

① Sphärische Multipolentwicklung

$$\varphi(\vec{r}) = \frac{q}{64\pi a_0^5} r^2 e^{-r/a_0} \sin^2 \theta, \quad a_0 > 0$$

(a) Entwicklung nach sphärischen Multipolen

$$q_{lm} = \int d^3x' \varphi(\vec{r}') r'^l Y_{lm}^*(\theta', \varphi') \quad \oplus$$

drücke winkelabhängigen Teil durch Kugelflächenfunktionen aus: (suche ein Y_{lm} , das einen $\sin^2 \theta$ -Beitrag enthält – kein $e^{i\varphi}$, kein $\cos \theta \rightarrow$ jedoch 3.5)

$$Y_{20} = \sqrt{\frac{5}{4\pi}} \left(\frac{3}{2} \underbrace{\cos^2 \theta}_{1-\sin^2 \theta} - \frac{1}{2} \right) = \sqrt{\frac{5}{4\pi}} \left(1 - \frac{3}{2} \sin^2 \theta \right)$$

$$\Rightarrow \sin^2 \theta = -\sqrt{\frac{4\pi}{5}} \frac{2}{3} Y_{20}(\theta, \varphi) + \frac{2}{3} \quad \left. \begin{array}{l} Y_{00} = \frac{1}{\sqrt{4\pi}} \\ \frac{2\sqrt{4\pi}}{3} Y_{00}(\theta, \varphi) \end{array} \right\}$$

$$\begin{aligned} \Rightarrow q_{lm} &= \frac{q}{64\pi a_0^5} \int_0^\infty dr' r'^l \underbrace{r'^2}_{\text{Jacobi}} e^{-r'/a_0} \int d\Omega' Y_{lm}^*(\theta', \varphi') \underbrace{\left[Y_{00}(\theta', \varphi') - \frac{1}{\sqrt{4\pi}} Y_{20}(\theta', \varphi') \right]}_{\frac{2}{3} \sqrt{\frac{4\pi}{5}} \left(\delta_{l0}\delta_{m0} - \frac{1}{\sqrt{5}} \delta_{l2}\delta_{m0} \right)} \\ &= \frac{q}{64\pi a_0^5} \int_0^\infty dr' r'^{l+4} e^{-r'/a_0} \underbrace{\int d\Omega' Y_{lm}^*(\theta', \varphi') \left(\delta_{l0}\delta_{m0} - \frac{1}{\sqrt{5}} \delta_{l2}\delta_{m0} \right)}_{\text{Orthogonalität}} \\ &= \frac{q}{64\pi a_0^5} \int_0^\infty dr' r'^{l+4} e^{-r'/a_0} \underbrace{(l+4)! \frac{(+1)^{l+4}}{+1}}_{\substack{(l+4) \text{ mal} \\ \text{partiell integrieren}}} a_0^{l+4} \int_0^\infty dr' e^{-r'/a_0} \\ &= (l+4)! a_0^{l+5} \end{aligned}$$

$$\Rightarrow q_{00} = \frac{q}{64\pi a_0^5} \frac{2}{3} \sqrt{4\pi} (4+4)! a_0^{0+5} = \frac{q}{2\sqrt{\pi}}$$

$$q_{20} = \frac{q}{64\pi a_0^5} \frac{2}{3} \sqrt{4\pi} (2+4)! a_0^{2+5} \left(\frac{-1}{\sqrt{5}} \right) = \frac{-15}{\sqrt{5\pi}} q a_0^2$$

(b) Potential für große r nach Legendre - Polynom in $\cos\theta$ entwickeln

aximale Symmetrie
keine φ -Abhängigkeit

(2)

$$\Phi(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int d^3r' \frac{\rho(\vec{r}')}{|\vec{r} - \vec{r}'|} = \frac{1}{\epsilon_0} \sum_{l,m} \frac{1}{2l+1} Y_{lm}(\theta, \varphi) \int d^3r' \rho(\vec{r}') \frac{r'^l}{r^{l+1}} Y_{lm}^*(\theta', \varphi')$$

$$r'_l = \min(r, r'), \quad r'_r = \max(r, r')$$

Entwicklung für große $r \rightarrow$ nur $\frac{r'^l}{r^{l+1}}$ relevant

$$\text{da } \int_0^{\infty} dr' r'^2 \rho(r') \frac{r'^l}{r^{l+1}} = \int_0^r dr' r'^{l+2} \rho(r') + \int_r^{\infty} dr' r'^2 \frac{r'^l}{r^{l+1}} \rho(r')$$

$$\underbrace{\int_r^{\infty} dr' r'^{l+2} \rho(r')}_{\sim e^{-r'/a_0} \int_r^{\infty} dr' r'^{l+2} e^{-r'/a_0}} \sim e^{-r/a_0} \text{ f. } r \rightarrow \infty$$

$r \rightarrow \infty$

$$\Phi(\vec{r}) = \frac{1}{\epsilon_0} \sum_{l,m} \frac{Y_{lm}(\theta, \varphi)}{2l+1} \frac{1}{r^{l+1}} \int d^3r' \frac{r'^l}{(r')^{l+1}} \rho(\vec{r}') \int d\Omega' Y_{lm}^*(\theta', \varphi')$$

$$q_{lm} = \delta_{l0} \delta_{m0} \frac{q}{\sqrt{4\pi}} - \delta_{l2} \delta_{m0} \frac{15}{\sqrt{4\pi}} q a_0^2 - q_{20}$$

$$\boxed{\Phi(\vec{r}) = \frac{1}{\epsilon_0} Y_{00}(\theta, \varphi) \frac{q_{00}}{r} + \frac{1}{\epsilon_0} Y_{20}(\theta, \varphi) \frac{q_{20}}{r^3}}$$

$$\text{Kartesische Multipoles: } \Phi(\vec{r}) = \frac{1}{4\pi\epsilon_0} \left[\frac{Q}{|\vec{r}|} + \frac{\vec{p} \cdot \vec{r}}{|\vec{r}|^3} + \frac{1}{2} \sum_{ij} \frac{x_i Q_{ij} x_j}{|\vec{r}|^5} + \dots \right]$$

$$\text{ablesen: } \frac{1}{4\pi} \frac{Q}{r} = Y_{00} \frac{q_{00}}{r} = \frac{1}{\sqrt{4\pi}} \frac{q}{\sqrt{4\pi} r} \rightarrow \boxed{Q = q}$$

$\vec{p} = 0$ (kein Term $\sim r^{-2}$)

$$\frac{1}{r^2} \sum_{ij} x_i Q_{ij} x_j = 2 \cdot 4\pi Y_{20} \frac{-15}{\sqrt{4\pi}} \frac{q a_0^2}{r} = 8 \cdot 4\pi \sqrt{\frac{15}{4\pi}} \frac{-15}{\sqrt{4\pi}} \frac{q a_0^2}{r} \left(\frac{3}{2} \cos^2\theta - \frac{1}{2} \right)$$

$$= -6 q a_0^2 (3 \cos^2\theta - 1)$$

$$= -6 \frac{q a_0^2}{r^2} (3z^2 - r^2)$$

$$x^2 Q_{xx} + y^2 Q_{yy} + z^2 Q_{zz}$$

aximale Symm.: $Q_{xx} = Q_{yy}$

$Q_{zz} = -2 Q_{xx}$ (Spurlos)

$$\frac{1}{2} (2z^2 - x^2 - y^2) = Q_{zz} (3z^2 - r^2) \rightarrow Q_{zz} = -12 q a_0^2 = -2 \frac{Q_{xx}}{r^2}$$

$$= -2 \frac{Q_{xx}}{r^2}$$

Entwicklung nach Kugelflächenfunktionen:

(3)

$$\Phi(\vec{r}) = \frac{1}{\epsilon_0} \sum_{l,m} \frac{Y_{lm}(\theta, \varphi)}{2l+1} \int d\Omega' Y_{lm}^*(\theta', \varphi') \frac{r'^l}{r^{l+1}} \rho(\vec{r}')$$

$$r'_1 = \min(r, r'), \quad r'_2 = \max(r, r')$$

(c) Nahe $r=0$

$$\Phi(\vec{r}) = \frac{1}{\epsilon_0} \sum_{l,m} \frac{Y_{lm}(\theta, \varphi)}{2l+1} r^l \int d\Omega' Y_{lm}^*(\theta', \varphi') \rho(\vec{r}')$$

$$= \frac{1}{\epsilon_0} \sum_{l,m} \frac{Y_{lm}(\theta, \varphi)}{2l+1} r^l \int_0^\infty dr' r'^{l+2} e^{-r'/a_0} \left(\delta_{l0} \delta_{m0} - \frac{1}{\sqrt{5}} \delta_{l2} \delta_{m0} \right) \frac{2\sqrt{4\pi} q}{3 \cdot 64 \pi a_0^5}$$

$$= \frac{1}{\epsilon_0} \frac{q}{64 \pi a_0^5} \frac{2\sqrt{4\pi}}{3} \left\{ Y_{00} \int_0^\infty dr' r'^3 e^{-r'/a_0} - \frac{1}{\sqrt{5}} Y_{20} \int_0^\infty dr' r'^3 e^{-r'/a_0} \right\}$$

$$= \frac{1}{\epsilon_0} \frac{q}{64 \pi a_0^5} \frac{2\sqrt{4\pi}}{3} \left\{ -a_0^4 e^{-r/a_0} \Big|_0^\infty + a_0^4 \int_0^\infty dr' e^{-r'/a_0} - \frac{1}{\sqrt{5}} Y_{20} \left(-a_0^4 e^{-r/a_0} \Big|_0^\infty + a_0^4 \int_0^\infty dr' e^{-r'/a_0} \right) \right\}$$

$$= \frac{q}{48 \pi \epsilon_0 a_0^5} \left[Y_{00} a_0 (6a_0^3 + 6a_0^2 r + 3a_0 r^2 + r^3) e^{-r/a_0} - \frac{r^2}{\sqrt{5}} Y_{20} a_0 (r+a_0) e^{-r/a_0} \right]$$

Entwickle $e^{-r/a_0} = 1 - \frac{r}{a_0} + \frac{r^2}{2a_0^2} - \frac{r^3}{6a_0^3} + \dots$

dann: $a_0 (6a_0^3 + 6a_0^2 r + 3a_0 r^2 + r^3) \left(1 - \frac{r}{a_0} + \frac{r^2}{2a_0^2} - \frac{r^3}{6a_0^3} + \dots \right)$

$$= 6a_0^4 + \mathcal{O}(r^4)$$

ebenso $r^2 a_0 (a_0 + r) e^{-r/a_0} = a_0^2 r^2 + \mathcal{O}(r^4)$

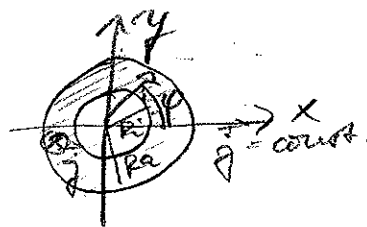
$$= \frac{q}{48 \pi \epsilon_0 a_0^5} \left[\frac{Y_{00}}{\sqrt{4\pi}} \cdot 6a_0^4 - \frac{1}{\sqrt{5}} Y_{20} r^2 a_0^2 + \mathcal{O}(r^4) \right]$$

$$= \frac{q}{36 \pi \epsilon_0} \left[\frac{6}{a_0} - \frac{1}{\sqrt{5}} \frac{r^2}{a_0^3} \left(\frac{3}{2} \cos^2 \theta - \frac{1}{2} \right) + \mathcal{O}(r^4) \right]$$

$$P_2(\cos \theta)$$

$$= \frac{q}{4 \pi \epsilon_0 a_0} \left[\frac{1}{4} - \frac{1}{120} \frac{r^2}{a_0^2} P_2(\cos \theta) + \mathcal{O}(r^4) \right]$$

② zylinderförmiger Hohlleiter



(a) magnetische Induktion mittels

Biot-Savart: $\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int d^3x' \frac{\vec{j}(\vec{r}') \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$

Rotationsymmetrie um z-Achse: $\vec{B}$ φ -unabhängig

$\vec{r} = \rho \vec{e}_\rho + z \vec{e}_z$, $\vec{j} = j_0 \vec{e}_z$ mit $j_0 = \text{const.}$

$|\vec{r} - \vec{r}'| = (\rho^2 + \rho'^2 - 2\rho\rho' \cos \varphi' + (z - z')^2)^{1/2}$

Wähle o.B.d.A. $\varphi = 0$

$\vec{j} \times \vec{r} = j_0 \vec{e}_z \times (\rho \vec{e}_\rho + z \vec{e}_z) = j_0 \rho \vec{e}_\varphi$

$\vec{B}(\vec{r}) = \frac{\mu_0 j_0}{4\pi} \int_{R_i}^{R_a} d\rho' \rho' \int_0^{2\pi} d\varphi' \int_{-\infty}^{\infty} dz' \frac{\rho \vec{e}_\varphi - \rho' \vec{e}_{\varphi'}}{\sqrt{\rho^2 + \rho'^2 - 2\rho\rho' \cos \varphi' + (z - z')^2}}$

$= \frac{\mu_0 j_0}{4\pi} \int_{R_i}^{R_a} d\rho' \rho' \int_0^{2\pi} d\varphi' \frac{2(\rho \vec{e}_\varphi - \rho' \vec{e}_{\varphi'})}{\rho^2 + \rho'^2 - 2\rho\rho' \cos \varphi'}$

$\vec{e}_{\varphi'} = \begin{pmatrix} -\sin \varphi' \\ \cos \varphi' \\ 0 \end{pmatrix}$

$\vec{e}_\varphi = \vec{e}_y$ wg. $\varphi = 0$

$\rho \vec{e}_\varphi - \rho' \vec{e}_{\varphi'} = \sin \varphi' \vec{e}_x + (\rho - \rho' \cos \varphi') \vec{e}_y$

$\vec{e}_y \int_0^{2\pi} d\varphi' \frac{\rho - \rho' \cos \varphi'}{\rho^2 + \rho'^2 - 2\rho\rho' \cos \varphi'} = \vec{e}_y \int_0^{2\pi} d\varphi' \frac{1}{3} \left(\frac{\rho^2 + \rho'^2 - 2\rho\rho' \cos \varphi'}{\rho^2 + \rho'^2 - 2\rho\rho' \cos \varphi'} + \frac{\rho^2 - \rho'^2}{\rho^2 + \rho'^2 - 2\rho\rho' \cos \varphi'} \right)$

$= \frac{2\pi}{\rho} + \frac{\rho^2 - \rho'^2}{\rho} \frac{2\pi}{|\rho^2 - \rho'^2|}$ da $\frac{\rho^2 + \rho'^2 - 2\rho\rho' \cos \varphi'}{|\rho^2 - \rho'^2|} = 1$

$\vec{B}(\vec{r}) = \frac{\mu_0 j_0}{4\pi} \vec{e}_y \int_{R_i}^{R_a} d\rho' \rho' \left[\frac{2\pi}{\rho} + \frac{\rho^2 - \rho'^2}{\rho} \frac{2\pi}{|\rho^2 - \rho'^2|} \right]$

$= \frac{\mu_0 j_0}{4\pi} \vec{e}_y \int_{R_i}^{R_a} d\rho' \rho' \frac{4\pi}{\rho} \Theta(\rho - \rho') \quad \text{da} \quad \frac{x}{|x|} = \text{sgn}(x)$

$\hookrightarrow \frac{1}{\rho} - \frac{1}{\rho} \frac{\rho^2 - \rho'^2}{|\rho^2 - \rho'^2|} = \frac{2}{\rho} \Theta(\rho - \rho')$

$\vec{B}(\vec{r}) = \begin{cases} 0 & \text{für } \rho < R_i \\ \vec{e}_y \frac{\mu_0 j_0}{4\pi} \frac{4\pi}{\rho} \frac{R_a^2 - R_i^2}{2} = \frac{\mu_0 j_0}{2} (R_a^2 - R_i^2) \vec{e}_y & \text{für } \rho > R_a \\ \vec{e}_y \frac{\mu_0 j_0}{4\pi} \frac{4\pi}{\rho} \frac{\rho^2 - R_i^2}{2} = \frac{\mu_0 j_0}{2} (\rho^2 - R_i^2) \vec{e}_y & \text{für } R_i < \rho < R_a \end{cases}$
(obere Grenze = ρ)

(b) Symmetrieüberlegungen: $\vec{B}(\vec{r}) = B_\rho \vec{e}_\rho + B_\varphi \vec{e}_\varphi + B_z \vec{e}_z$
 wobei: $\vec{B}(\vec{r}) = \vec{B}(\rho)$ (keine Abhängigkeit von φ und z)

Maxwell-Gleichungen:

$$\vec{\nabla} \cdot \vec{B} = 0 \rightarrow \text{Gauß: } 0 = \int (\vec{\nabla} \cdot \vec{B}) dV = \oint \vec{B} \cdot d\vec{a} = B_\rho \int d\varphi \int dz B_\rho(\rho)$$

zu pol. $\vec{e}_\rho \Rightarrow \oint B_\rho = 0$

$$\vec{\nabla} \times \vec{B} = \mu_0 j_0 \vec{e}_z \rightarrow B_z = 0 \Rightarrow \boxed{\vec{B}(\vec{r}) = B_\varphi(\rho) \vec{e}_\varphi}$$

Berechne B_φ : $2\pi \rho B_\varphi(\rho) = \mu_0 \int \vec{j} \cdot d\vec{a}$ (über Stokes: $\vec{\nabla} \times \vec{B} = \mu_0 \vec{j}$)

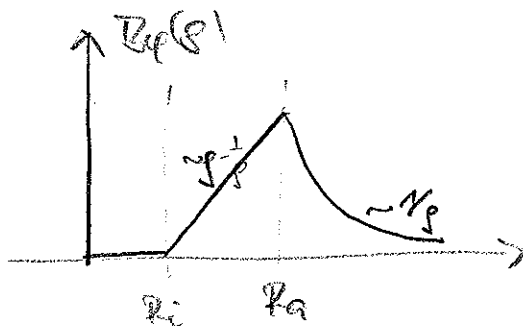
$$= \begin{cases} 0 & \text{für } \rho \leq R_i \\ \mu_0 I & \text{für } \rho \geq R_a \\ \mu_0 I \frac{\rho^2 - R_i^2}{R_a^2 - R_i^2} & \text{für } R_i \leq \rho < R_a \end{cases}$$

$\int_{\vec{B}} d\vec{B} = \mu_0 \int \vec{j} \cdot d\vec{a}$
 $\int \vec{j} \cdot d\vec{a} = \int j_0 d\varphi dz$

$$\int \vec{j} \cdot d\vec{a} = j_0 \int_0^{2\pi} d\varphi \int_{R_i}^{\rho} ds s = \underbrace{2\pi j_0 (R_a^2 - R_i^2)}_{\equiv I} (\rho^2 - R_i^2)$$

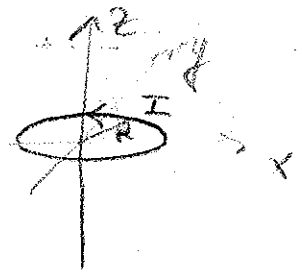
Integrationen konstante: $j_0 \rightarrow R_i$
 Normierung auf Fläche $\rightarrow j_0$: Stromdichte damit $\equiv 0$ für $\rho = R_i$

$$B_\varphi(\rho) = \frac{\mu_0 I}{2\pi \rho} \begin{cases} 0 & , \rho \leq R_i \\ \frac{\rho^2 - R_i^2}{R_a^2 - R_i^2} & , R_i \leq \rho < R_a \\ 1 & , \rho \geq R_a \end{cases}$$



③ Kreisförmige Leiterschleife

⑥



(a) Biot-Savart:

$$\vec{B}(\vec{r}) = \frac{\mu_0 I}{4\pi} \oint \frac{d\vec{r}' \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}, \quad \text{Feld entlang z-Achse: } \vec{r} \sim \vec{e}_z$$

Zylinderkoordinaten: $\vec{r}' = R \vec{e}_{\varphi'} = R \begin{pmatrix} \cos \varphi' \\ \sin \varphi' \\ 0 \end{pmatrix}$

$$(\vec{e}_3 \times \vec{e}_{\varphi'} = \vec{e}_z)$$

$$d\vec{r}' = R d\varphi' \vec{e}_{\varphi'} = R d\varphi' \begin{pmatrix} -\sin \varphi' \\ \cos \varphi' \\ 0 \end{pmatrix}$$

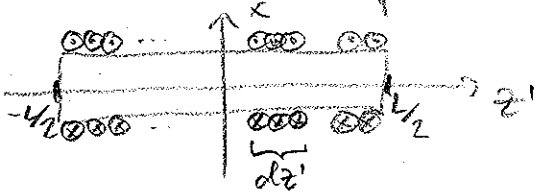
$$\vec{r} - \vec{r}' = \begin{pmatrix} -R \cos \varphi' \\ -R \sin \varphi' \\ z \end{pmatrix}, \quad d\vec{r}' \times (\vec{r} - \vec{r}') = R d\varphi' \vec{e}_{\varphi'} \times (-R \vec{e}_{\varphi'} + z \vec{e}_z) = R d\varphi' (+R \vec{e}_z + z \vec{e}_{\varphi'})$$

$$|\vec{r} - \vec{r}'| = \sqrt{R^2 + z^2}$$

$$= R d\varphi' \begin{pmatrix} z \cos \varphi' \\ z \sin \varphi' \\ R \end{pmatrix}$$

$$\begin{aligned} \vec{B}(\vec{r}) &= \frac{\mu_0 I}{4\pi} \int_0^{2\pi} d\varphi' \frac{R \begin{pmatrix} z \cos \varphi' \\ z \sin \varphi' \\ R \end{pmatrix}}{\sqrt{R^2 + z^2}^3} = \frac{\mu_0 I R}{4\pi \sqrt{R^2 + z^2}^3} \begin{pmatrix} 0 \\ 0 \\ 2\pi R \end{pmatrix} \\ &= \frac{\mu_0 I}{2} \frac{R^2}{\sqrt{R^2 + z^2}^3} \vec{e}_z = \int_0^{2\pi} \frac{\mu_0 I}{2} \frac{R^2}{R^3} \frac{1}{2R} d\varphi', \quad z \ll R \quad \text{Integration über volle Periode} \\ &\quad \left[\frac{\mu_0 I}{2} \frac{R^2}{z^3} \left(1 - \frac{3}{2} \frac{R^2}{z^2} + \dots \right), \quad z \gg R \right] \end{aligned}$$

(b) lange, dicht gewickelte Spule (Länge L, Radius R, Windungszahl N)
 ↳ Annäherung kreisförmiger Leiterschleifen



$$dN = \frac{N}{L} dz' = n dz' \quad (\# \text{ Windungen in Intervall } dz')$$

$$\hookrightarrow \text{Strom } dI = I n dz'$$

Magnetfeld in z-Richtung (aus a)) $dB_z = \frac{\mu_0}{2} dI \frac{R^2}{\sqrt{R^2 + z'^2}^3}$

$$B_z(z) = \frac{\mu_0 I}{2} n R^2 \int_{-L/2}^{L/2} \frac{dz'}{[R^2 + (z - z')^2]^{3/2}} = \frac{\mu_0 I}{2} n \left[\frac{z - L/2}{[R^2 + (z - L/2)^2]^{3/2}} + \frac{z + L/2}{[R^2 + (z + L/2)^2]^{3/2}} \right]$$

Sehr lange Spule: $\lim_{L \rightarrow \infty} B_z = \frac{\mu_0 I n}{2} \cdot 2 = \mu_0 I n = \text{const.}$

④ Kraft auf lokale Stromverteilung

$$\vec{F} = \int d^3r \vec{j}(\vec{r}) \times (\vec{r} \cdot \vec{\nabla}) \vec{B}(\vec{r}) \Big|_{\vec{r}=0} + \dots$$

$$\Leftrightarrow \vec{F} = \frac{1}{2} \int d^3r (\vec{r} \times \vec{j}(\vec{r})) \times \vec{\nabla} \times \vec{B}(0) \Big|_{\vec{r}=0} + \dots$$

$$\rightarrow F_i = \epsilon_{ijk} \int d^3r j_j \underbrace{(\vec{r} \cdot \vec{\nabla}) B_k(0)}_{\vec{r} \cdot (\vec{\nabla} B_k(0))} \quad \textcircled{\ast} \quad \left. \vec{B}(\vec{r}) \right|_{\vec{r}=0} = \vec{B}(0)$$

$$= \epsilon_{ijk} \delta_{mn} \int d^3r j_j r_m \partial_n B_k$$

Nutze Kontinuitätsgleichung $\vec{\nabla} \cdot \vec{j} = 0$:

$$\int d^3r r_k j_e = \int d^3r r_k \underbrace{\vec{\nabla} \cdot (\epsilon_{ekl} \vec{r})}_{\delta_{ek} j_l + 0} \stackrel{\text{partiell integrieren}}{=} - \int d^3r (\vec{\nabla} r_k) r_e j_l = - \int d^3r r_e j_l$$

aus $\vec{\nabla} \cdot \vec{j} = 0$

$$\int d^3r (\vec{a} \cdot \vec{r}) \vec{j} \stackrel{\text{vec. calc}}{=} - \int d^3r (\vec{a} \cdot \vec{\nabla}) \vec{r} \stackrel{\text{vec. calc}}{=} - \frac{1}{2} \vec{a} \times \int d^3r (\vec{r} \times \vec{j}) \quad \textcircled{\ast\ast}$$

$$= -\frac{1}{2} \epsilon_{ijk} a_j \underbrace{\int d^3r \epsilon_{klm} r_e j_m}_{\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}}$$

$$= -\frac{1}{2} a_j \int d^3r (r_e j_i - r_j j_e) = \vec{a} \cdot \int d^3r \vec{r} j_i = \int d^3r (\vec{a} \cdot \vec{r}) j_i$$

$$\textcircled{\ast} = \epsilon_{ijk} \int d^3r j_j \vec{r} \cdot \vec{a}_k \text{ mit } \vec{a}_k = \vec{\nabla} B_k$$

$$\stackrel{\textcircled{\ast\ast}}{=} -\frac{1}{2} \epsilon_{ijk} \left[\underbrace{\vec{\nabla} B_k}_{\vec{m}} \times \underbrace{\int d^3r (\vec{r} \times \vec{j})}_{\vec{m}} \right]_j = -\epsilon_{ijk} [\vec{m} \times \vec{\nabla} B_k]_j = -\epsilon_{ijk} [\vec{m} \times \vec{\nabla}]_j B_k$$

$$= +\epsilon_{ijk} [\vec{m} \times \vec{\nabla}]_j B_k$$

$$\rightarrow \vec{F} = (\vec{m} \times \vec{\nabla}) \times \vec{B}(0) = \frac{1}{2} \int d^3r [(\vec{r} \times \vec{j}) \times \vec{\nabla}] \times \vec{B}(0)$$