

# Problem Set 8

## Nonlinear Optics (NLO)

Due: July 03, 2018, 09:45 AM

### 1) Electro-optic Mach-Zehnder modulator

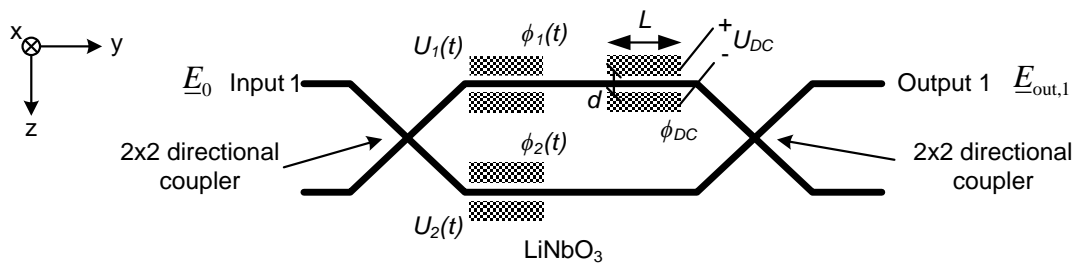


Figure 1: Dual-drive Mach-Zehnder modulator

Figure 1 shows a dual-drive Mach-Zehnder modulator. The device consists of a waveguide-based Mach-Zehnder interferometer having voltage-controlled phase shifters in each arm. For high-speed modulation, time-dependent voltages  $U_1(t)$  and  $U_2(t)$  are applied to two phase-shifters ( $\phi_1(t)$  and  $\phi_2(t)$ ) in the upper and lower arm, respectively, whereas a third phase shifter ( $\phi_{DC}$ ) operated by a constant DC bias voltage  $U_{DC}$  is used to set the operating point. The device is made of lithium-niobate ( $\text{LiNbO}_3$ ) using  $x$ -cut geometry. The principal axes<sup>1</sup> are the  $x$ ,  $y$  and  $z$  axes shown in Figure 1. The propagating light of wavelength  $\lambda = 1.55 \mu\text{m}$  is polarized along the  $z$  axis. The refractive indices are  $n_o = 2.211$  and  $n_e = 2.138$ . The electro-optic coefficients, measured at a wavelength of  $0.5 \mu\text{m}$  are  $r_{13} = 9.6 \text{ pm/V}$ ,  $r_{22} = 6.8 \text{ pm/V}$ ,  $r_{33} = 30.9 \text{ pm/V}$ , and  $r_{42} = 32.6 \text{ pm/V}$ . Assume that these values are also valid at the wavelength of  $1.55 \mu\text{m}$ .

1. Consider that  $U_1(t) = U_2(t) = 0$ , and an external voltage  $U_{DC}$  is applied to the two parallel metal contacts (length  $L = 2 \text{ mm}$ , distance  $d = 5 \mu\text{m}$ ), inducing a phase shift  $\phi_{DC}$  in the upper arm. What voltage  $U_{\pi,DC}$  is needed for a phase shift of  $\pi$  between both arms?

Hint: Start by calculating the change of refractive index as a function of the applied voltage  $U_{DC}$  and approximate the modulating electric field along the  $z$ -direction by the field of a parallel plate capacitor with electrode spacing  $d$ , i.e.,  $E_z^{(el)} \approx U_{DC} / d$ .

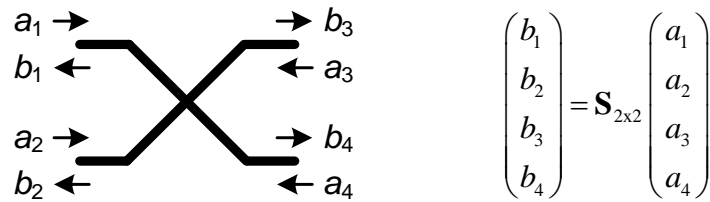
2. Consider the initial complex amplitude  $E_0$  at Input 1. Express the general amplitude transfer function for output 1 of the device,  $T_{out,1} = E_{out,1} / E_0$ , as a function of the applied phase shifts  $\phi_1(t)$ ,  $\phi_2(t)$ , and  $\phi_{DC}$ . Next, consider the situation from part 1 ( $U_1(t) = U_2(t) = 0$ ) and sketch the amplitude transfer function  $T_{out,1}$  and the power transfer function  $|T_{out,1}|^2$  versus the normalized applied voltage  $U_{DC} / U_{\pi}$ .

<sup>1</sup> The symmetry group of  $\text{LiNbO}_3$  is  $C_{3v} = 3m$ . The convention used here is that the  $z$ -axis is parallel to the threefold rotational axis of the crystal.

Hint: Assume that the device consists of lumped elements with individual scattering matrices. Using the input and output amplitudes  $a_i$  and  $b_i$  of a symmetric 2x2 directional coupler as indicated in Figure 2, its scattering matrix  $\mathbf{S}_{2 \times 2}$  can be written as

$$\mathbf{S}_{2 \times 2} = \frac{1}{\sqrt{2}} \begin{pmatrix} 0 & 0 & 1 & -j \\ 0 & 0 & -j & 1 \\ 1 & -j & 0 & 0 \\ -j & 1 & 0 & 0 \end{pmatrix}$$

where  $b_m = S_{nm} \cdot a_n$ .



**Figure 2: Definition of input and output amplitudes of a 2x2 directional coupler**

For operating the modulator in so-called push-pull mode, voltages of equal amplitude but opposite signs are applied to the two arms,  $U_1(t) = -U_2(t) = U(t)$ . The phase difference between both arms then amounts to  $\Delta\phi(t) = \phi_1(t) - \phi_2(t)$ .

- Adapt the expression of  $T_{out,1}$  from part 2 to the push-pull configuration. Sketch the amplitude transfer function as a function of the voltage  $U(t)$  normalized to the  $\pi$ -voltage  $U_{\pi,AC}$  of the high-frequency phase-shifters for  $\phi_{DC} = 0$ .  $U_{\pi,AC}$  is the voltage required to generate a phase difference of  $\Delta\phi(t) = \pi$  between the two arms.
- In some applications it is important to have a **linear** relationship between small variations  $\delta U(t)$  of the **input voltage** and the associated variations  $\delta E_{out,1}$  of the **optical amplitude** at output 1. This can be achieved by choosing a suitable DC bias,  $U_{DC}$ . Which bias voltage would you choose for this case?
- For the case that  $\phi_{DC} = 0$ , sketch the power transfer function at output 1 as a function of the normalized voltage  $U(t) / U_{\pi,AC}$ . Which output power is obtained when adjusting the bias voltage according to part 4?
- In other applications it is important to have a **linear** relationship between small variations of the **input voltage** and the associated variations of the **optical power**  $P \propto |E_{out,1}|^2$ . Which bias voltage would you choose for this case?

Pablo Marin-Palomo

Building: 30.10, Room: 2.33

Phone: 0721/608-42487

Philipp Trocha

Building: 30.10, Room: 2.32-2

Phone: 0721/608-42480

[nlo@ipq.kit.edu](mailto:nlo@ipq.kit.edu)