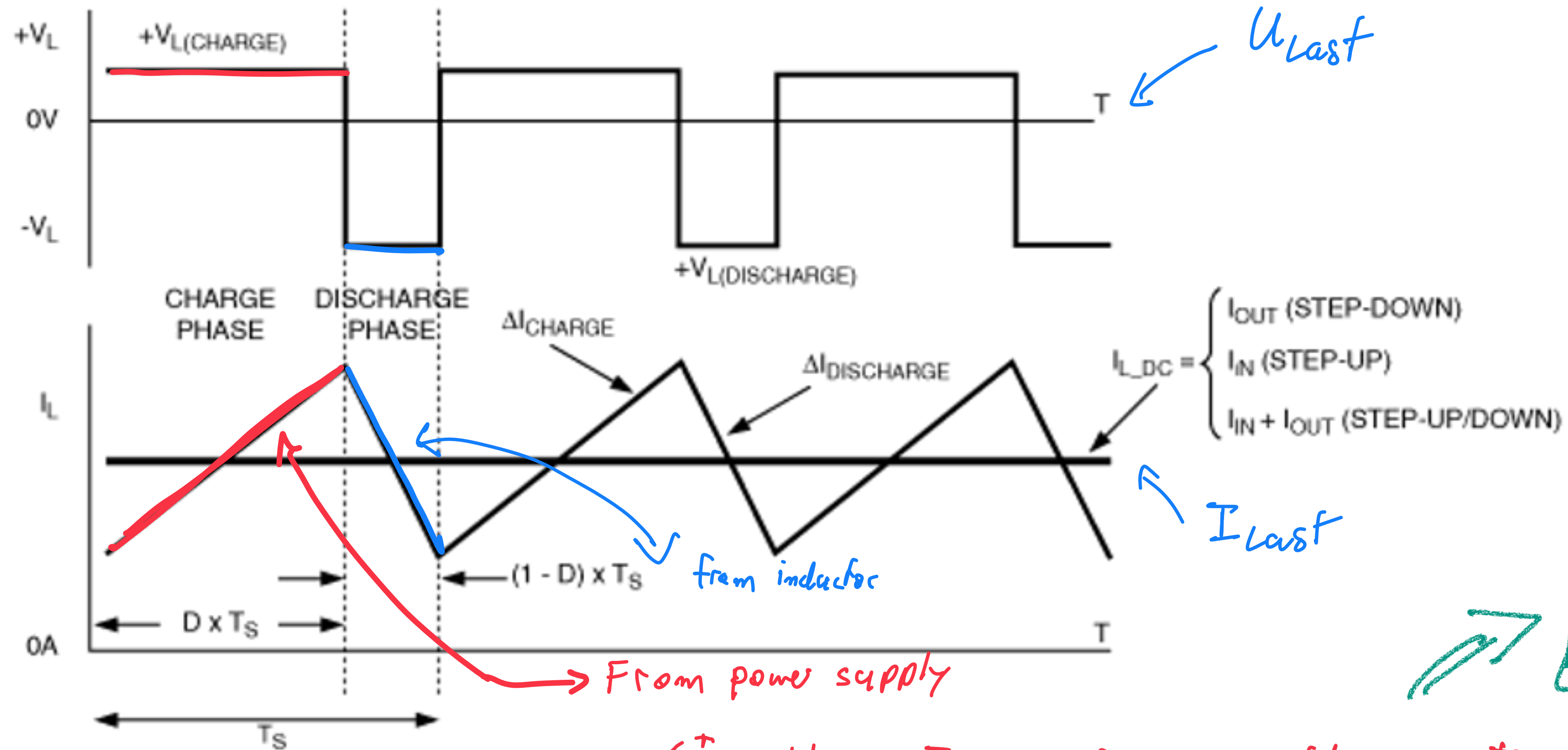
Results in:

$$(U_{\text{ein}} - U_{\text{Last}}) T_{\text{on}} = U_{\text{Last}} (T - T_{\text{on}}) \Rightarrow \boxed{\frac{U_{\text{Last}}}{U_{\text{ein}}} = D}$$

Buck Converter / Step-Down Converter

Down conversion - a classic circuit

- Time dependence of voltages and currents



$$\frac{U_{last}}{U_{ein}} = D$$

Efficiency ∇
 $\sim 100\%$

$$\oint \vec{P} = U_{ein} \cdot I_{last} \cdot D \cdot T = U_{last} \cdot I_{last} \cdot T$$

Voltage Regulation with Zener Diodes

Reminder

For sufficiently high U_{ein} :

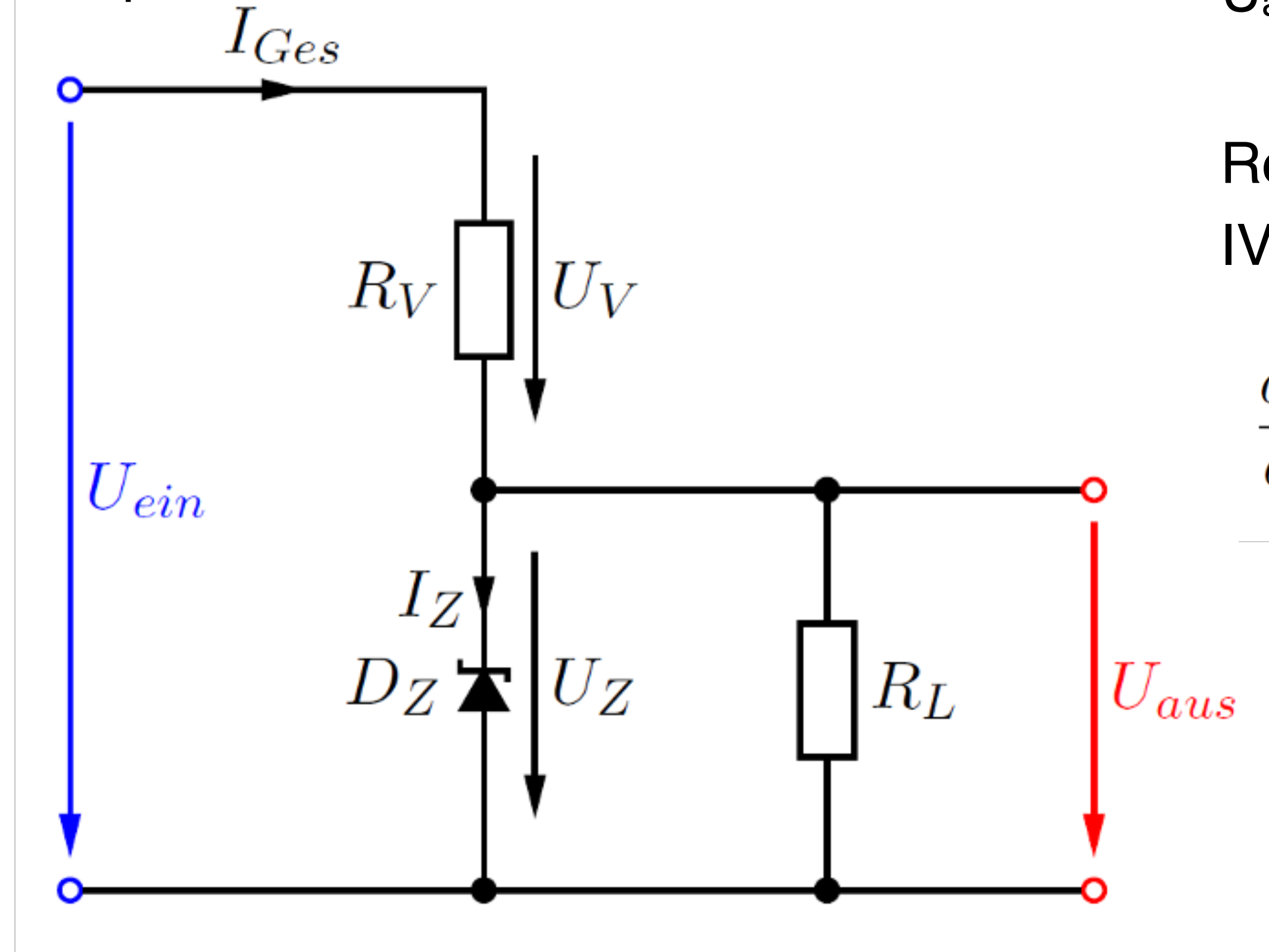
$U_{\text{aus}} = U_Z$; independent on U_{ein} .

Remains stable also for fluctuating load currents due to steep IV curve: U_Z reasonably independent from I_L .

$$\frac{dU_{\text{aus}}}{dU_{\text{ein}}} = \frac{R_Z \parallel R_L}{(R_Z \parallel R_L) + R_V} \approx \frac{R_Z}{R_V}$$

(good approximation:
 $R_Z \ll R_L$)

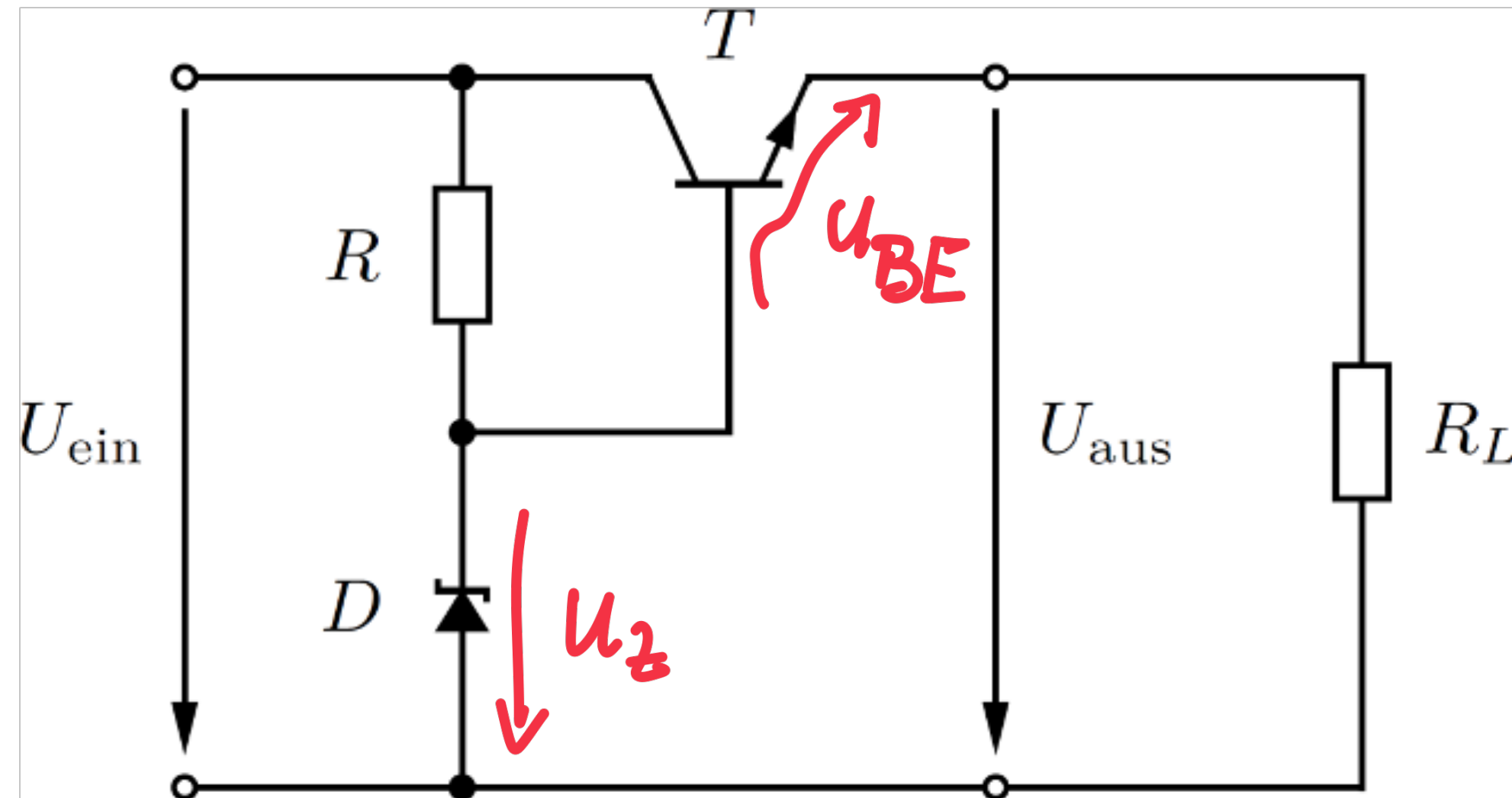
Chapter 03



Simple, but hits limits for high load currents. Strong temperature dependence due to diode.

Voltage Regulation with Zener Diodes

Extension for high Load Currents



- Additional transistor:
Enables high load currents since current flows through T , not R .

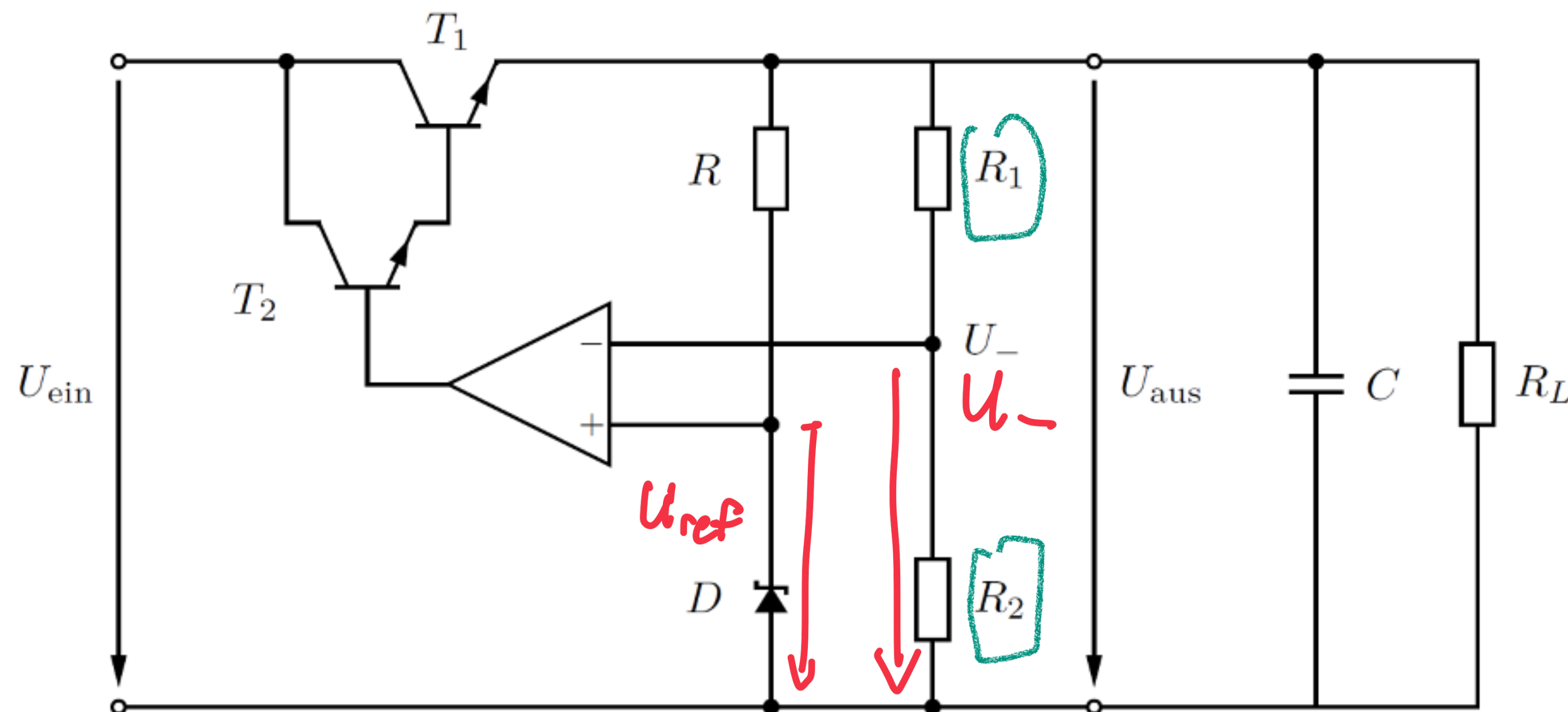
$$U_{\text{aus}} = U_Z - U_{BE}$$

Transistor configured as emitter follower
(common collector).

But: U_{BE} depends on current: not constant - typically between 0.5 V and 0.8 V
 U_{aus} only stable to within a few 100 mV!

Voltage Regulation

Extension with OpAmp



Darlington transistor T_1 , T_2 : Enables high load currents

How does this work?

U_{aus} is given by R_1 , R_2 , the Zener-Diode serves as voltage reference:

Golden rule:

$$U_- = U_{\text{ref}}$$

$$\Rightarrow U_- = U_{\text{aus}} \cdot \frac{R_2}{R_1 + R_2}$$

$$\Rightarrow U_{\text{aus}} = U_{\text{ref}} \left(\frac{R_1 + R_2}{R_2} \right)$$

Next (and final) Lecture:

Analog 15 - Chapter 08 - Tuesday, February 13, 2024

Time Plan for Next Lectures

A few Changes coming up!

Calender Week	Tuesday	Thursday
45	07.11. Analog	09.11. Digital
46	14.11. Analog	16.11. Digital
47	21.11. Digital	23.11. Analog
48	28.11. Digital	30.11. Digital
49	05.12. Digital	07.12. Analog
50	12.12. Digital	14.12. Analog
51	19.12. Analog	21.12. Digital
2	09.01. Analog	11.01. Digital
3	16.01. Digital	18.01. Digital
4	23.01. Analog	25.01. Digital
5	30.01. Analog	01.02. Digital
6	06.02. Analog	08.02. Analog
7	13.02. Analog	15.02. -

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